



Bidirectional wakes over complex terrain using SCADA data and wake models

Nanako Sasanuma¹, Akihiro Honda², Christian Bak³, Niels Trolldborg³, Mac Gaunaa³, Morten Nielsen³,
and Teruhisa Shimada¹

¹Graduate School of Science and Technology, Hirosaki University, Bunkyo-cho 3, Hirosaki, 036–8561, Japan

²Aomori Public University, Department of Management and Economics, Aomori, 030-0196, Japan

³DTU Wind and Energy Systems, Technical University of Denmark, Roskilde, 4000, Denmark

Correspondence: Nanako Sasanuma (h22ds203@hirosaki-u.ac.jp)

Received: 17 July 2025 – Discussion started: 25 July 2025

Revised: 5 December 2025 – Accepted: 16 December 2025 – Published: 23 January 2026

Abstract. We investigate bidirectional wake effects between two wind turbines of the same type in a hill region in northern Japan using supervisory control and data acquisition (SCADA) data and validate the simulated wakes using 12 wake models. The extent to which complex terrain affects wake behavior has not yet been fully studied, and further understanding of the fundamental characteristics of bidirectional wakes over complex terrain is required. The two wind turbines are located 3.17 times the rotor diameter apart, with a different elevation of 0.44 times the rotor diameter. First, we identify the wake effects in terms of wind speed ratio, which is defined as a ratio of wind speed at the downstream wind turbine to that at the upstream wind turbine. By comparing the conditions according to the operating state of the upstream wind turbine, the wakes are clearly detected as minimum wind speed ratios for northeasterly and southwesterly winds. The wind speed ratio with a maximum wake effect occurs below the rated wind speed. Increases in turbulence intensity and decreases in power output are greater for southwesterly wind than for northeasterly wind. This difference arises from the combined effects of the turbine-induced wake and the terrain-induced variation in wind speed. Then, we examine the winds and the wakes over complex terrain by using Wind Atlas Analysis and Application Program Computational Fluid Dynamics (WAsP CFD) in combination with PyWake. The wind speed ratios derived from the wake models show strong dependence on inflow wind speed, reflecting the thrust coefficient curve used in the wake models. The wake models commonly overestimate the reduction in wind speed ratio for northeasterly wind and underestimate it for southwesterly wind. This comparative study contributes to understanding the additional effects of topography on wake effects in onshore wind power plants and offshore wind power plants near the coast.

1 Introduction

Considering the effects of wakes generated by neighboring wind turbines is crucial in designing a layout of wind power plants. We need to manage the wake effects; otherwise, wakes can negatively impact downstream wind turbines by reducing wind speeds and power output and by increasing turbulence intensity and load fluctuation. Moreover, the topography affects the wakes and makes the airflow more complex. An increasing number of wind turbines are being installed in complex terrains, such as hills, escarpments, valleys, and gorges, as the availability of flat terrain suitable

for wind power plants is decreasing. Although installation in complex terrain poses logistic challenges, strong winds induced by topographic effects offer an advantage for wind resources (e.g., Yamaguchi et al., 2024). Thus, the combined effects of wake and terrain further complicate the optimization of the performance and control strategies of wind power plants.

Analyzing wind measurement data is essential for understanding wake phenomena (e.g., Rhodes and Lundquist, 2013; Hansen et al., 2016; El-Asha et al., 2017; Mittelmeier et al., 2017; Astolfi et al., 2018; Han et al., 2018). Among

various observational data, the method of supervisory control and data acquisition (SCADA) provides the advantage of enabling concurrent analysis of wind conditions at hub height and operating states of wind turbines. In addition to the SCADA data, external measurements, such as light detection and ranging (lidar) measurements, are widely used to observe wakes. Combined use of various observations enables us to further investigate the impact of wakes on the power generation of downstream wind turbines in flat terrain (El-Asha et al., 2017) and in complex terrain (Han et al., 2018) and on turbulence intensity at downstream wind turbines (Mittelmeier et al., 2017). Rhodes and Lundquist (2013) indicate a dependence of wake effects on the inflow wind speed and show the vertical structures of reductions in wind speed and increases in turbulence intensity due to wakes by installing two Doppler lidars on the upstream and downstream sides of a wind turbine. Astolfi et al. (2018) use SCADA data with numerical simulation to demonstrate that the wake structures are distorted by the surrounding terrain and that wind speed recovery is quicker over complex terrain than over flat terrain. Using SCADA data in conjunction with external measurements is an effective method for wake detection. However, using external measurements involves high costs for operation and maintenance, and operation periods of the external measurements are often limited.

Numerical simulations enable us to effectively analyze the wake and to complement observations (Göçmen et al., 2016; Carbajo Fuertes et al., 2018; Bastankhah and Porté-Agel, 2014; Fischereit et al. 2022; Troldborg et al., 2022). Göçmen et al. (2016) show that wake models have different advantages in terms of usability, accuracy, quantity and quality of input data, and computational costs by evaluating the utilization of the six wake models with SCADA data in onshore and offshore wind power plants. A Gaussian wake model is validated by two pulsed scanning Doppler lidars mounted on the nacelle, which measure both the incoming flow and the downstream wake (Carbajo Fuertes et al., 2018). Bastankhah and Porté-Agel (2014) validate a Gaussian model for the reproducibility of wind speed at the downstream wind turbine by means of wind tunnel measurements and the large-eddy simulations (LESs). Fischereit et al. (2022) indicate that the selected wake models accurately represent intra-farm wakes; however, they underestimate the farm–farm wake effects compared with high-fidelity simulations. Troldborg et al. (2022), using LESs, found that the performance of wind turbines in complex terrain is highly variable compared to that in flat homogeneous terrain. Wake models have been validated by various methods; however, a limited number of studies have validated simulated wakes over the complex terrain.

The following studies have investigated the fundamental behavior of wakes over complex terrain. The measurement campaign in a double-ridge site using the meteorological measurement in Perdigo field in 2017 is a well-known observational field experiment over a complex terrain (Wagner

et al., 2019). The wake generated by a single wind turbine at the ridge goes up because a strong recirculation zone forms on the leeward side of the hill (e.g., Berg et al., 2017; Dar et al., 2019; Wenz et al., 2022). Letzger et al. (2022), using numerical simulation, demonstrate that high turbulence flow due to the topography results in asymmetric torque distributions and leads to increased load fluctuations of a wind turbine in a flat plateau downstream of an escarpment. However, Porté-Agel et al. (2020) mention that the combined study of wind turbine wakes and topography still has much room for development. The simulation of wind over complex terrain is still a challenge (Castellani et al., 2015), and the inflow wind speed over complex terrain is unclear (Politis et al., 2011). Yang et al. (2015) show the decrease in wind speed and the increase in the turbulence intensity induced by the upstream trench using several hypothetical wind turbines. Fleming et al. (2019, 2020) demonstrate a 14 % increase in power generation of a downstream wind turbine by applying wake steering to an upstream wind turbine. Sasanuma and Honda (2022, 2024) focus on two onshore wind turbines in complex terrain in northern Japan (Fig. 1) and investigate the wake effects of one turbine on the other. The southwesterly wind results in a significant reduction in wind speed and an increase in turbulence intensity at the downstream wind turbine (Sasanuma and Honda, 2022). Sasanuma and Honda (2024) indicate that wake models generally underestimate the reduction in wind speed in the wakes compared with the observations. Further advancements in the study of the fundamental behavior of wakes over complex terrain are required to evaluate wake effects induced by multiple upstream wind turbines or by entire wind power plants.

A detailed investigation of the bidirectional wakes between two wind turbines is effective. First, we need to compare bidirectional wake effects between the two wind turbines to clarify the differences in wake effects over the complex terrain according to the wind directions. Sasanuma and Honda (2022, 2024) investigate wake effects in a one-way direction between the two wind turbines. Wake effects in the other direction remain unclear. Moreover, we need to look into the dependence of wake effects on inflow wind speed over complex terrain. Second, we need to validate the performance of the wake models by comparing the simulated results with the observed results and by clarifying the dependence of simulated wake effects on inflow wind speed. The validation of simulated wakes over complex terrain is still insufficient. We need to identify similarities and differences among the wake models by comparing the mutual wake effects between wake models.

We investigate the bidirectional wake behavior between two wind turbines over the complex terrain using the SCADA data and validate the performance of wake models in terms of reductions in wind speed at the downstream wind turbine by comparing with the SCADA data. We specifically address the following two issues: (1) identifying the wake effects at the downstream wind turbine by comparing the conditions

with and without the operation of the upstream wind turbine and evaluating the wake effects in terms of reductions in wind speed, turbulence intensity, and power output and (2) demonstrating the differences in the reproducibility of mutual wakes between the two wind turbines using 12 wake models.

Section 2 describes the wind turbines, the SCADA data, the wind condition at the site, the methodology to detect wakes, and the flow simulation with wake models. Section 3 analyses the SCADA data to examine the wake effects and compares the observed results with the results simulated by wake models. Section 4 presents the summary and conclusions.

2 Data and methodology

2.1 Study site and two wind turbines

This study focuses on two wind turbines (WT1 and WT2) located near the northern tip of the Tsugaru Peninsula, Japan (Fig. 1). Because abundant wind resources and steep topography characterize the region near Cape Tappi, this site has been a research site for the operation of wind turbines since the first utility-scale wind farm in Japan was built in 1991 (Fig. 1; e.g., Ushiyama, 1999; Inomata et al., 1999; Enomoto et al., 2001; Fujikawa et al., 2002; Hasegawa et al., 2003). The two wind turbines were originally J82-2.0 models manufactured by Japan Steel Works. To satisfy safety requirements for fatigue strength in this site, their hub height was modified from 80.0 to 65.0 m, and the rated power output was reduced from 2 to 1.675 MW (Fig. 2a). The rotor diameter is 83.3 m. Full operation started in 2010. The two wind turbines are located almost in a southwest–northeast direction (Fig. 1), and the horizontal distance between the two wind turbines is 3.17 times the rotor diameter (264 m; Fig. 2b). WT1 and WT2 are located at an altitude of 132 and 169 m, respectively. The difference in elevation corresponds to 0.44 times the rotor diameter. Along the line connecting the two turbines, WT2 is located at the highest location (Fig. 2b). The surrounding terrain is covered by bush trees (Fig. 2a).

2.2 SCADA data of the two wind turbines

We used 10 min mean SCADA data of the two wind turbines from 5 September 2015 to 31 December 2017. The original data were sampled at an interval of 1 s. The dataset includes wind speed, wind direction, standard deviation of wind speed, nacelle direction, blade pitch angle, rotor speed, and power output. The wind data are measured by a wind vane and a three-cup-type anemometer mounted at the rear of the nacelle. Turbulence intensity is defined as σ/WS , where σ is the standard deviation of wind speed, and WS is the 10 min mean wind speed. To effectively investigate the dependency of the wind turbine wake on wind directions, we used the data with the yaw misalignment, a difference be-

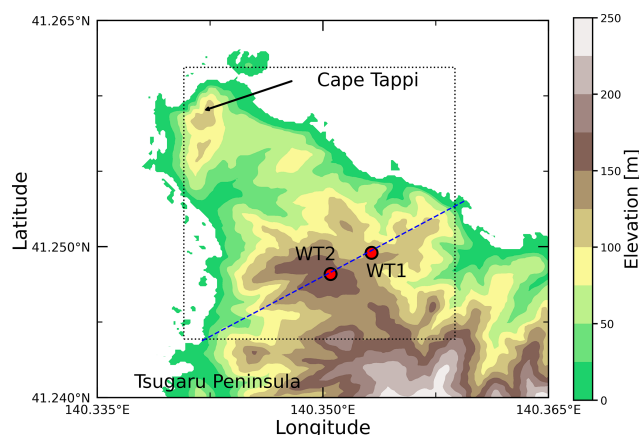


Figure 1. The topography of the study site (color shading) and the locations of the two wind turbines (WT1 and WT2; red circles). The dashed blue line represents the line connecting the two wind turbines to show the vertical topography in Fig. 2b and to analyze the vertical cross-sections in Fig. 14. The square enclosed by the dotted line is a $2\text{ km} \times 2\text{ km}$ computational domain for WAsP CFD.

tween wind direction and nacelle direction, within plus or minus 10° . A total of 80 % of the data satisfy this condition. In the following analyses, we used the SCADA data after applying this selection based on yaw misalignment.

2.3 Wind climate

We present the wind climate at the two wind turbines from the SCADA data (Figs. 3 and 4). The westerly winds and easterly winds commonly dominate at WT1 and WT2 (Fig. 3). Strong westerly winds dominate in winter due to the Siberian high, whereas easterly winds intermittently blow in summer due to the Okhotsk high (Shimada et al., 2014). Westerly winds are stronger than easterly winds, and the wind direction from south-southwest to west-northwest accounts for 70 % at WT2 (Fig. 3a) and 69 % at WT1 (Fig. 3b). Both wind turbines have abundant wind resources with an annual mean wind speed above 8 m s^{-1} . WT2 exhibits higher speeds than WT1 because WT2 is located on top of the hill, and the wind is accelerated on the hill (Fig. 2b; Yamaguchi et al., 2002). The frequency exceeding 15 m s^{-1} amounts to 5 % at WT1 and 14 % at WT2 in all wind directions. The overall results are consistent with the results without data selection based on yaw misalignment (Sasanuma and Honda, 2022, 2024). The wind speeds at WT1 and WT2 show significant correlation (Fig. 4a). Wind speeds at WT2 are 16 % higher than those at WT1. Wind directions at WT1 and WT2 are in good agreement (Fig. 4b). The data are concentrated in the easterly winds ($90\text{--}100^\circ$) and the westerly winds ($220\text{--}260^\circ$), which is consistent with Fig. 3. The wind blowing from WT1 to WT2 accounts for 2 %, and the wind blowing from WT2 to WT1 accounts for 17 %. At these frequencies, wakes are expected to occur. Thus, the locations of the two

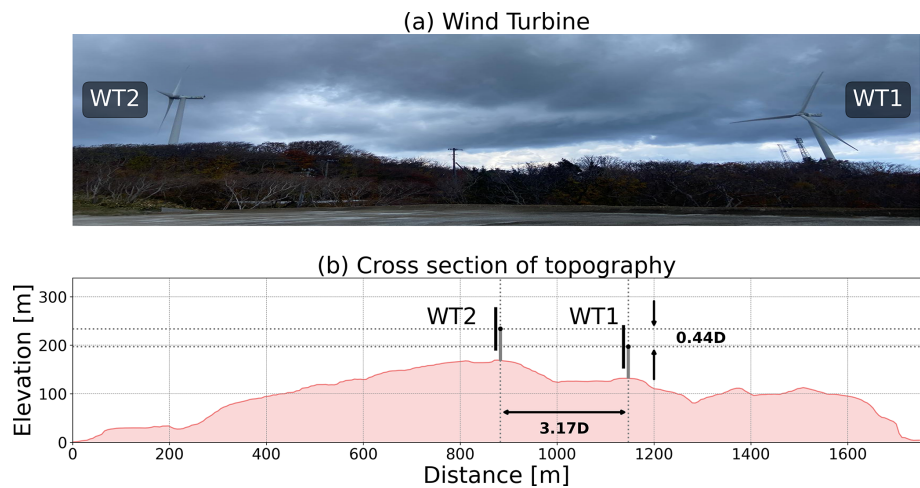


Figure 2. (a) Photo of the two wind turbines. (b) Cross-section of the topography along the line connecting the two wind turbines shown in Fig. 1. The elevation data are obtained from the website of the Geospatial Information Authority of Japan (Geospatial Information Authority of Japan, 2025).

wind turbines are suitable for analyzing mutual wake effects between the wind turbines.

2.4 Detection of wake effects

To assess the wake effects generated by the upstream wind turbine using the SCADA data, we divided the data into two categories based on the operating state of the upstream wind turbine: “no-wake conditions” and “wake conditions” (Sasanuma and Honda, 2022; Sasanuma and Honda, 2024). No-wake conditions are when the upstream wind turbine is not operating, and wake conditions are when the upstream wind turbine is in operation. Sasanuma and Honda (2024) identify the operating states of the upstream wind turbines by means of a combination of rotor speed, blade pitch angle, and power output. We found that we can distinguish whether the wind turbine is operating or not by only the blade pitch angle. The blade pitch angle is 90° when the upstream wind turbine is not operating. By imposing the condition that the blade pitch angle is within ±3°, we can extract data when the upstream wind turbine is in operation below the rated wind speed. The blade pitch angle is 90° when the wind turbine is not operating. When considering wake conditions, we focus on the data with wind speeds ranging from the cut-in wind speed to the rated wind speed. In this range, wake effects are maximized; however, above the rated wind speed, wake effects are reduced by the blade pitch control (e.g., El-Asha et al., 2017; Dilip and Porté-Agel, 2017; Duncan et al., 2020). Thus, by comparing no-wake conditions and wake conditions, we can statistically analyze the influence of wakes generated by the upstream wind turbine on wind speed, turbulence intensity, and power output at the downstream wind turbine.

Table 1. Definition of wind speed ratio according to the wind directions and the presence or absence of wakes. Note that WS_1 and WS_2 in the denominator differ between no-wake conditions and wake conditions. Under no-wake conditions, the denominator represents the wind speed when the upstream wind turbine is not in operation. Under wake conditions, the denominator represents the wind speed when the upstream wind turbine is in operation.

	Northeasterly wind	Southeasterly wind
No-wake conditions	WS_2/WS_1	WS_1/WS_2
Wake conditions	WS_2/WS_1	WS_1/WS_2

2.5 Wind speed ratios

To analyze mutual wake effects between the two wind turbines, we define a wind speed ratio, which is a ratio of the wind speed at the downstream wind turbine to that at the upstream wind turbine. We should notice that the definition of the wind speed ratio between wind speed at WT1 (WS_1) and that at WT2 (WS_2) differs in terms of wind directions. When northeasterly wind blows, the wake induced by WT1 influences WT2. Thus, the wind speed ratio is defined as WS_2/WS_1 . When southwesterly wind blows, the wake induced by WT2 influences WT1. Thus, the wind speed ratio is defined as WS_1/WS_2 . We summarize the wind speed ratios in no-wake conditions and in wake conditions for the respective northeasterly wind and southwesterly wind in Table 1. We compare the wind speed ratios between no-wake conditions and wake conditions for northeasterly wind and southwesterly wind to evaluate the wake effects in the following analyses.

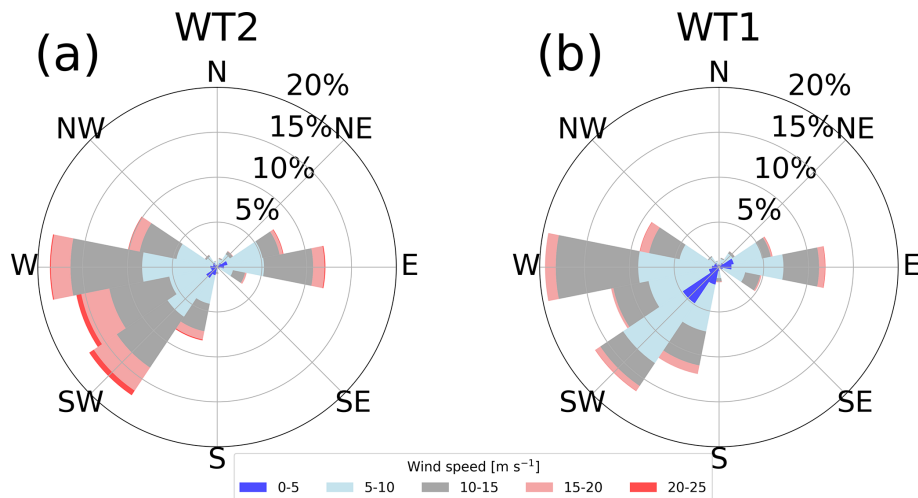


Figure 3. Wind roses derived from the SCADA data of (a) WT2 and (b) WT1. The different colors are used every 5 m s^{-1} . Wind direction is defined as the direction from which the wind blows.

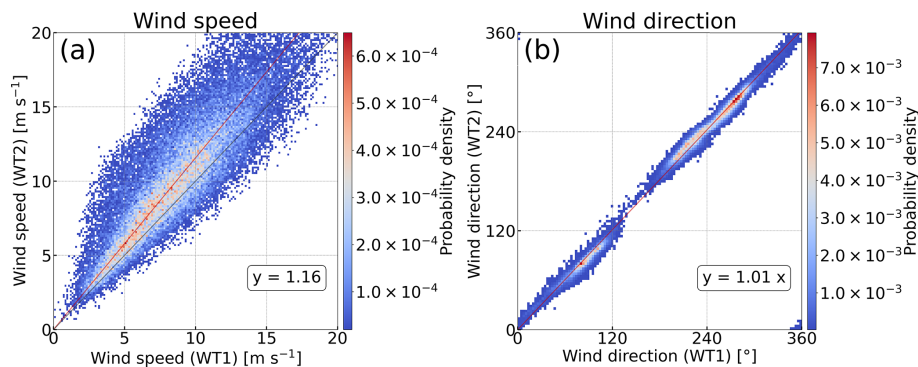


Figure 4. Scatterplots of (a) wind speed and (b) wind direction between WT1 and WT2 from the SCADA data. The color represents the data density. The red lines in (a) and (b) are the linear regression lines, shown by the equations in the figures. The black line in (a) represents a 1 : 1 line.

2.6 Flow simulations with wake models

We utilized Wind Atlas Analysis and Application Program Computational Fluid Dynamics (WAsP CFD; Bechmann, 2012) in combination with PyWake (Pedersen et al., 2023) to closely examine the observed wind and wakes over complex terrain. WAsP CFD constitutes a CFD model integrated into WAsP, designed for simulating winds over complex terrain. The model is based on Ellipsys 3D code, which is a multi-block finite-volume discretization of incompressible Reynolds-averaged Navier–Stokes (RANS) equations. The two-equation k - ε RANS model by Launder and Spalding (1974) is used for turbulence. Simulations are conducted under the assumption of a neutral atmospheric stability. Coriolis forcing is neglected. The validity of WAsP CFD in complex terrain has been demonstrated (e.g., Bechmann et al., 2011; Troen and Hansen, 2015; Bechmann, 2016; Sharma et al., 2020). We used WAsP CFD for evaluating the influence of topography on wind flow. The computational domain is

shown in Fig. 1. The horizontal calculations were conducted at 90 m intervals, and the elevation map is spaced at 5 m intervals (Geospatial Information Authority of Japan, 2025). The output data are at 13 vertical levels from 5 to 300 m (5, 10, 20, 33, 48, 65, 80, 100, 120, 150, 200, 250, and 300 m) in every 5° bin of wind direction. The upper boundary of the computational domain is 7000 m. We set the inflow wind speed far upwind to 10 m s^{-1} at 100 m height, and the roughness length is assumed to be 0.0032 m, corresponding to the sea surface. Therefore, the inflow wind speed has a slightly sheared profile. WAsP CFD uses the roughness length depending on the landscape type. The roughness length in the study area ranges from 0 to 1.5 m.

PyWake is an open-source wind farm simulation tool written in Python. This tool simulates the flow with wind turbines by incorporating wake models. PyWake has 12 wake models (Appendix A): 11 engineering wake models and a linearized RANS wake model (Fuga). Note that we used the default parameter values of the 12 wake models without adjusting the

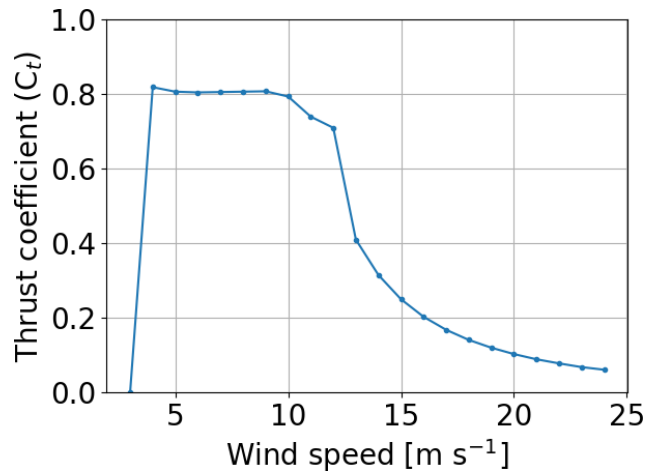


Figure 5. Thrust coefficient as a function of wind speed from V80 wind turbine.

parameters to obtain the results close to the SCADA data. The sensitivity analysis of the model parameters is beyond the scope of this study. The Bastankhah model and Turbo-Gaussian model, which we particularly focus on, have a reduction in wind speed with a Gaussian profile (Bastankhah and Porté-Agel, 2014; Pedersen et al., 2022). They have been validated for onshore fields (e.g., Jeon et al., 2015; Ruisi and Bossanyi, 2019; Fleming et al., 2020; zum Berge et al., 2024) and offshore fields (Farrell et al., 2021; Fischereit et al., 2022; Centurelli et al., 2024). The turbulence intensity is set to 0.2 in PyWake. We used the thrust coefficient curve of the V80 2 MW wind turbine because the rated power output of this wind turbine is closest to that of the wind turbines in this study among the wind turbine models available in PyWake. The thrust coefficient curve of the V80 is shown in Fig. 5. In this study, we discuss similarities and differences among the 12 wake models for mutual wind directions when a typical thrust coefficient curve is used.

3 Results

3.1 Observational results

We examine the wind speed ratios to evaluate wake effects caused by the upstream wind turbine. Figure 6 shows wind speed ratios between the two wind turbines before we divided the data into two categories on the basis of the operating state of the upstream wind turbine. Variations in the wind speed ratio with wind direction are caused by the surrounding terrain and turbine wakes. The wind speed ratios are generally above 1.0 in Fig. 6a and below 1.0 in Fig. 6b, whereas we can identify V-shaped curves or significant reductions in wind speed ratios at around 40° and 225° (light-blue shading in Fig. 6a and b). These wind directions correspond approximately to the direction of the line connecting the two wind turbines (Fig. 1). The ranges of these significant reductions in

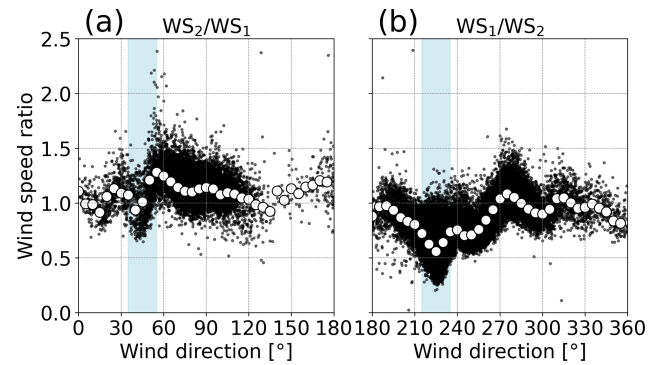


Figure 6. Wind speed ratios as a function of wind direction. Black dots denote 10 min mean data, and white circles denote median values in every 5° bin. In (a) and (b), wind directions at WT2 are commonly used for horizontal axes. Note that the definition of the wind speed ratio differs between (a) and (b). In (a), the wind speed ratio is defined as the ratio of wind speed at WT2 (WS_2) to that at WT1 (WS_1). In (b), the wind speed ratio is defined as the ratio of WS_1 to WS_2 . These definitions of the wind speed ratio are common in the following analyses. Light-blue shading indicates the ranges of wind directions with wake effects for (a) $45^\circ \pm 10^\circ$ and (b) $225^\circ \pm 10^\circ$.

wind speed ratio are approximately $\pm 10^\circ$ on both sides of the wind directions. We can see no other significant reduction in the remaining wind direction ranges. We focus on these two wind directions in the following analyses.

To clearly elucidate wake effects from the results of Fig. 6, we divide the data by the operating state of the upstream wind turbine. The condition of blade pitch angle is applied, and, resultantly, the data with wind speeds higher than the rated wind speed are excluded. We compare the wind speed ratio between no-wake conditions and wake conditions, with a focus on the V-shaped curves at around $45^\circ \pm 10^\circ$ and $225^\circ \pm 10^\circ$ (Fig. 7). For northeasterly wind, the plots show no V-shaped curve and remain generally constant under no-wake conditions (Fig. 7a). The wind speed ratios are higher than 1.0, with a median value of 1.18 at 45° , and this means that the wind speeds at downstream WT2 are higher than those at upstream WT1. Under wake conditions, we can see a significant reduction in wind speed ratio due to the wake of WT1, with a maximum reduction of 23 % for a wind direction of 45° (Fig. 7b). For southwesterly wind, as is the case with Fig. 7a, the plots show no V-shaped curve and an almost constant wind speed ratio under no-wake conditions (Fig. 7c). The median value of wind speed ratio is 0.87 at 225° . The wind decelerates from the location of WT2 to the location of WT1 even without wakes generated by WT2 because WT1 is located behind the hill. Under wake conditions, wind speed ratio decreases to 0.47 from 0.87 under no-wake conditions at 225° , and this means a 46 % reduction (Fig. 7d). This reduction observed for southwesterly wind is greater than that observed for northeasterly winds. This reduction for southwesterly wind is 22 % larger than that derived by

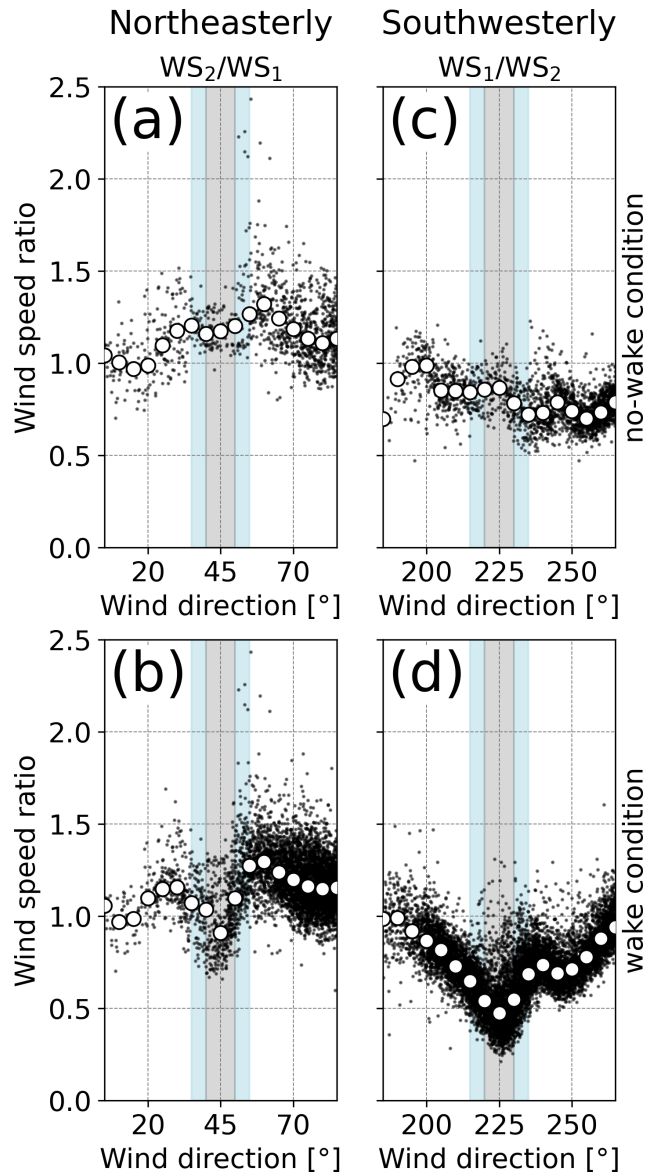


Figure 7. The same as in Fig. 6 but for being classified by the operating state of the upstream wind turbine under (a, c) no-wake conditions and (b, d) wake conditions for (a, b) northeasterly wind and (c, d) southwesterly wind. Light-blue and gray shadings indicate the range of the wind direction with wake effects. The gray shading in the ranges of (a, b) $45^\circ \pm 5^\circ$ and (c, d) $225^\circ \pm 5^\circ$ represents the focused ranges of wind direction for the analyses in Figs. 8, 9, and 10.

Sasanuma and Honda (2022) because they use the mean values rather than the median values. From the above results, we find that the operation of the upstream wind turbine causes a wind speed reduction at the downstream wind turbine and that the wake effect on the downhill side for southwesterly wind is more pronounced than that on the uphill side for northeasterly wind.

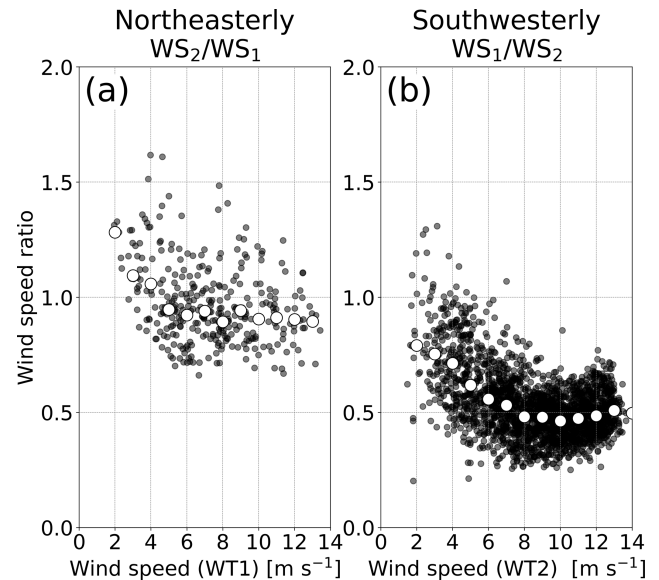


Figure 8. Wind speed ratio as a function of wind speed at the upstream wind turbine in operation for (a) northeasterly wind and (b) southwesterly wind. Black dots denote 10 min mean data, and white circles denote median values in every 1 m s^{-1} bin. The data are extracted from the focused ranges of wind direction, denoted by the gray shading in Fig. 7b and d.

We examine the dependence of the magnitude of the reduction in wind speed on inflow wind speed under wake conditions (Fig. 8). To examine the maximum wake effects, we focus on the ranges of wind direction for $45^\circ \pm 5^\circ$ and $225^\circ \pm 5^\circ$ (gray shading in Fig. 7b and d). We use the wind speed of the upstream wind turbine in operation as the inflow wind speed on the horizontal axis. Figure 8 clearly shows the relationship between the inflow wind speed and the wind speed ratio for both northeasterly and southwesterly winds. The decrease in wind speed ratio means an increase in wake effect or a reduction in wind speed at the downstream wind turbine. For northeasterly wind, the wind speed ratio decreases as the inflow wind speed increases below a wind speed of 6 m s^{-1} , whereas, above 6 m s^{-1} , the wind speed ratio remains almost constant (Fig. 8a). For southwesterly wind, the wind speed ratio decreases with inflow wind speed and reaches a minimum at 10 m s^{-1} (Fig. 8b). The gradual increase for inflow wind speeds above 10 m s^{-1} suggests a start of control of the blade pitch angle. Thus, the wind turbine extracts the kinetic energy significantly from the wind below the rated wind speed, and the resulting momentum loss in the downstream induces the maximum wake effects. These results are consistent with those of Rhodes and Lundquist (2013), showing that the maximum reduction in wind speed occurs below the rated wind speed.

We investigate the wake effects on the turbulence intensity at the downstream wind turbine by comparing the observed turbulence intensity with the standard curves of turbulence

intensity defined by the International Electrotechnical Commission (IEC, 2019). Two categories of the standard curves are given by the following equations. WS is wind speed.

$$\text{Turbulence intensity}_{\text{category A}} = 0.16 (0.75 + 5.6/\text{WS}) \quad (1)$$

$$\text{Turbulence intensity}_{\text{category A}^+} = 0.18 (0.75 + 5.6/\text{WS}) \quad (2)$$

For northeasterly wind, the 90th-percentile values of turbulence intensity hardly exceed the line of the A+ category under both no-wake conditions and wake conditions (Fig. 9a and b). The wakes generated by WT1 contribute little to the increase in turbulence intensity at WT2. For southwesterly wind, the 90th-percentile values of turbulence intensity for wind speeds greater than 7 m s^{-1} follow the line of the A+ category under no-wake conditions (Fig. 9c; Sasanuma and Honda, 2022). Under wake conditions, wind speed at WT1 decreases to less than 10 m s^{-1} due to the wake generated by WT2, and the 90th-percentile values of turbulence intensity follow the lines of the A+ category and A category (Fig. 9d). However, the 10 min mean data of turbulence intensity above the 90th percentile significantly exceed the line of the A+ category. The 10 min mean data of turbulence intensity exceed 0.3 for wind speeds less than 6 m s^{-1} . This is a noticeable difference between no-wake conditions and wake conditions. These results suggest that the wake effects on the turbulence intensity vary significantly depending on the wind directions.

The impact of the wake on the power output of the downstream wind turbine is examined within the ranges of wind direction of $45^\circ \pm 5^\circ$ and $225^\circ \pm 5^\circ$ (Fig. 10). Note that the horizontal axis in Fig. 10 represents wind speed at the upstream wind turbine to examine the reduced power output at the downstream wind turbine compared with the power output at the upstream wind turbine. For northeasterly wind, the power output at the downstream wind turbine WT2 is lower than that expected from the wind speed at the upstream wind turbine WT1 (Fig. 10a and b). For example, under no-wake conditions, the normalized power output is approximately 0.5 at a wind speed of 8 m s^{-1} (Fig. 10a). Under wake conditions, a wind speed of 9 m s^{-1} or a 12.5 % increase in wind speed at the downstream wind turbine is required to generate the same power output (Fig. 10b). For southwesterly wind, the power output at the downstream wind turbine WT1 decreases more significantly than that expected from the wind speed at the upstream wind turbine WT2 (Fig. 10c and d). For instance, the normalized power output is approximately 0.2 at 7 m s^{-1} under no-wake conditions (Fig. 10c). Under wake conditions, a wind speed of 12 m s^{-1} or a 71 % increase in wind speed is required to generate the same power output (Fig. 10d). At 14 m s^{-1} , the normalized power output under no-wake conditions is approximately 0.9 (Fig. 10c), whereas it decreases to approximately 0.3 under wake conditions (Fig. 10d). This result represents a 67 % reduction in power output if the inflow wind speed at the downstream wind turbine is assumed to be identical to that at the upstream

wind turbine. These findings suggest that the wake effects have a more pronounced impact on power output for southwesterly wind than for northeasterly wind. Even when the same wind speed is observed at the upstream wind turbine for northeasterly wind and southwesterly wind, the degree of reduction in wind speed or the resulting power output at the downstream wind turbine is different depending on the installation conditions of wind turbines.

3.2 Simulated wake and wind flow

We validate the performance of 12 wake models in PyWake by comparing the wind speed ratios computed from the wake models with those from the SCADA data. We show the comparison results of wind speed ratio for different inflow wind speeds computed by WAsP CFD and a typical wake model, the TurboGaussian wake model for northeasterly and southwesterly winds (Fig. 11). The wind speed ratio decreases significantly with a decrease in the inflow wind speed in the ranges of wind direction with wake effects for both northeasterly wind and southwesterly wind. This means that a significant reduction in wind speed ratio occurs when the inflow wind speed is small. The magnitudes of reduction in wind speed ratio are the same for wind speeds below 9 m s^{-1} for northeasterly wind (Fig. 11a) and below 8 m s^{-1} for southwesterly wind (Fig. 11b), resulting from the thrust coefficient curve used for the wake model (Fig. 5). The wake model shows the results close to the SCADA data at an inflow wind speed of 13 m s^{-1} for northeasterly wind and at an inflow wind speed of less than 8 m s^{-1} for southwesterly wind. The model results overestimate the reduction in wind speed for northeasterly wind and underestimate it for southwesterly wind, which is generally consistent with the results of other wake models (Figs. B1 and B2 in the Appendix). We can conclude that the topographic effects cause an opposite change in wake reproduction between northeasterly and southwesterly winds.

We compare the wind speed ratios derived from the 12 wake models at the inflow wind speeds at 13 m s^{-1} for northeasterly wind and 8 m s^{-1} for southwesterly wind (Fig. 12). For both northeasterly wind and southwesterly wind, most of the wake models underestimate the reduction in wind speed and represent weak wakes (Fig. 12a and b). For northeasterly wind, most of the wake models hardly represent the wakes (Fig. 12a), whereas, for southwesterly wind, all of the wake models except the GCL wake model represent a reduction in wind speed ratio (Fig. 12b). Only the Bastankhah and the TurboGaussian wake models closely represent the minimum value of wind speed ratio derived from the SCADA data for both northeasterly wind and southwesterly wind. To summarize the validation results from each wake model, we show the wind speed ratio for 12 wake models for wind directions with a maximum reduction in wind speed ratio for both northeasterly and southwesterly winds in Fig. 13. The order of the wake models according to the difference

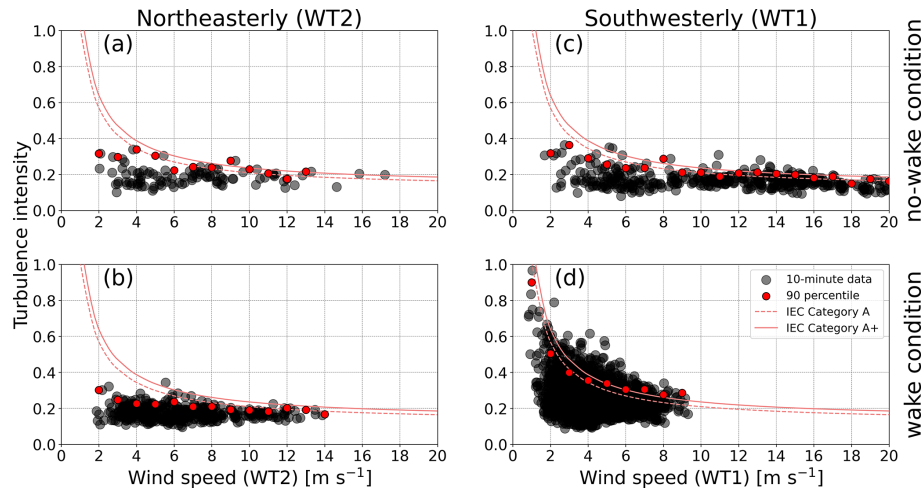


Figure 9. Turbulence intensity as a function of wind speed at the downstream wind turbine under (a, c) no-wake conditions and (b, d) wake conditions for (a, b) northeasterly wind and (c, d) southwesterly wind. The horizontal axis represents wind speed at the downstream wind turbine WS_2 in (a) and (b) and at WS_1 in (c) and (d). Black dots denote 10 min mean data, and red circles denote 90th-percentile values in every 1 m s^{-1} bin. The dashed red lines indicate standard curves of the International Electrotechnical Commission (IEC) category A for high turbulence, as shown in Eq. (1), and the solid red lines indicate standard curves of the IEC category A+ for very high turbulence, as shown in Eq. (2). The data are extracted from the focused ranges of wind direction, denoted by the gray shading in Fig. 7.

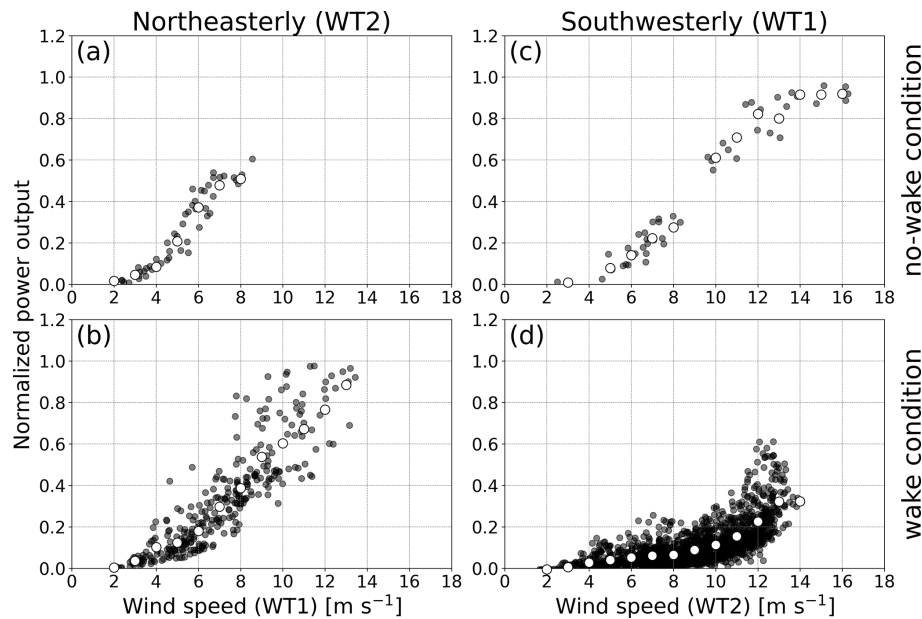


Figure 10. Normalized power output as a function of wind speed at the upstream wind turbine under (a, c) no-wake conditions and (b, d) wake conditions for (a, b) northeasterly wind and (c, d) southwesterly wind. The normalized power output in the vertical axis represents power output divided by the rated power output. The horizontal axis represents wind speed at the upstream wind turbine WS_1 in (a) and (b) and WS_2 in (c) and (d). Black dots denote 10 min mean data, and white circles denote median values in every 1 m s^{-1} bin. The data are extracted from the focused ranges of wind direction, denoted by the gray shading in Fig. 7.

of the results between each wake model and the SCADA data is almost the same for northeasterly and southwesterly winds (Fig. 13a and b). The results from the TurboGaussian and the Bastankhah wake models are consistent with those from the SCADA data, followed by the Blondel2020 and

the Blondel2023 wake models for northeasterly and southwesterly winds. The differences from the SCADA data range from 0.001 to 0.151 for northeasterly wind and from 0.032 to 0.323 for southwesterly wind. The differences among the

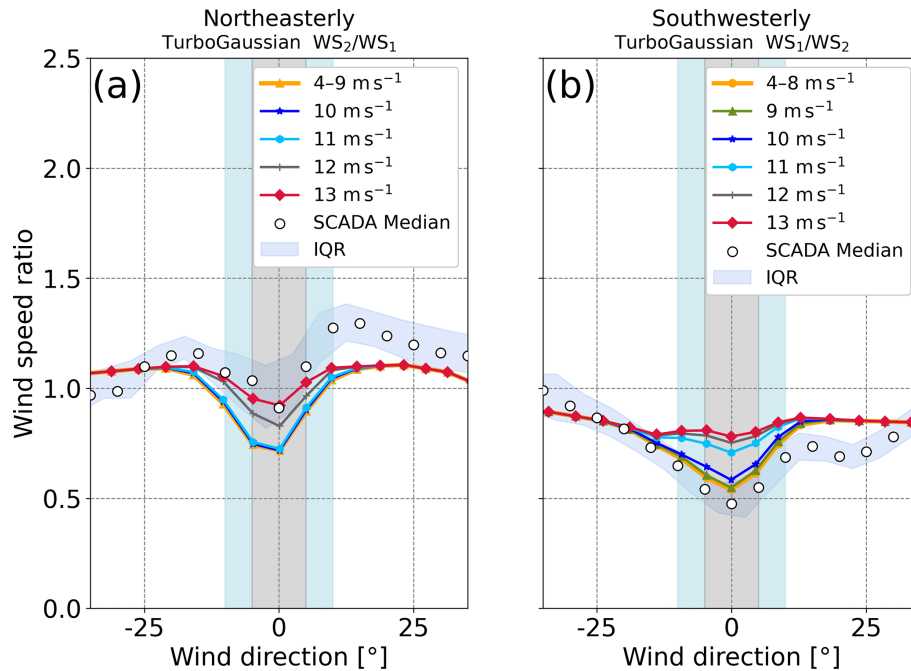


Figure 11. Wind speed ratio as a function of wind direction for (a) northeasterly wind and (b) southwesterly wind. Colored lines are results derived from the TurboGaussian wake model for inflow wind speeds ranging from 4 to 13 m s^{-1} at an interval of 1 m s^{-1} . The results for (a) $4\text{--}9 \text{ m s}^{-1}$ and (b) $4\text{--}8 \text{ m s}^{-1}$ are shown by one line because the differences are negligible. The horizontal axis indicates differences in wind direction, with the minimum wind speed ratio at 0° for both the SCADA data and the results of the wake model. The blue band denotes the interquartile range (IQR) of the SCADA data, and white circles denote median values in every 5° bin. Light-blue and gray shadings indicate the ranges of wind directions with wake effects.

wake models are more prominent for southwesterly wind than for northeasterly wind.

To investigate the different wake effects between northeasterly and southwesterly winds, we show vertical structures of wind as computed by WASP CFD and PyWake along the line connecting the two wind turbines (Fig. 14). We computed wind flows with and without the wake effects with a far-upstream wind speed of 10 m s^{-1} and derived the reduction in horizontal wind speed due to the wakes. In Fig. 14b and d, the TurboGaussian wake model is used. We can consider the path of the wakes generated by the upstream wind turbine from the streamline passing through the center of the wind turbine wakes (Sessarego et al., 2020). For northeasterly wind, the wind reaches the hub height of WT2 from the hub height of WT1 due to the wind ascending the hill (Fig. 14a). Moreover, the flow accelerates over the top of the hill around the location of WT2, and the accelerated wind blows through the rotor surface of WT2. When the wind turbines are installed and operating, the Gaussian-shaped wake generated by WT1 rises upward along the terrain and reaches the center of the rotor of WT2 (Fig. 14b). However, the wake weakens at WT2 because the flow accelerates over the top of the hill. Thus, the wind speed ratios are generally higher than 1.0 due to the acceleration of wind speed over the hill under no-wake conditions (Fig. 7a), and the wind speed ra-

tios decrease slightly because the wake is weakened by the flow acceleration under wake conditions (Fig. 7b). For southwesterly wind, the weak winds in the lee of the hill of WT2 cover the location of WT1 and extend through the height of the lower part of the WT1 rotor (Fig. 14c). In contrast, the strong winds over the top of the hill reach the hub height of WT1. The resulting strong vertical wind shear across the rotor of WT1 contributes to the increase in turbulence. When the wind turbines are installed and operating, the wake generated by WT2 extends horizontally through the upper part of the rotor of WT1 (Fig. 14d). The wake does not follow the terrain slope in the lee of the hill, which is consistent with the previous studies (Berg et al., 2017; Dar et al., 2019; Wenz et al., 2022). Thus, the wind speed ratios under no-wake conditions are generally lower than 1.0 due to the acceleration of wind over the hill and the weak winds in the lee of the hill (Fig. 7c). The wind speed ratios decrease further under wake conditions due to the inclusion of the wake extending from the upstream wind turbine (Fig. 7d).

From the results obtained so far, we consider the differences among the 12 wake models. The degree of wake reproducibility depends on inflow wind speed (Figs. 11, B1, and B2). Terrain effects induce a systematic bias in the reproducibility of wakes (Figs. 11, 12, 13, B1, and B2). From the perspective of wake structure, the differences among the

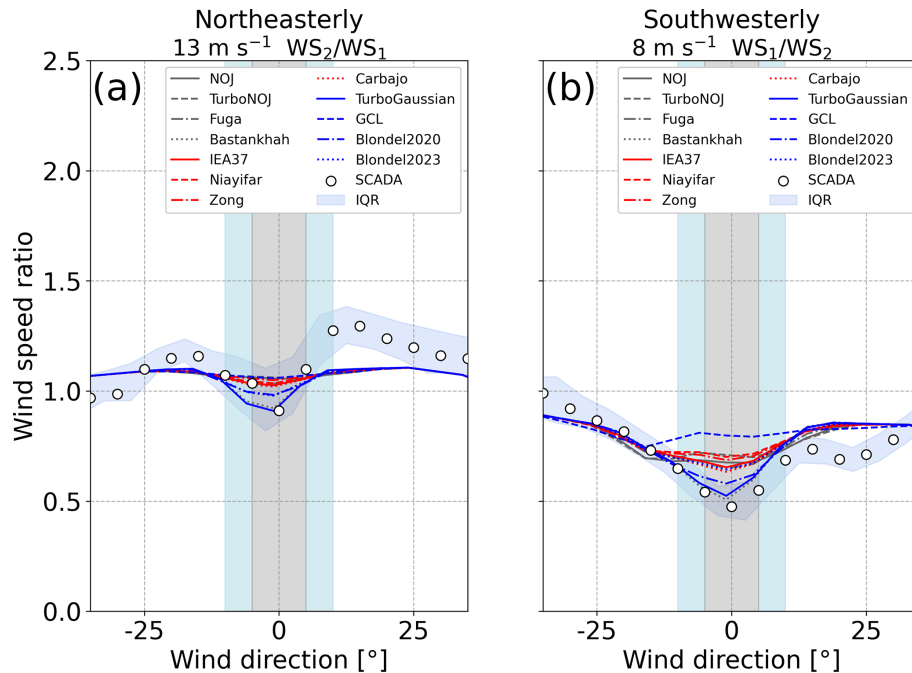


Figure 12. Wind speed ratio as a function of wind direction for (a) northeasterly wind and (b) southwesterly wind. Colored lines are results derived from 12 wake models at an inflow wind speed of (a) 13 m s^{-1} and (b) 8 m s^{-1} . The horizontal axis indicates differences in wind direction, with the minimum wind speed ratio at 0° for both the SCADA data and the results of the wake models. The blue band denotes the interquartile range (IQR) of the SCADA data, and white circles denote median values in every 5° bin. Light-blue and gray shadings indicate the ranges of wind direction with wake effects.

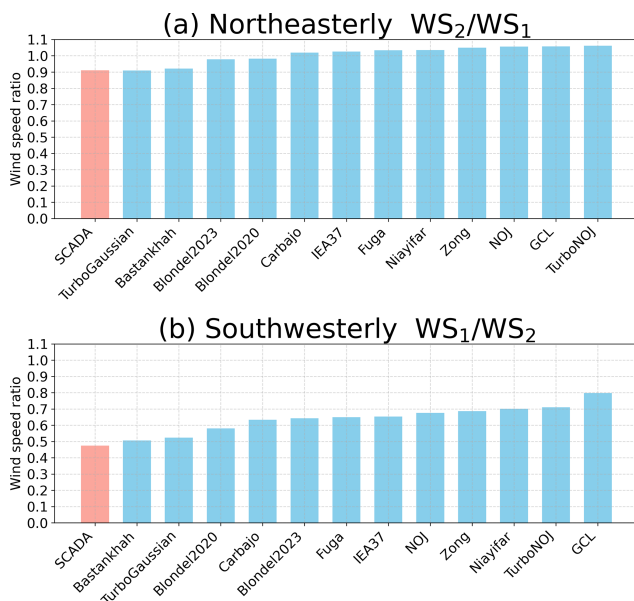


Figure 13. Wind speed ratio derived from the SCADA data and 12 wake models for wind direction with maximum wake effects at wind speeds of (a) 13 m s^{-1} for northeasterly wind and of (b) 8 m s^{-1} for southwesterly wind.

12 wake models lie in the downstream extents of the wakes and the magnitude of the wind speed reduction immediately behind the wind turbine (Figs. 14, C1, and C2). In particular, the downstream extents of the wakes are key for obtaining results consistent with the SCADA observations. Although the simulation results might depend on parameter settings of the wake models, the present results suggest that the major differences arise from the model formulation. These results highlight the importance of selecting appropriate wake models and considering topographic conditions.

4 Summary and conclusions

We have investigated the bidirectional wake effects between the two wind turbines in complex terrain at a site in northern Japan using the SCADA data and validated the performance of the wake models. We have addressed the following two issues: (1) identifying the wake effects generated by the upstream wind turbine for northeasterly and southwesterly winds in terms of wind speed ratio, turbulence intensity, and power output at the downstream wind turbine and (2) validating the performance of the 12 wake models and the impacts of the topography on the simulated wakes. The main results are summarized as follows.

1. Using the SCADA data, we detected wake effects from the differences in the wind speed ratio between no-wake

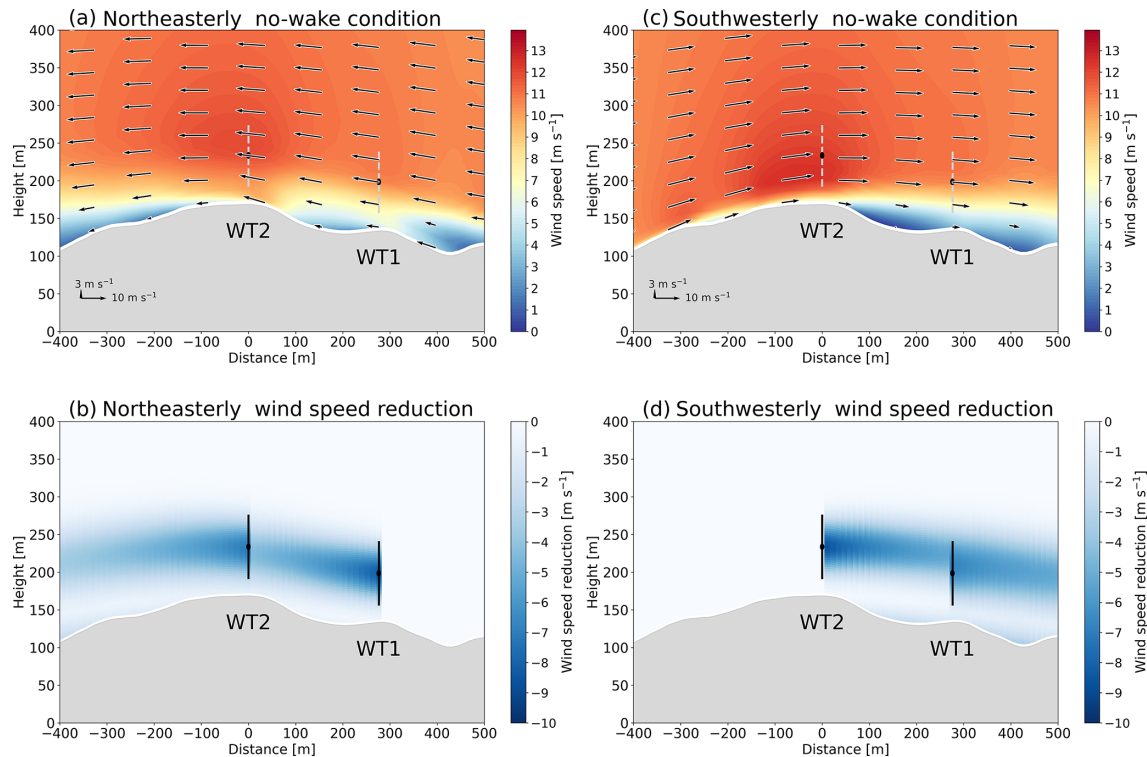


Figure 14. Vertical cross-sections along the dashed blue line in Fig. 1 for **(a, b)** northeasterly wind and **(c, d)** southwesterly wind with a far-upstream wind speed of 10 m s^{-1} . In **(a)** and **(c)**, we show horizontal wind speed (color shading) and wind vectors on the cross-section under no-wake conditions, although we show the positions of the wind turbine rotors by means of a dashed gray line. In **(b)** and **(d)**, we show a reduction in horizontal wind speed (color shading) due to the wind turbine wake simulated by the TurboGaussian wake model. A reduction in horizontal wind speed is the difference between no-wake conditions and wake conditions. The black lines indicate the positions of the wind turbine rotors. The data from WAsP CFD are available from 5 m above ground level.

conditions and wake conditions. These conditions are classified by the operating state of the upstream wind turbine based on the blade pitch angle. The upstream wind turbine, in the operating state, reduces wind speed at the downstream wind turbine for both northeasterly and southwesterly winds. For northeasterly wind, the wind speed ratio under no-wake conditions generally exceeds 1.0, and the maximum reduction in wind speed ratio due to the wake is 23 %. For southwesterly wind, the wind speed ratio under no-wake conditions is generally below 1.0, and the maximum reduction in wind speed ratio due to the wake is 46 %. Wake effects are enhanced more for southwesterly wind than for northeasterly wind. Wake effects reach their maximum below the rated wind speed for both northeasterly and southwesterly winds. Turbulence intensity at the downstream wind turbine increases due to the wake generated by the upstream wind turbine for southwesterly wind, and the 10 min data of the turbulence intensity exceed the level of the A+ category. The power output at the downstream wind turbine for southwesterly wind decreases more significantly than for northeasterly wind. From the analysis of the SCADA data, this study demonstrated

that wake effects depend on the surrounding terrain and inflow wind speed. These results indicate the importance of considering the combined effects of wakes and topography.

2. We compared the wind speed ratios derived from 12 wake models in PyWake with those from the SCADA data. The wind speed ratios derived from the wake models show strong dependence on the inflow wind speed. This dependence reflects the thrust coefficient curve used for wake computation in the wake models. The wake models commonly overestimate the reduction in wind speed ratio for northeasterly wind and underestimate it for southwesterly wind. We can conclude that the topographic effects cause an opposite change in the simulated wakes compared to the SCADA data. The wake models with high reproducibility are the TurboGaussian and the Bastankhah wake models. These two wake models represent the minimum wind speed ratio or the maximum reduction in wind speed close to the observations when inflow wind speeds are 13 m s^{-1} for northeasterly wind and 8 m s^{-1} for southwesterly wind. Then, we examined the wind field by means of WAsP

CFD and the wake models in PyWake. For northeasterly wind, the wake effects weaken at the downstream wind turbine due to the acceleration of wind over the top of the hill. For southwesterly wind, the wind speed at the downstream wind turbine decreases significantly because of the weak winds in the lee of the hill and the wake extending horizontally to the downstream wind turbine from the upstream wind turbine. From the simulation results, this study demonstrated that the downstream extents of the wakes are key for obtaining results consistent with the SCADA observations. These results indicate the importance of considering the selection of wake models and topographic conditions.

By analyzing the SCADA data, this study reveals the fundamental characteristics of bidirectional wake effects over complex terrain. The SCADA data have the potential to provide much information on wakes. The method used for detecting wake effects in this study demonstrates the potential to utilize the SCADA data collected during the downtime of wind turbines due to maintenance and curtailment. Although this study focuses on onshore wind turbines, the findings provide important suggestions for offshore wind turbines near the coast influenced by terrain effects and for wind power plants subject to multiple wake interactions.

Furthermore, we need to investigate the following aspects. First, examining the impacts of atmospheric stability on wind turbine wakes is a challenge. In the study area, northeasterly wind dominates in summer, and southwesterly wind dominates in winter (Sasanuma and Honda, 2020). That is, dominant winds and stability conditions might typically be fixed to the seasons. Several studies have investigated atmospheric stability effects on wakes using numerical simulations (Uchida and Takakuwa, 2019; Yamaguchi et al., 2024) and observations (Oqaily et al., 2025). Uchida and Takakuwa (2019) show that the wind turbine wakes on the top of the hill follow the terrain under stable atmospheric conditions, whereas the wake rises on the lee side under neutral atmospheric conditions. Therefore, the extent of the wake effect depends not only on the terrain but also on the atmospheric stability. Then, increased turbulence intensity owing to wakes increases the risks of fatigue loads and shortens the lifespan of wind turbines. We have a plan to quantitatively evaluate the fatigue loads and fatigue lifetime at the downstream wind turbine by using aeroelastic simulation. Insights into the risks of the downstream wind turbine will be valuable for the operation and control of wind power plants.

Appendix A: List of the 12 wake models

We present the 12 wake models used in this study in Table A1.

Table A1. Abbreviations and full names for the 12 wake models in PyWake.

Abbreviation	Full name	Reference
NOJ	NOJDeficit	Jensen (1983)
TurboNOJ	TurboNOJDeficit	Nygaard et al. (2020)
Fuga	FugaDeficit	Ott et al. (2011)
Bastankhah	BastankhahGaussianDeficit	Bastankhah and Porté-Agel (2014)
IEA37	IEA37SimpleBastankhahGaussianDeficit	Bastankhah and Porté-Agel (2016)
Niayifar	NiayifarGaussianDeficit	Niayifar and Porté-Agel (2016)
Zong	ZongGaussianDeficit	Zong and Porté-Agel (2020)
Carbajofuertes	CarbajofuertesGaussianDeficit	Carbajo Fuertes et al. (2018)
TurboGaussian	TurboGaussianDeficit	Nygaard et al. (2020)
GCL	GCLDeficit	Larsen (2009)
Blondel2020	BlondelSuperGaussianDeficit2020	Blondel and Cathelain (2020)
Blondel2023	BlondelSuperGaussianDeficit2023	Blondel (2023)

Appendix B: Wind speed ratio simulated by the 12 wake models

We show the results of wind speed ratio using the 12 wake models for northeasterly wind and southwesterly wind (Figs. B1 and B2). The horizontal axis indicates differences in wind direction, with the minimum wind speed ratio at 0° for both the SCADA data and the results of the wake models. For northeasterly wind, the wake models shown in Fig. B1d, e, h, i, k, and l commonly represent the wake well and overestimate the reduction in wind speed ratio at low wind speeds (Fig. B1d, e, h, i, k, and l). For southwesterly wind, most of the wake models underestimate the reduction in wind speed ratio. Only the Bastankhah wake model (Fig. B2d) and the TurboGaussian wake model (Fig. B2i) show the closest results of the SCADA data below 10 m s⁻¹.

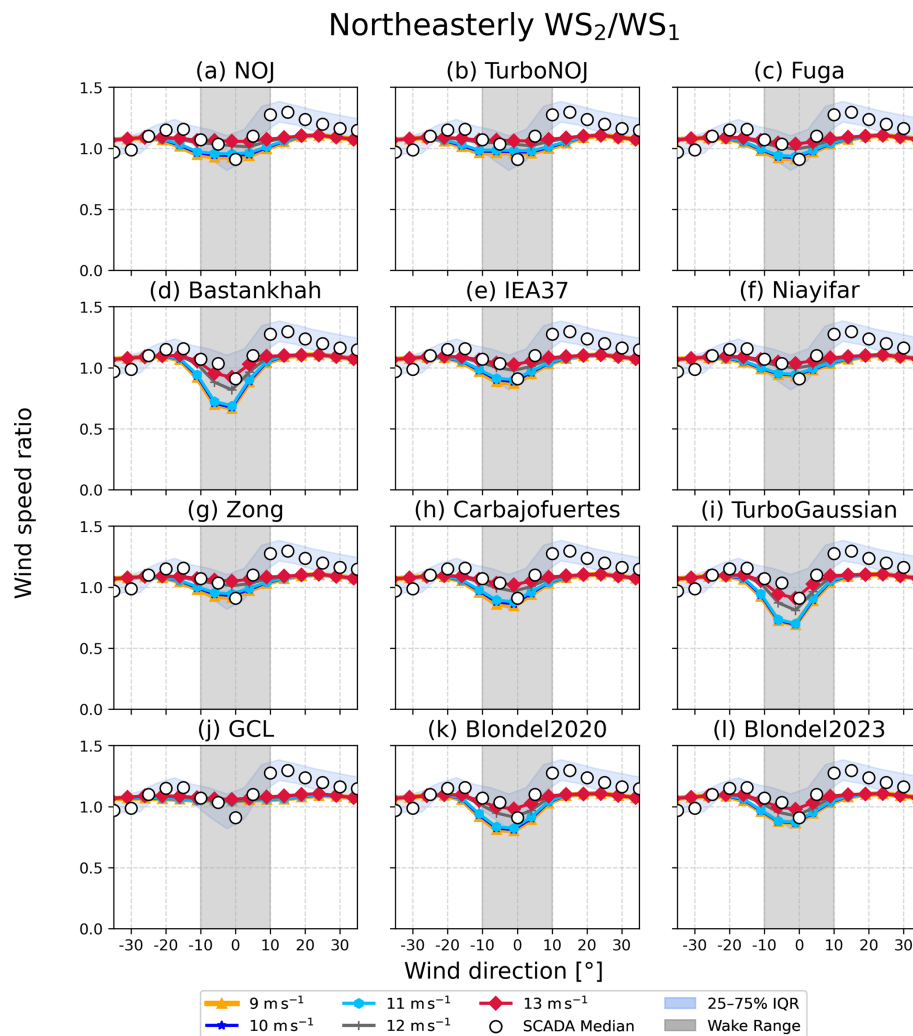


Figure B1. Wind speed ratio derived from the 12 wake models for northeasterly wind. Colored lines are results derived from each wake model for every 1 m s^{-1} , ranging from 4 to 13 m s^{-1} . The results ranging from 4 to 9 m s^{-1} are shown by one line. The horizontal axis indicates differences in wind direction, with the minimum wind speed ratio at 0° for both the SCADA data and the results of the wake models. The blue band denotes the interquartile range (IQR) of the SCADA data, and white circles denote median values in every 5° bin. Gray shading indicates the ranges of wind directions with wake effects.

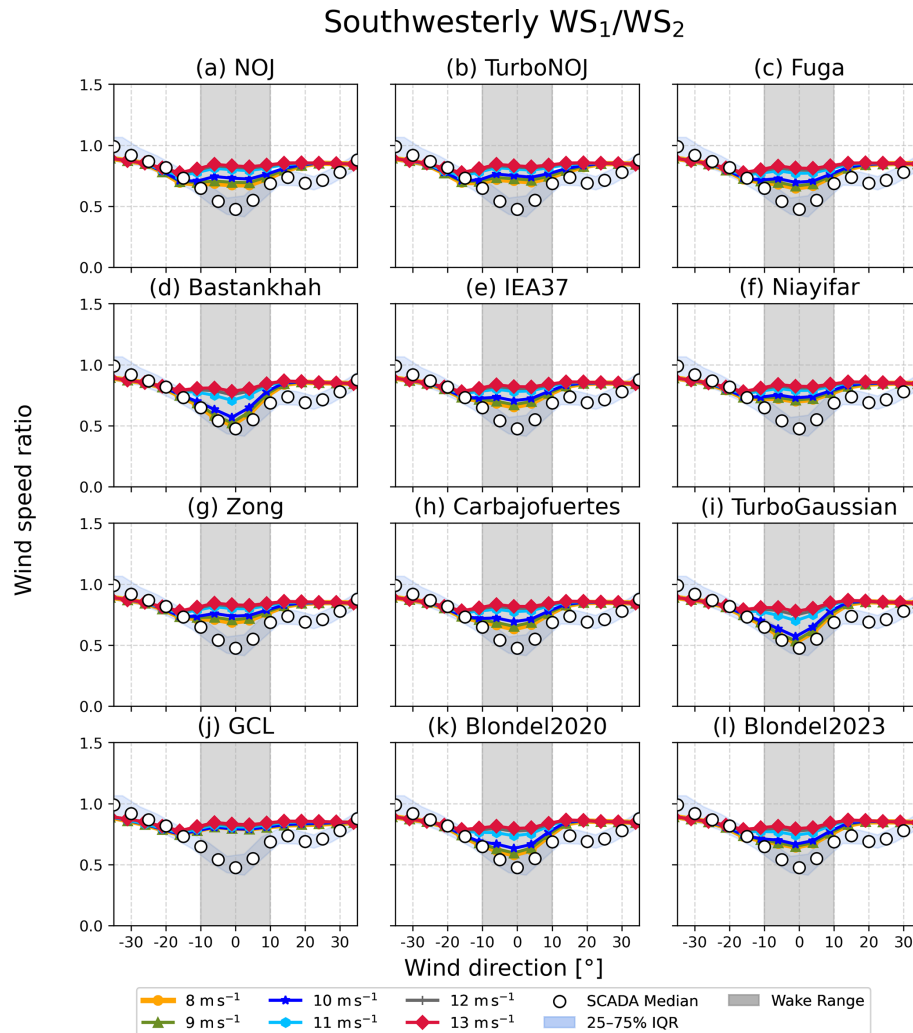


Figure B2. The same as in Fig. B1 but for southwesterly wind. The results ranging from 4 to 8 m s⁻¹ are shown by one line.

Appendix C: Vertical structures of wakes simulated by the 12 wake models

We compare the vertical structures of wakes over complex terrain among the 12 wake models for northeasterly wind and southwesterly wind (Figs. C1 and C2). In Figs. C1a and b and C2a and b, the wakes show linear downstream extensions and no vertical variation. The Fuga wake model exhibits the reduction in wind speed outside the rotor areas (Figs. C1c and C2c). The other wake models produce Gaussian-shaped wakes, whereas the simulated results differ in terms of their wake extents and the reduction in wind speed immediately behind the wind turbines. The Bastankhah wake model and the TurboGaussian wake model show that the wakes generated by the upstream wind turbines reach the rotor of the downstream wind turbines without significant attenuation (Figs. C1d, i and C2d, i).

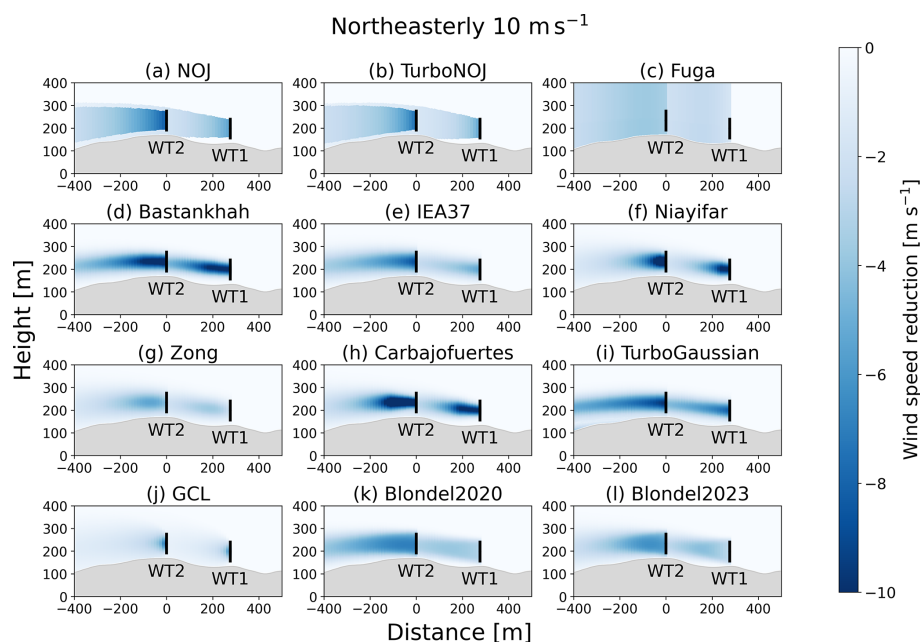


Figure C1. Reduction in horizontal wind speed due to the wakes simulated by the 12 wake models for northeasterly wind. The inflow wind speed far upstream is set to 10 m s^{-1} . The color shading represents the difference in horizontal wind speed between no-wake conditions and wake conditions. The black lines indicate the positions of the wind turbine rotors.

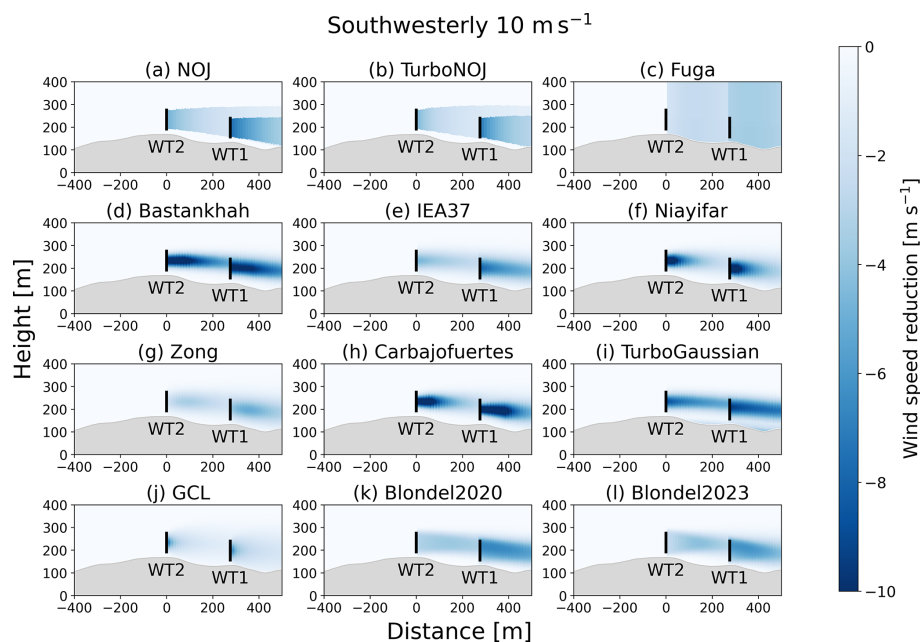


Figure C2. The same as in Fig. C1 but for southwesterly wind.

Code availability. We used open-source code in PyWake 2.5 (<https://topfarm.pages.windenergy.dtu.dk/PyWake/>, last access: 17 July 2025) and WAsP 12 (<https://wasp.dtu.dk/>, last access: 17 July 2025) in this study.

Data availability. The SCADA data were provided by Tsugaru Peninsula Eco Energy Co., Ltd. and are unavailable to the public.

Author contributions. Writing (original draft preparation) and visualization: NS and TS. Writing (review and editing): NS, TS, AH, CB, NT, MG, and MN. Methodology and investigation: NS,

AH, MG, and TS. Software: NS and MN. Conceptualization: NS, AH, and TS. All of the authors contributed with critical feedback on this research and have read and agreed to the published version of the paper.

Competing interests. The contact author has declared that none of the authors has any competing interests.

Disclaimer. Publisher's note: Copernicus Publications remains neutral with regard to jurisdictional claims made in the text, published maps, institutional affiliations, or any other geographical representation in this paper. The authors bear the ultimate responsibility for providing appropriate place names. Views expressed in the text are those of the authors and do not necessarily reflect the views of the publisher.

Acknowledgements. We would like to thank the anonymous reviewers and the editor for their constructive comments on this paper. We wish to express our gratitude to the staff of Tsugaru Peninsula Eco Energy Co., Ltd. and the staff of Japan Steel Works, Ltd. for providing the observational data. We thank Mads Mølgaard Pedersen for analyzing PyWake and Ginka Georgieva Yankova for analyzing the data uncertainty.

Financial support. This research has been supported by the Japan Science and Technology Agency, Support for Pioneering Research Initiated by the Next Generation (grant no. JPMSP2152).

Review statement. This paper was edited by Xiaolei Yang and reviewed by four anonymous referees.

References

- Astolfi, D., Castellani, F., and Terzi, L.: A study of wind turbine wakes in complex terrain through RANS simulation and SCADA data, *J. Sol. Energy Eng.*, 140, 031001, <https://doi.org/10.1115/1.4039093>, 2018.
- Bastankhah, M. and Porté-Agel, F.: A new analytical model for wind-turbine wakes, *Renewable Energy*, 70, 116–123, <https://doi.org/10.1016/j.renene.2014.01.002>, 2014.
- Bastankhah, M. and Porté-Agel, F.: Experimental and theoretical study of wind turbines wakes in yawed conditions, *Journal of Fluid Mechanics*, 806, 506–541, <https://doi.org/10.1017/jfm.2016.595>, 2016.
- Bechmann, A.: WASP CFD A new beginning in wind resource assessment, Tech. rep., Risø National Laboratory, Denmark, <https://www.wasp.dk/-/media/sites/wasp/news/wasp-cfd-a-new-beginning-in-wind-resource-assessment.pdf> (last access: 15 January 2026), 2012.
- Bechmann, A.: Perdigão CFD Grid Study, DTU Wind Energy E 0120, 2016.
- Bechmann, A., Sørensen, N. N., Berg, J., Mann, J., and Réthoré, P.-E.: The Bolund Experiment, Part II: Blind Comparison of Microscale Flow Models, *Boundary-Layer Meteorology*, 141, 245–271, <https://doi.org/10.1007/s10546-011-9637-x>, 2011.
- Berg, J., Troldborg, N., Sørensen, N. N., Patton, E. G., and Sullivan, P. P.: Large-Eddy Simulation of turbine wake in complex terrain, *J. Phys.: Conf. Ser.*, 854, 012003, <https://doi.org/10.1088/1742-6596/854/1/012003>, 2017.
- Blondel, F.: Brief communication: A momentum-conserving superposition method applied to the super-Gaussian wind turbine wake model, *Wind Energ. Sci.*, 8, 141–147, <https://doi.org/10.5194/wes-8-141-2023>, 2023.
- Blondel, F. and Cathelain, M.: An alternative form of the super-Gaussian wind turbine wake model, *Wind Energ. Sci.*, 5, 1225–1236, <https://doi.org/10.5194/wes-5-1225-2020>, 2020.
- Carbajo Fuertes, F., Markfort, C. D., and Porté-Agel, F.: Wind Turbine Wake Characterization with Nacelle-Mounted Wind Lidars for Analytical Wake Model Validation, *Remote Sensing*, 10, 668, <https://doi.org/10.3390/rs10050668>, 2018.
- Castellani, F., Astolfi, D., Burlando, M., and Terzi, L.: Numerical modelling for wind farm operational assessment in complex terrain, *Journal of Wind Engineering and Industrial Aerodynamics*, 147, 320–329, <https://doi.org/10.1016/j.jweia.2015.07.016>, 2015.
- Centurelli, G., Dörenkämper, M., Bange, J., and Platis, A.: Evaluation of Engineering Models for large-scale cluster wakes with the help of in situ airborne measurements, *Wind Energy*, 27, 1040–1062, <https://doi.org/10.1002/we.2942>, 2024.
- Dar, A. S., Berg, J., Troldborg, N., and Patton, E. G.: On the self-similarity of wind turbine wakes in a complex terrain using large eddy simulation, *Wind Energ. Sci.*, 4, 633–644, <https://doi.org/10.5194/wes-4-633-2019>, 2019.
- Dilip, D. and Porté-Agel, F.: Wind turbine wake mitigation through blade pitch offset, *Energies*, 10, 757, <https://doi.org/10.3390/en10060757>, 2017.
- Duncan Jr., J. B., Hirth, B. D., and Schroeder, J. L.: Exploring the complexities associated with full-scale wind plant wake mitigation control experiments, *Wind Energ. Sci.*, 5, 469–488, <https://doi.org/10.5194/wes-5-469-2020>, 2020.
- El-Asha, S., Zhan, L., and Iungo, G. V.: Quantification of power losses due to wind turbine wake interaction through SCADA, meteorological and wind LiDAR data, *Wind Energy*, 20, 1823–1839, <https://doi.org/10.1002/we.2123>, 2017.
- Enomoto, S., Inomata, N., Yamada, T., Chiba, H., Tanikawa, R., Oota, T., and Fukuda, H.: Prediction of power output from wind farm using local meteorological analysis, in: *Proceedings of the European Wind Energy Conference*, Copenhagen, Denmark, 2–5 June 2001, 749–752, ISBN 3-936338-09-4, 2001.
- Farrell, A., King, J., Draxl, C., Mudafort, R., Hamilton, N., Bay, C. J., Fleming, P., and Simley, E.: Design and analysis of a wake model for spatially heterogeneous flow, *Wind Energ. Sci.*, 6, 737–758, <https://doi.org/10.5194/wes-6-737-2021>, 2021.
- Fischereit, J., Schaldemose Hansen, K., Larsén, X. G., van der Laan, M. P., Réthoré, P.-E., and Murcia Leon, J. P.: Comparing and validating intra-farm and farm-to-farm wakes across different mesoscale and high-resolution wake models, *Wind Energ. Sci.*, 7, 1069–1091, <https://doi.org/10.5194/wes-7-1069-2022>, 2022.
- Fleming, P., King, J., Dykes, K., Simley, E., Roadman, J., Scholbrock, A., Murphy, P., Lundquist, J. K., Moriarty, P., Fleming, K., van Dam, J., Bay, C., Mudafort, R., Lopez, H., Skopek, J., Scott, M., Ryan, B., Guernsey, C., and Brake, D.: Initial re-

- sults from a field campaign of wake steering applied at a commercial wind farm – Part 1, *Wind Energ. Sci.*, 4, 273–285, <https://doi.org/10.5194/wes-4-273-2019>, 2019.
- Fleming, P., King, J., Simley, E., Roadman, J., Scholbrock, A., Murphy, P., Lundquist, J. K., Moriarty, P., Fleming, K., van Dam, J., Bay, C., Mudafort, R., Jager, D., Skopek, J., Scott, M., Ryan, B., Guernsey, C., and Brake, D.: Continued results from a field campaign of wake steering applied at a commercial wind farm – Part 2, *Wind Energ. Sci.*, 5, 945–958, <https://doi.org/10.5194/wes-5-945-2020>, 2020.
- Fujikawa, T., Iwasaki, N., Suguro, Y., Iwanaga, Y., and Shibata, M.: Mitsubishi high efficiency large capacity wind turbines, Mitsubishi heavy industries, Ltd. Technical review, 39, 101–106, <https://www.researchgate.net/publication/237268778> (last access: 15 January 2026), 2002.
- Geospatial Information Authority of Japan: Digital national land web, Geospatial information authority map, <https://maps.gsi.go.jp/>, last access: 9 April 2025.
- Göçmen, T., Laan, P. V. D., Réthoré, P., Diaz, A. P., Larsen, G. C., and Ott, S.: Wind turbine wake models developed at the technical university of Denmark: A review, *Renewable and Sustainable Energy Reviews*, 60, 752–769, <https://doi.org/10.1016/j.rser.2016.01.113>, 2016.
- Han, X., Liu, D., Xu, C., and Shen, W. Z.: Atmospheric stability and topography effects on wind turbine performance and wake properties in complex terrain, *Renewable Energy*, 126, 640–651, <https://doi.org/10.1016/j.renene.2018.03.048>, 2018.
- Hansen, K. S., Larsen, G. C., Menke, R., Vasiljevic, N., Angelou, N., Feng, J., Zhu, W. J., Vignaroli, A., Liu, W., Xu, C., and Shen, W. Z.: Wind turbine wake measurement in complex terrain, *J. Phys. Conf. Ser.* 753, 1–10, <https://doi.org/10.1088/1742-6596/753/3/032013>, 2016.
- Hasegawa, Y., Kikuyama, K., Imamura, H., Inomata, N., Suzuki, H., and Ishikawa, H.: Fundamental study for estimation of wind energy resources (Wind Measurements at Tappi Wind Park), *Nihon kikai gakkai ronbunshu, B Hen/Transactions of the Japan Society of Mechanical Engineers, Part B*, 69, 2052–2058, <https://doi.org/10.1299/kikaib.69.2052>, 2003.
- Inomata, N., Tsuchiya, K., and Yamada, S.: Measurement of stress on blade of NEDO's 500 kW prototype wind turbine, *Renewable Energy*, 16, 912–915, [https://doi.org/10.1016/S0960-1481\(98\)00309-7](https://doi.org/10.1016/S0960-1481(98)00309-7), 1999.
- International Electrotechnical Commission (IEC): IEC 61400-1: Wind energy generation systems – Part 1: Design requirements, 4th edn., Geneva, Switzerland, <https://webstore.iec.ch/en/publication/26423> (last access: 15 January 2026), 2019.
- Jeon, S., Kim, B., and Huh, J.: Comparison and verification of wake models in an onshore wind farm considering single wake condition of the 2 MW wind turbine, *Energy*, 93, 1769–1777, <https://doi.org/10.1016/j.energy.2015.09.086>, 2015.
- Jensen, N., O.: A note on wind generator interaction, Risø National Laboratory, ISBN 87-550-0971-9, <https://orbit.dtu.dk/en/publications/a-note-on-wind-generator-interaction/> (last access: 15 January 2026), 1983.
- Larsen, G. C.: A simple stationary semi-analytical wake model”, Risø National Laboratory for Sustainable Energy, Technical University of Denmark, Denmark, Forskningscenter Risøe, Risøe-R, No. 1713(EN), <https://orbit.dtu.dk/en/publications/a-simple-stationary-semi-analytical-wake-model/> (last access: 15 January 2026), 2009.
- Launder, B. E. and Spalding, D. B.: The numerical computation of turbulent flows, *Computer Methods in Applied Mechanics and Engineering*, 3, 269–289, [https://doi.org/10.1016/0045-7825\(74\)90029-2](https://doi.org/10.1016/0045-7825(74)90029-2), 1974.
- Letzgus, P., Guma, G., and Lutz, T.: Computational fluid dynamics studies on wind turbine interactions with the turbulent local flow field influenced by complex topography and thermal stratification, *Wind Energ. Sci.*, 7, 1551–1573, <https://doi.org/10.5194/wes-7-1551-2022>, 2022.
- Mittelmeier, N., Allin, J., Blodau, T., Trabucchi, D., Steinfeld, G., Rott, A., and Kühn, M.: An analysis of offshore wind farm SCADA measurements to identify key parameters influencing the magnitude of wake effects, *Wind Energ. Sci.*, 2, 477–490, <https://doi.org/10.5194/wes-2-477-2017>, 2017.
- Niayifar, A. and Porté-Agel, F.: Analytical Modeling of Wind Farms: A New Approach for Power Prediction. *Energies*, 9, 741, <https://doi.org/10.3390/en9090741>, 2016.
- Nygaard, N., G., Steen, S., T., Poulsen, L., and Pedersen, J., G.: Modelling cluster wakes and wind farm blockage, *J. Phys. Conf. Ser.*, 1618, 062072, <https://doi.org/10.1088/1742-6596/1618/6/062072>, 2020.
- Oqaily, D. A., Giani, P., and Crippa, P.: Evaluating WRF Multiscale Wind Simulations in Complex Terrain: Insights from the Perdigão Field Campaign, *Journal of Geophysical Research: Atmospheres*, 130, e2025JD044055, <https://doi.org/10.1029/2025JD044055>, 2025.
- Ott, S., Berg, J., and Nielsen, M.: Linearised CFD models for wakes. Technical report, Danmarks Tekniske Universitet, Risø Nationallaboratoriet for Bæredygtig Energi, Forskningscenter Risøe, Risøe-R No. 1772(EN), <https://orbit.dtu.dk/en/publications/linearised-cfd-models-for-wakes/> (last access: 15 January 2026), 2011.
- Pedersen, J. G., Svensson, E., Poulsen, L., and Nygaard, N. G.: Turbulence Optimized Park model with Gaussian wake profile, *J. Phys. Conf. Ser.*, 2265 022063, <https://doi.org/10.1088/1742-6596/2265/2/022063>, 2022.
- Pedersen, M. M., van der Laan, P., Friis-Møller, M., Forsting, A. M., Riva, R., Román, L. A. A., Risco, J., C., Quick, J., Christiansen, J. P. S., Olsen B. T., Rodrigues, R. V., and Réthoré, P. E., DTU WindEnergy/PyWake: PyWake (v2.5.0), Zenodo [code], <https://doi.org/10.5281/zenodo.6806136>, 2023.
- Politis, E. S., Prospathopoulos, J., Cabezón, D., Hansen, K. S., Chaviaropoulos, P. K., and Barthelmie, R. J.: Modeling wake effects in large wind farms in complex terrain: The problem, the methods and the issues, *Wind Energy*, 15, 161–182, <https://doi.org/10.1002/we.481>, 2011.
- Porté-Agel, F., Bastankhah, M., and Shamsoddin, S.: Wind-Turbine and Wind-Farm Flows: A Review, *Boundary-Layer Meteorol.*, 174, 1–59, <https://doi.org/10.1007/s10546-019-00473-0>, 2020.
- Rhodes, M. E. and Lundquist, J. K.: The effect of wind-turbine wakes on summertime US midwest atmospheric wind profiles as observed with ground-based Doppler lidar, 149, 85–103, <https://doi.org/10.1007/s10546-013-9834-x>, 2013.
- Ruisi, R. and Bossanyi, E.: Engineering models for turbine wake velocity deficit and wake deflection. A new proposed approach for onshore and offshore applications, in: *Journal of Physics: Con-*

- ference Series, vol. 1222, 012004, <https://doi.org/10.1088/1742-6596/1222/1/012004>, 2019.
- Sasanuma, N. and Honda, A.: Wind analyzing of wind turbines and lighthouse in Tappi with relative point of view, *Wind Engineering Symposium*, 26, 19–24, https://doi.org/10.14887/natsympwindengproc.26.0_19, 2020.
- Sasanuma, N. and Honda, A.: Study on wind characteristic and wind wake effect in complex terrain, *Journal of Wind Engineering*, 27, 294–302, https://doi.org/10.14887/windengresearch.27.0_294, 2022.
- Sasanuma, N. and Honda, A.: Observation survey on wind turbines installed close to complex terrain: the effects terrain and wind turbine wake, *Journal of Wind Engineering*, 28, 267–275, https://doi.org/10.14887/windengresearch.28.0_267, 2024.
- Sessarego, M., Feng, J., Friis-Møller, M., Xu, Y., Xu, M., and Shen, W., Z.: Development of a streamline wake model for wind farm performance predictions, *J. Phys. Conf. Ser.*, 1618, 062027, <https://doi.org/10.1088/1742-6596/1618/6/062027>, 2020.
- Sharma, P. K., Warudkar, V., and Ahmed, S.: Application of a new method to develop a CFD model to analyze wind characteristics for a complex terrain, *Sustainable Energy Technologies and Assessments*, 37, 100580, <https://doi.org/10.1016/j.seta.2019.100580>, 2020.
- Shimada, T., Sawada, M., and Iwasaki, T.: Indices of cool summer climate in northern Japan: Yamase indices, *J. Meteor. Soc. Japan*, 92, 17–35, <https://doi.org/10.2151/jmsj.2014-102>, 2014.
- Troen, I. and Hansen, B. O.: Wind Resource Estimation in Complex Terrain: Prediction Skill of Linear and Nonlinear Micro-Scale Models, Paper presented at AWEA Windpower Conference & Exhibition, Orlando Orange County Convention Center, United States. May 18, https://backend.orbit.dtu.dk/ws/portalfiles/portal/110738156/Wind_resource_estimation.pdf (last access: 15 January 2026), 2015.
- Troldborg, N., Andersen, S. J., Hodgson, E. L., and Meyer Forsting, A.: Brief communication: How does complex terrain change the power curve of a wind turbine?, *Wind Energ. Sci.*, 7, 1527–1532, <https://doi.org/10.5194/wes-7-1527-2022>, 2022.
- Uchida, T. and Takakuwa, S.: Numerical Investigation of Stable Stratification Effects on Wind Resource Assessment in Complex Terrain, *Energies*, 13, 6638, <https://doi.org/10.3390/en13246638>, 2019.
- Ushiyama, I.: Wind energy activities in Japan, *Renewable Energy*, 16, 811–816, [https://doi.org/10.1016/S0960-1481\(98\)00261-4](https://doi.org/10.1016/S0960-1481(98)00261-4), 1999.
- Wagner, J., Gerz, T., Wildmann, N., and Gramitzky, K.: Long-term simulation of the boundary layer flow over the double-ridge site during the Perdigão 2017 field campaign, *Atmos. Chem. Phys.*, 19, 1129–1146, <https://doi.org/10.5194/acp-19-1129-2019>, 2019.
- Wenz, F., Langner, J., Lutz, T., and Krämer, E.: Impact of the wind field at the complex-terrain site Perdigão on the surface pressure fluctuations of a wind turbine, *Wind Energ. Sci.*, 7, 1321–1340, <https://doi.org/10.5194/wes-7-1321-2022>, 2022.
- Yamaguchi, A., Ishihara, T., and Fujino, Y.: Applicability of linear and nonlinear wind prediction models to wind flow in complex terrain, in: *Proceedings of The World Wind Energy Conference and Exhibition*, Berlin, Germany, 3–8 July 2002, 1–4, <https://www.researchgate.net/publication/266863617> (last access: 15 January 2026), 2002.
- Yamaguchi, A., Tavana, A., and Ishihara, T.: Assessment of wind over complex terrain considering the effects of topography, Atmospheric stability and turbine wakes, *Atmosphere*, 15, 723, <https://www.mdpi.com/2073-4433/15/6/723> (last access: 15 January 2026), 2024.
- Yang, X., Sotiropoulos, F., Conzemius, R. J., Wachtler, J. N., and Strong, M. B.: Large-eddy simulation of turbulent flow past wind turbines/farms: The Virtual Wind Simulator (VWiS), *Wind Energy*, 18, 2025–2045, <https://doi.org/10.1002/we.1802>, 2015.
- Zong, H. and Porté-Agel, F.: A momentum-conserving wake superposition method for wind farm power prediction, *Journal of Fluid Mechanics*, 889, <https://doi.org/10.1017/jfm.2020.77>, 2020.
- zum Berge, K., Centurelli, G., Dörenkämper, M., Bange, J., and Platis, A.: Evaluation of Engineering Models for large-scale cluster wakes with the help of in situ airborne measurements, *Wind Energy*, 27, 1040–1062, <https://doi.org/10.1002/we.2942>, 2024.