# [..* ]Evaluation of the impact of active wake control techniques on ultimate loads for a 10 MW wind turbine.

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**Abstract.** Wind farm control is one of the solutions recently proposed to increase the overall energy production of a wind power plant.

A generic wind farm control is typically synthesized so as to optimize the energy production of the entire wind farm by reducing the detrimental effects due to wake-turbine interactions. As a matter of fact, the performance of a farm control is typically measured by looking [..[2] ]at the increase of the power production, properly weighted [..[3] ]through the wind statistics. Sometimes, also fatigue loads are considered in the control optimization problem. However, an aspect which is rather overlooked [..[4] ]in the literature on this subject is the evaluation of the impact that a farm control law has on the individual wind turbine in [..[5] ]terms of maximum loads and dynamic response under extreme conditions.

In this work, two promising wind farm controls, based respectively on Wake Redirection (WR) and Dynamic Induction Control (DIC) strategy, are evaluated at [..[6] ]the level of a single front-row wind turbine. To do so, a two-pronged analysis is performed. Firstly, the control techniques are evaluated in terms of the related impact on some specific key performance indicators[..[7] ], with special emphasis on ultimate loads and maximum blade deflection[..[8] ]. Secondarily, an optimal blade redesign process [..[9] ]is performed with the goal of quantifying the [..[10] ]modification in the structure of the blade [..[11] ]entailed by a possible increase in ultimate values due to the presence of wind farm control. Such an analysis provides for an important piece of information for assessing the impact of the farm control on the Cost of Energy model.

## 1 Introduction and motivation

So far, the majority of the works devoted to wind farm control is aimed at evaluating the effectiveness of such techniques as means of power harvesting maximization. Among all, one can mention the methodologies based on wake steering (see Fleming

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et al. (2019); Gebraad et al. (2017, 2016)), steady axial induction (see Annoni et al. (2016)) and dynamic induction control,
20   also called active wake mixing (see Munters and Meyers (2018, 2017)). When it comes to farm control synthesis, the energy production is typically viewed as the most significant merit figure, and seldom the fatigue loads on single wind turbine (WT) are considered within the control optimization problem (Bossanyi, 2018; Knudsen et al., 2015).

[..[12] ]The quantification of the impact of wind farm control setpoint on turbine fatigue, needed for any load assessment process, has been object of an extensive research in recent years, especially in relation to yawed operations (Cardaun et al.,
25   2019; Ennis et al., 2018; White et al., 2018). All works suggested that the impact of misalignment depends strongly on ambient conditions (such as vertical shear and turbulence intensity).

Boorsma (2012) evaluated the fatigue loads of a 2.5 MW turbine operating in misaligned conditions using different aero-dynamic models [..[13] ]and compared the results with field measurements. It was shown that the combination of vertical shear layer and misalignment may lead to an increase or decrease of fatigue loads, depending on the sign of the yaw misalignment
30   angle.

A similar study[..[14] ], based on a dedicated and systematic [..[15] ]field test campaign, for a 1.5 MW turbine, yielded similar conclusions (Damiani et al., 2018).

Zalkind and Pao (2016) analyzed the impact of wake redirection control in terms of fatigue loads considering a simple two-turbine cluster and a reference wind rose. The aggregate damage equivalent loads were computed from the actual yaw
35   misalignment angles which the upstream turbine would experience for maximizing the total power of the cluster. In such an ideal case, the impact of wake redirection control resulted to be small due to the large amount of time spent with no yaw misalignment.

Mendez Reyes et al. (2019) and Kanev et al. (2018) considered the problem of quantifying the fatigue loads of downstream turbines impinged by the wakes shed by upstream machines. Both studies concluded that, in terms of loading, impinging
40   wakes are typically more detrimental [..[16] ]than operations with yaw misalignment[..[17] ]. Consequently, wake redirection is expected to reduce the overall lifetime fatigue thanks to the mitigation of rotor-wake interactions.

Finally, Frederik et al. (2020b) provided the first evaluation of the impact [..[18] ]of dynamic induction control on fatigue, considering a reference 5 MW turbine model.

Despite the availability of such relevant results, the question over the actual impact of farm control on rotor design is still
45   an open question. In fact, while fatigue loads may [..[19] ]even decrease in controlled farms, ultimate values for loads and blade tip deflections, typically coming from extreme events [..[20] ]like gusts or faults, may significantly increase due to the different wind turbine operating conditions connected to the wind farm control. Ultimate loads, maximum tip displacements,

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as well as fatigue loads, participate together in the definitions of the constraints to which a machine is subject during the design phase. Hence, the possible increase in machine [..[21] ]ultimate values due to wind farm control [..[22] ]could determine whether

50   a turbine structure is to be re-designed, with an eventual increase of its mass and cost, or not.

[..[23] ]

As expected, the advantages (i.e. the increased power production at farm level) and the disadvantages (i.e. the possible increased loading at turbine level) of a farm control [..[24] ]should be combined to determine their impact in terms of cost of energy (CoE). In order to show this concept, one may consider the simple definition of the CoE of a single turbine, reported in

55   Fingersh et al. (2006),

$$CoE = \frac{FCR \cdot ICC}{AEP} + AOE,$$

where FCR is the fixed charge rate, ICC the initial capital cost, consisting mainly in the turbine cost, and AOE the annual operating expenses (expressed per unit energy yield), which may include land or sea lease[..[25] ], operation and maintenance costs. Clearly, the AEP of a single turbine may be reduced or increased by the farm control according to the fact that a

60   machine operates mainly upstream or downstream. The sum of the AEPs of all turbines belonging to the farm increases for a farm control neatly designed.

Besides that, [..[26] ]

[..[27] ]given a specific wind farm control technique, the component loading should be evaluated [..[28] ]at turbine level, so as to clarify if a generic turbine within a "controlled farm" would need a dedicated design[..[29] ]. If so, the farm control, in addition

65   to an expected increase of farm AEP, will also have an influence in terms of ICC.

The scope of this paper is twofold. First, to quantify the impact of [..[30] ]wake steering and dynamic induction control [..[31] ]at the level of the front-row turbine through some indicators strictly connected to machine design, which are the ultimate loads and the maximum blade tip deflection, computed according to the present Standards. To the best of the Authors' knowledge, the implications of farm control in terms these indicators have never been addressed, hence this part of the work represents the

70   major source of novelty of the paper. Second, in order to provide an insight in the impact of farm control on the cost of the

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[23]removed: This consideration is of paramount importance as the turbine design and the resulting CoE can be considered as the ultimate indicators of the effectiveness of a farm control strategy.

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rotor, an optimal blade re-design process is performed, which takes into consideration the [..[32] ]possible influence that wind farm control [..[33] ]has on blade ultimate loads and maximum blade tip deflections.

A complete procedure for a wind turbine design should, in principle, consider all the machines of [..[34] ]farm. To do so, it would be necessary to know the farm layout and the wind rose. This complex and site-specific procedure is out of the scope

75 of this research activity and hence the [..[35] ]present analyses will focus only on the front-row wind turbine, i.e. the one [..[36] ]which is subject to the undisturbed wind and has to operate according to the farm control inputs.

Clearly, in a single farm, there is a subset of machines which see most of the time a clean flow, i.e. the outermost ones exposed according to the most probable wind direction, and another subset of turbines, the innermost ones, which sometimes see a waked flow. In this scenario, since different turbines may be exposed to different flows on average, it is certainly

80 interesting to evaluate a possible usage of partially customized or totally different turbines in a single farm, depending on the specific machine location. In such a case, the turbines proposed for [..[37] ]some farm locations could be characterized by more competitive designs thanks to the farm control. Although extremely interesting, this idea falls out of the scope of the present paper. [..[38] ]However, the final design process presented in Sec. 4.4 supports this investigation providing a preliminary indication on the potential impact of farm controls on the rotor design of the front-row wind [..[39] ]turbines.

85 Finally, in this work, all analyses are performed on the INNWIND.EU 10 MW wind turbine (DTU, 2012), which can be considered as a generic reference model for present and future machines proposed for the exploitation of on- and off-shore resources.

The [..[40] ]paper is organized as follows. Sections 2 and 3 deal with the explanation of the methodologies adopted to evaluate the impact of wind farm control [..[41] ]at single wind turbine level. These sections include the [..[42] ]definition of the wind turbine

90 used [..[43] ]in the analysis and its controller, along with the description of the multibody software [..[44] ]employed for the aeroservoelastic simulations and [..[45] ]the optimal rotor design tool. In Sec. 4, a sensitivity analysis on the effects of two wind farm control techniques (i.e. WR and DIC) is considered. Specifically, ultimate loads and maximum blade tip deflection are evaluated considering different [..[46] ]settings of the controls (e.g. different yaw misalignment angles for wake redirection[..[47] ]) in order to find the most impacting conditions for the turbine. Such sensitivity analysis is viewed as a preliminary step for

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95 the optimal blade design process which is described in Sec. 4.4. Finally, Sec. 5 concludes [..[48] ]the manuscript listing the main findings and possible outlooks of the work.

## 2 Methodology

Having an overview of the effects that a wind farm control [..[49] ]may have on a single wind turbine and eventually quantifying its impact on the design of the rotor is not an easy task. In fact, when dealing with an entire wind farm, the problem of
100 analyzing wind turbine performance becomes highly [..[50] ]site-specific because the inputs of the farm control will depend on many factors, such as the farm layout, the wind distribution and rose as well as the turbulence intensities. In such a scenario, deriving conclusions of general validity without focusing too much on a specific case is [..[51] ]rather difficult.

[..[52] ]

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105 Moreover, wind turbines are designed according to international Standards, which prescribe the computation of fatigue and ultimate loads in a certain number of conditions, e.g. for specific wind speeds and turbulence intensity levels. [..[54] ]

A recent position paper on certification and standardization issues of wind farm control considers, among all, the problem of the integration of this new technology into the current regulatory framework (?). According to that position paper, although existing Standards do not cover explicitly the wind farm control case, they can be used for this aim
110 following three practical approaches, based on either long-term measurements, risk-based certifications or temporary allowance to test novel control applications. Additionally, Standards offer some tools, which could be useful to handle design of wind turbines operating in a controlled farm. For example, IEC 61400-1 Ed.3. (2004) suggests to either *a)* verify that the specific flow conditions at single turbine locations are covered by the reference wind statistics or *b)* simulate the site-specific loads through the straightforward added-turbulence Frandsen model (?). The recently published ?, in order
115 to assist load assessment of a specific turbine, also proposes a wake meandering model, which is expected to be more adequate than added-turbulence techniques.

Notwithstanding the present regulatory framework offers such possibilities, the Authors of the Position Paper admit that applying the current Standards to specific project can be challenging and that a fast and accurate calculation of loads is

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[52] removed: Moreover, in the same wind farm, a turbine may act according to a farm control input (e.g. operates at a specific yaw misalignment angle to redirect its wake) and/or feel the effects of the control action performed by another machine, depending on whether it is up- or down-stream with respect to the wind direction. As a consequence, one should have to model all possible cases to have a global overview. This clearly poses some difficulties as the study would result to be again strongly dependent on the farm geometry and would lose, at least in part, its generality.

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[54] removed: Hence, the impact of a farm control , in this work, has been evaluated through those existing Standards specifications. Although adhering to Standards poses some limitations to the analyses, e. g. fatigue is verified only for a single shear layer exponent and for specific combinations of wind speed and turbulence intensity, it is only through such an approach that one can evaluate the "practical" impact

needed for designing turbines in all positions of the farm in case a wind farm control law is implemented. In this scenario,
120  the possible increase in fatigue and ultimate loads certainly represents a risk to carefully handle for the future practical
usage of wind farm controls.

This discussion highlights the topicality of the object of the present work, mainly focused on the impact of farm controls
on ultimate loads. In fact, as already mentioned in Sec. 1, much has been done in terms of fatigue but, at the same time,
much is still to be done for quantifying if and how the farm control modifies ultimate loads and maximum tip deflections,
125  which are typical drivers for component design of modern wind turbine blades.

Although, the response of downstream machines is surely influenced by the presence of wind farm [..[55] ]

[..[56] ]controls, it is important to provide first a preliminary quantification of such an impact on upstream machines,
i.e. those implementing a wake control logic. In this work, we will analyze only this case and consequently the obtained
results apply to only front row wind turbines. This clearly represents a strong simplification of the problem, as one does
130  not have to model the in-farm flow. In this regard, one could stress that real turbines operating in real farms typically
experience wake interaction phenomena. Despite that, when a wind farm comes to its end of service, most turbines
still have some residual life to exploit (Ziegler et al., 2018), even if wake impingement represents a significant source of
loading (Mendez Reyes et al., 2019; Kanev et al., 2018). On the other side, operating according to the farm control, e.g.
in prolonged misalignment conditions, represent a clear source of risk for front-row turbines also in light of the present
135  regulatory framework. Accordingly, the choice of focusing only on the upstream turbines is not to be viewed as a limitation
of the analysis but rather as a further step towards a comprehensive knowledge of positive and negative aspects of wind
farm control [..[57] ]in terms of its implication on the design of the machines.

[..[58] ]Looking at the sole front-row wind turbines leads to a simplified analysis which takes into account only the well-
known list of Design Load Cases (cf. IEC 61400-1 Ed.3. (2004), § 7.4), to be neatly modified so as to include the oper-
140  ations under wind farm control inputs. In this regard, the work of this paper considers only a wind speed-dependency of
the control and imposes as limit for its activation 15 m/s no matter of TI.

In order to have an indication of general validity, which may support further activities on the same topic, the analyses have
been conducted as sensitivity studies[..[59] ]. The effects of the wind farm control are considered as functions of some important
[..[60] ]parameters. For example, the study of the wake redirection was carried out for different values of yaw misalignment,
145  whereas that of the DIC for different frequency and amplitude values of the pitch oscillation. From this point of view, such a

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[55]removed: control on turbine design.Unfortunately, regulations, in their current status, do not consider yet the fact that a turbine may operate out of the
design conditions according to a farm control.

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problem, if and how to consider the effects of

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sensitivity analysis can be [..[61] ]used as input for the synthesis and fine tuning of a farm control by reducing its authority in conditions which could be critical from the loading side.

For example, since a turbine operating in yawed conditions may be more exposed to extreme events (i.e. gusts or extreme shear), it could be interesting to bound the operational range of the controller within certain values of misalignment, in order

150   to limit the increase of the [..[62] ]design-driving loads.

Similarly, the amplitude and the frequency of the pitch motion for dynamic induction control can be chosen also by looking at the effect of fatigue and actuator duty cycle. This possibility, although interesting, is not considered in this paper, as it is out of its scope, and will be further investigated as a follow-up of this work.

[..[63] ]

155   The next sections will show that, even if only the front wind turbine [..[64] ]is investigated, the design loads, coming from extreme events, may increase under these wind [..[65] ]farm control inputs.

Clearly, determining how much the loads could increase when considering the "internal" wind turbines [..[66] ]is not possible with the present approach. Such an investigation is beyond the scope of this work.

To further investigate the effect of these wind farm controls, in the last section, it is presented a state-of-the-art pro-

160   cedure in which the rotor blades have been redesigned with the DIC algorithm enabled. The goal of this last analysis is to quantify the changes in internal blade geometry required when the wind farm control is operating on the wind turbine itself. The subsequent increase in mass, and thus blade cost, is, in fact, an important and direct indicator of the impact of the wind farm control as discussed previously.

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[62]removed: driving loads. Otherwise

[63]removed: Dealing with the effects of the farm control on downstream machines, it is important to stress the fact that real turbines typically operate in a farm and are certainly influenced by wake interaction phenomena. Despite that, when a wind farm comes to its end of service, most turbines still have some residual life to exploit (Ziegler et al., 2018). For this reason, even if wake interactions represent a significant source of loading, as demonstrated in some recent publications (Mendez Reyes et al., 2019; Kanev et al., 2018), one could conclude that modern design procedures and regulations are adequate to guarantee safe wind turbine operations even in presence of normal wake impingement events. Accordingly, the analyses conducted in this work refer only to the upstream turbine, i.e. the one which performs an action according to the control of the farm; an aspect which is actually not considered in current design procedures. Moreover, in order to simplify the treatment, the work of this paper considered only a wind speed-dependency of the control and imposed as limit for its activation 15 m/s no matter of TI.

[64]removed: , e.g. the one which operates the wind farm control out of the wakes of other turbines,

[65]removed: farms controllers. Clearly this assumption, e.g. not to consider the inner wind turbines, does not make it possible to determine

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[67]removed: To further investigate the effect of these wind farm controls, in the last section is presented a state-of-the-art procedure in which the rotor blades have been redesigned with the DIC algorithm enabled. The goal of this last analysis is to quantify the changes in internal blade geometry required when the wind farm control is operating on the wind turbine itself. The subsequent increase in mass, and thus blade cost, is, in fact, an important and direct indicator of the impact of the wind farm control as discussed in the previous section.

## 3 Analysis and design framework

In this work we use the INNWIND.EU 10 MW wind turbine (DTU, 2012) as a reference for all parametric analyses and design activities. All dynamic simulations are run by our in-house multibody solver `Cp-Lambda` (Bottasso and Croce, 2009–2018; Bottasso et al., 2006). This tool allows one to model the flexibility of blades, tower and shafts through a [..[68] ]geometrically exact beam model (Bauchau, 2011)[..[69] ], whose sectional structural properties are rendered through fully populated $6 \times 6$ [..[70] ]stiffness matrices. Aerodynamics is rendered via the classical BEM theory with hub- and tip-losses and tower shadow. First and second order dynamical models are employed to include respectively generator and pitch actuator dynamics.

The control of the turbine in operating conditions is managed by the CL-WINDCON standard controller (CL-Windcon, 2016 -2019; IK4 Research Alliance, 2016), while non-operating conditions like faults, startups, shutdowns and parking are all managed by the *POLI-Wind Supervisor* (Riboldi, 2012), that also supervises the transitions between different operating states[..[71] ].

The design and optimization activities are run by `Cp-Max`, a tool for the integrated design of wind turbines, jointly developed by Politecnico di Milano and the Technische Universität München. A detailed description of the algorithm, along with some design applications, is provided by Sartori (2019) and by Bortolotti et al. (2016)[..[72] ].

Thanks to its multi-level architecture, `Cp-Max` is able to both optimize the [..[73] ]main features of the turbine (rotor diameter, tower height, tilt and cone angle) and [..[74] ]conduct specific optimization of [..[75] ]turbine subcomponents like blades, tower and generator. This double capability is achieved through the coupling [..[76] ]among a Macro Design Loop (MDL) and several design submodules. In this work, we only use the Structural Design Submodule (SDS), whose workflow is shown in Fig. 1.

The purpose of the SDS is to manage the structural design of the rotor through a dedicated optimization in which the thicknesses of all structural components are [..[77] ]sized to minimize the turbine ICC. As shown in [..[78] ]Fig. 1, the structural optimization is conducted through a multi-steps procedure: initially, an arbitrarily large set of Design Load Cases (DLCs) is [..[79] ]performed with `Cp-Lambda` to extract the driving loads and displacements from fully-resolved aeroelastic simulations. Once maximum loads and displacements are computed, the structural optimization begins and the internal thicknesses are modified until a converged solution is found. Then, if the optimal blade mass is significantly different from the initial, the whole process (DLC + structural design) is repeated, so that the design can always account for the updated load spectra. [..[80]

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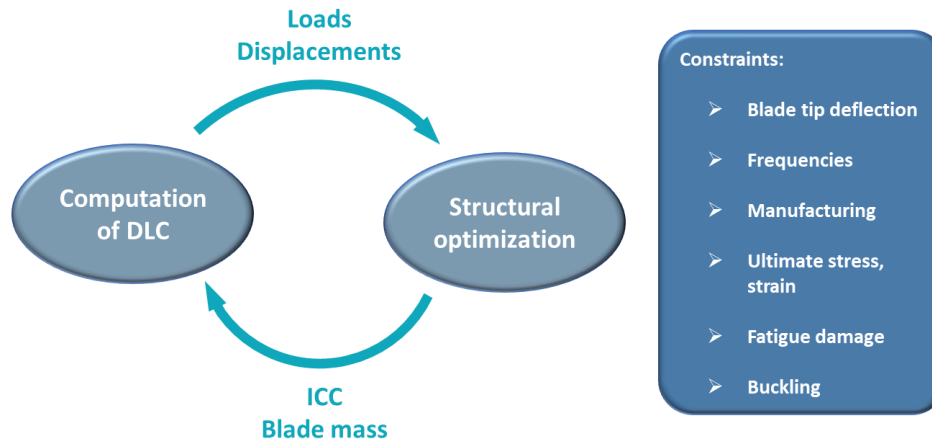[75]removed: the

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**Figure 1.** Architecture of the Structural Design Submodule (SDS).

]Throughout this process, structural integrity constraints are enforced according to international certification guidelines. Those account for maximum deflections, stiffness, strength, possible manufacturing limitations, fatigue and buckling.

Given the complexity of the problem at hand, any design-oriented activity should be [..[81] ]carefully planned out so as to identify the best trade-off between modelling accuracy, computational effort and design scope. In this view, we introduced some [..[82] ]assumptions in order to find a good balance between scope and CPU time. Our first choice was to limit the redesign effort to the optimization of the blade structure. In fact, although wind farm [..[83] ]controller may impact other [..[84] ]parts of the turbine and possibly also blade shape, it is reasonable to expect that [..[85] ]it mainly affects the driving loads, with important implications [..[86] ]for rotor structure. As a consequence, the macro parameters of the wind turbine like the rotor radius and tower height have not been modified[..[87] ]. Similarly, the aerodynamic shape of the rotor has been kept constant and coherent to that of the baseline. It must be noticed that, by introducing this scope limitation, it was possible to include a large set of fully-resolved DLCs directly in the design, without the need to adopt any simplification on the load spectra. In particular, it was possible to use the set of DLCs listed in Table 1, defined according to the chosen standards IEC 61400-1 Ed.3. (2004). The entire set includes about 130 load cases, for a total computational time of 26[..[88] ]~28 hours on a common desktop.

As clear from the fifth column of Table 1, the analyses performed in this work considered only failure modes related to the single turbine, without analyzing possible implications of malfunctions of wind farm control and its supporting technology. The relevant problem of wind farm control failure modes is currently an open topic to study. In general, as

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suggested in a recent report (**?**), a wind farm control can be practically implemented so as to minimize the impact that its possible failures may have on turbine operating conditions. In fact, in case of conflict between the individual turbine regulators and farm controllers, the priority should be given to the former. Moreover, like any modern turbine has its own protection system, which can shut the machine down in case of critical conditions (e.g. strong wind and high vibrations), it is reasonable to think that also farm controllers may be equipped with similar devices: in case failures are detected, the farm controller is disengaged, and nominal operations based on greedy control are restored. This suggests that, at least for the goal of this work, although an interesting topic, the failure modes of farm control can be neglected within the DLC list.

**Table 1.** Definition of the DLCs considered in the analyses.

| DLC | Wind Type | Wind speed | Horizontal Misalignment | Fault | Safety Factor | Performance indicator |
|-----|-----------|------------|-------------------------|-------|---------------|-----------------------|
| 1.1 | NTM | $V_{in} : V_{out}$ | - | - | 1.35 | Ultimate |
| 1.2 | NTM | $V_{in} : V_{out}$ | - | - | 1.0 | AEP, ADC, Fatigue |
| 1.3 | ETM | $V_{in} : V_{out}$ | - | - | 1.35 | Ultimate |
| 1.4 | ECD | $V_r, V_r \pm 2, V_{out}$ | - | | 1.35 | Ultimate |
| 1.5 | EWS | $V_r, V_r \pm 2, V_{out}$ | - | | 1.35 | Ultimate |
| 2.1 | NTM | $V_{in} : V_{out}$ | - | Grid Loss | 1.35 | Ultimate |
| 2.2 PF | NTM | $V_{in} : V_{out}$ | - | Pitch Freeze | 1.35 | Ultimate |
| 2.2 PR | NTM | $V_{in} : V_{out}$ | - | Pitch Runaway | 1.35 | Ultimate |
| 2.3 | EOG | $V_r, V_{out}$ | - | Grid Loss | 1.1 | Ultimate |
| 6.1 | EWM | $V_{ref}$ | $-8 : 8$ deg | - | 1.35 | Ultimate |
| 6.2 | EWM | $V_{ref}$ | $-180 : 180$ deg | Grid Loss | 1.1 | Ultimate |
| 6.3 | EWM | $V_{ref}$ | $-20 : 20$ deg | - | 1.1 | Ultimate |

## 4  Sensitivity analysis about the effects of wind farm control on turbine level

The Standards require a turbine to be designed under a full list of [..[89] ]loads cases which include normal operative conditions, [..[90] ]situations where the machine undergoes extreme events or faults, [..[91] ]as well as cases in which the turbine is parked. [..[92] ]

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[92]removed: Clearly, according to the specific case, we can either reasonably consider or completely exclude that the turbine may operate in a wind-farm-controlled regime.

[..[93] ]Obviously, in order to have a correct evaluation of the impact of farm control on ultimate loads, one has to simulate also those cases in which the farm control is certainly not active (e.g. parked conditions). In fact, one may

220 imagine a situation in which, without wind farm control, a specific sub-component [..[94] ]is sized on the basis of a particular ultimate load, noted $U^*$, [..[95] ]coming from a parked condition (DL6.n). In this case, [..[96] ]even if wind farm control [..[97] ]entails an increase of machine loading [..[98] ]in other operative conditions, unless such increase is not enough to exceed $U^*$, the presence of wind farm control [..[99] ]results irrelevant to that ultimate value and, in turn, to the design of that sub-component.

225 Along with the list of DLCs, it is necessary to select the range in which the wind farm control is active. Clearly, the activation of the wind farm control is based on the specific implementation of the control scheme, and may depend on wind speed, turbulence intensity, geometry of the farm and even on combinations of the previous factors. In this very complex scenario, in order to simplify the analysis, the farm control is considered active only [..[100] ]up to a given speed[..[101] ], chosen here as 15 m/s, no matter of the turbulence intensity or other factors.

## 230 4.1 Evaluation of the impact of wake redirection technique

In this Section the effects of the wake redirection control on wind turbine loads [..[102] ]and blade deflections are investigated.

The wind farm control based on the wake redirection technique consists in yawing an upstream turbine by a specific amount in order to deflect its wake out of one or more downstream turbines [..[103] ](Fleming et al. (2019); Gebraad et al. (2017, 2016)). Within such a wind farm control scenario, while the upstream machine experiences a loss of power, due to the wind

235 misalignment, the downstream ones produce more power thanks to a reduced wake impingement.

In this work, the turbine misalignment is reproduced in the simulations by rotating the nacelle. Positive angles are associated to counterclockwise rotations of the nacelle viewed from above. Hence, the turbine experiences positive yaw misalignment when the wind is coming from the right side, for an observer sitting on the hub and looking at the wind. In the reference configuration (i.e. for a null yaw angle) the wind is assumed to blow from North to South and, accordingly, the nacelle is

240 oriented towards North.

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[93] removed: For example, it may happen that, for a specific turbine and for a specific

[94] removed: , the related

[95] removed: comes from a case in which the wind farm control is not active (as for the DLC6.nin parked conditions

[96] removed: it is possible and foreseeable that the

[97] removed: may entail a general

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[100] removed: in a range of wind speeds (i.e.

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[102] removed: and blade deflections

[103] removed: ( Fleming et al. (2019); Gebraad et al. (2017, 2016))

The study [..104 ]is then carried out as a sensitivity analysis, where the effects of different steady yaw misalignment angles between -30 and 30 degrees [..105 ]are evaluated in terms of turbine fatigue, ultimate loads and maximum blade tip deflections.

The 10 MW INNWIND.EU model, implemented through the software `Cp-Lambda`, was subjected to the full list of DLCs described in Tab. 1. As already explained in Sec. 1, DLC6.n series was simulated only for the reference turbine (i.e. without misalignment), whereas DLC1.n and 2.n for reference and for other four different yaw misalignment angles ($\pm 15$, $\pm 30$ deg).

[..106 ]Once all load conditions have been calculated for each yaw angle, ultimate values are extracted for each wind turbine sub-component, having previously considered the relative safety factor as defined in Table 1. As explained above, the DLC6.n are computed only for the baseline case, but maximum load and blade tip displacement values coming from those cases are included also in the ranking related to all misalignment angles.

As an example of this analysis, figure 2 shows in the top plots the ultimate load increment at different yaw angles for the blade root combined moment (left) and for the tower base combined moment (right). The text above each bar indicates the DLC which has generated such maximum loads. In terms of blade, the effect of yaw misalignment is limited with just a small increase of about 1% at 30 deg. [..107 ]Tower loading seems to suffer a bit more at high misalignment angles with an increase of 7.5% at 30 deg[..108 ], due to a strong increment in the maximum load experienced in DLC1.4. On the other side, at lower angles, the ultimate value stays the same as it occurred in parking condition (DLC6.2), no matter of the presence of the farm control.

[..110 ]Similarly, the misalignment angle of 30 deg is associated also to an increase of [..111 ]about 6% [..112 ]of the maximum blade tip displacement (see bottom plot of Fig. [..113 ]2). This increment, although apparently small, deserves a special attention. In fact, often, the blade design is constrained by the maximum blade tip deflection which is to be bounded in order to avoid dramatic blade-tower collision. Since the maximum tip deflection typically enters in the design process as a constraint, it is possible that even a small increment of this value may lead to a violation of this constrain and in turn to the need of a blade redesign. [..114 ]In this specific case, the maximum blade deflection occurred during the DLC1.4, i.e. during the ECD gust (*Extreme Coherent gust with Direction change*), where an increase of the wind speed is coupled with a

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104 removed: in

105 removed: on turbine fatigueand ultimate loads have been evaluated

106 removed: Once all load conditions have been calculated for each yaw angle, it is possible to extract the maximum loads for each wind turbine sub-component, having previously considered the relative safety factor as defined in Table 1. As explained above, the DLC6.n are computed only for the baseline case, but are included also for the other angles. As an example of this analysis, figure ?? shows the

107 removed: Loading on tower

108 removed: , while at lower angles it does not change because caused by the parking conditions DLC6.2.

110 removed: The analysis of blade tip displacement, on the other hand, shows

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114 removed: In this specific case, this maximum blade deflection has been obtained during the DLC1.4, i.e. during the ECD gust (*Extreme Coherent gust with Direction change*), where an increase of the wind speed is coupled with a direction change. This combination causes the yawed rotor to experience a much higher axial wind when the rotor itself is tilted in the direction the gust is coming from.
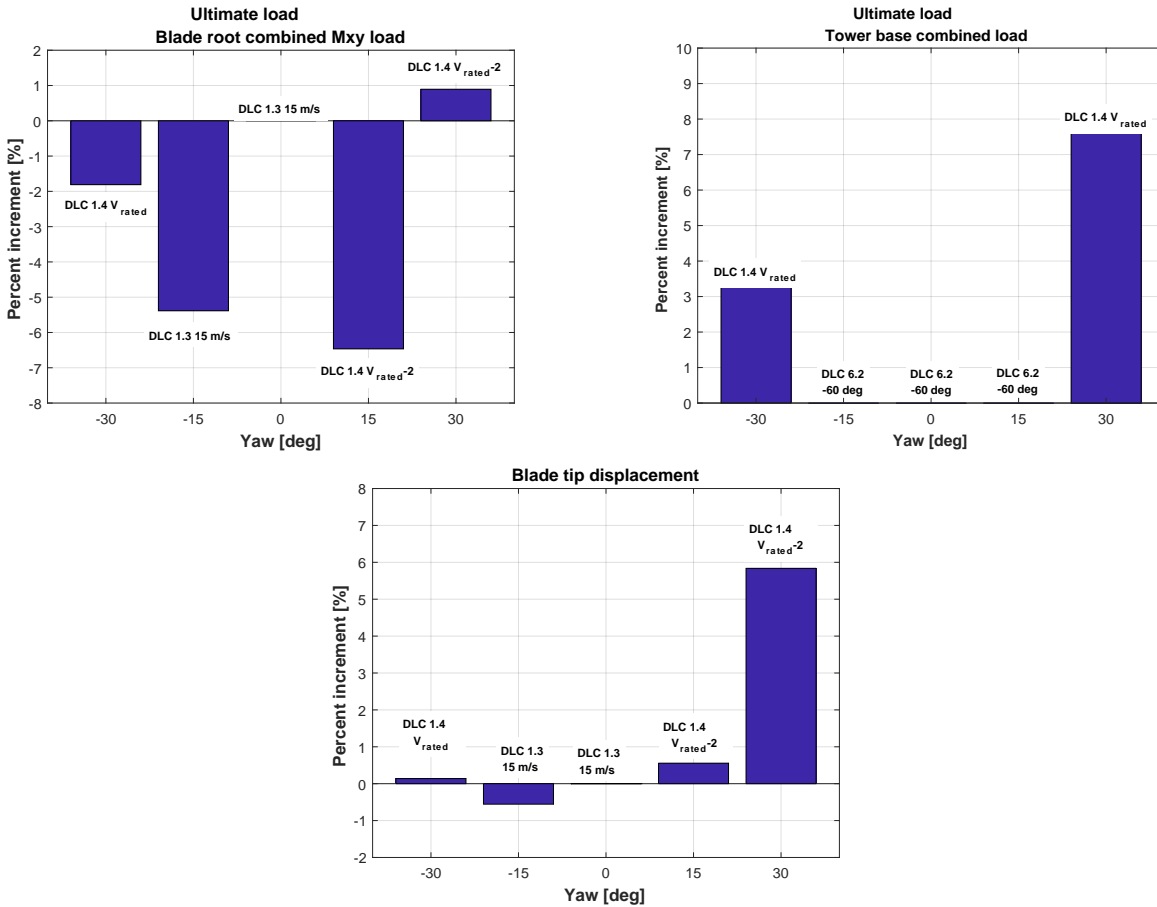
**Figure 2.** Comparison of ultimate loads and maximum tip deflection. [..[109] ]Top-left plot
: blade root combined moment. Top-right plot: tower base combined moment. Bottom plot: maximum blade tip displacement.

265  direction change. This combination causes the rotor to experience a much higher axial wind anytime the rotor itself is
initially oriented as the direction the gust is coming from.

[..[115] ]

[..[116] ]

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[115]removed: Comparison of maximum blade tip displacement (left) and of Annual Energy Production (AEP) (right).

[116]removed: From the same analysis, and in particular from DLC1.2 it is possible to estimate other Key Performance Indicators (KPIs). For instance, Fig. **??**
on the right shows the AEP reduction for the different yaw angles.As one can see, the single wind turbine may experience a loss up 18% at -30 deg. This result
is already known to the scientific community and is generally balanced by the increase in power of the downstream wind turbine(s). In terms of actuator duty
cycle, estimated in these

Finally, fatigue analysis is carried on on the basis of DLC1.2[..[117] ]. Even if such analysis would require a more so-
phisticated approach, possibly, including all turbines in a farm, we briefly present here the direct effect of the wind farm
controller on damage equivalent load (DEL) of the first-row wind turbine, i.e. the yawed one.

[..[118] ]The plot on the left of Fig. 3 shows the blade root flap-wise DEL increment associated to the wake redirection for
different yaw angles. [..[119] ]All DELs have been computed in power production with turbulent wind from the cut-in to the cut-
out wind speed (DLC1.2) and then weighted with the Weibull probability function for a class IA (IEC 61400-1 Ed.3., 2004). In
this analysis, and in the following ones, an equivalent frequency corresponding to 10M cycles in 20 years has been considered.
Moreover, [..[120] ]$m = 10$ and $m = 3$ have been used as inverse SN-curve slope (i.e. Wöhler exponent) values[..[121] ], for
composite blades and [..[122] ]steel tower, respectively. It is important to stress here that only for wind speed lower than 15 m/s
the wind farm controller (i.e. the wake steering) is active, so that at higher wind speeds there is no difference between the [..[123]
]performance of baseline and wind-farm-controlled ones. As a side remark, limit the activity of the farm control to 15 m/s is
reasonable for controllers aimed at maximizing the power production. It is however possible to have a farm control activity also
beyond this wind speed for downstream turbine fatigue mitigation, as proposed in Urbán et al. (2018). The same figure [..[124]
]shows that the overall effect of the yaw misalignment on the cumulated DEL is limited, with an increase of slightly more than
3% at −15 deg. The reduction experienced in most of the positive misalignment range is due to the coupling between vertical
shear layer and lateral flow velocity induced by yaw misalignment. In fact, vertical shear layer increases the blade loads when
it is upward and decreases them when downward, generating a load oscillation at the rotor frequency. A lateral component of
the wind is similarly responsible for oscillating loads, but with the difference that the increment may occur when the blade is
upward or downward depending on weather the misalignment angle is positive or negative. As a consequence, the impact of
yaw misalignment may be summed up to or subtracted from the one of the shear layer. This behaviour is not new, as was also
analyzed [..[125] ]in (Boorsma, 2012; Ennis et al., 2018).

The plot on the right of Fig. 3 shows the increment in the maximum directional DEL for tower base as function of the
yaw angle. [..[126] ]In this case these DELs have been computed looking for the worst direction as typically done for axial-
symmetric structures. Again, operating in yawed condition (for wind speed below 15m/s) does not seem critical in terms of
fatigue for the tower base.

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[117]removed: simulations, the wake redirection does not seem problematic. In fact, when a turbine operates in yawed condition, it experience a lower axial
wind . This makes the turbine working in below-rated region, with limited pitch activity, for a higher amount of time.A quantitative evaluation shows a decrease
of 41% in ADC for a misalignment of 30 deg.

[118]removed: Finally, DLC1.2 can be used to estimate fatigue loads. Even if these are not the goal of this work, and their estimation require a deep analysis,
where one also has to consider the inner wind turbines, the wind farm layout, etc., we present here the direct effect of the wind farm controller on this first-raw
wind turbine, i.e. the yawed one.

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[120]removed: the following

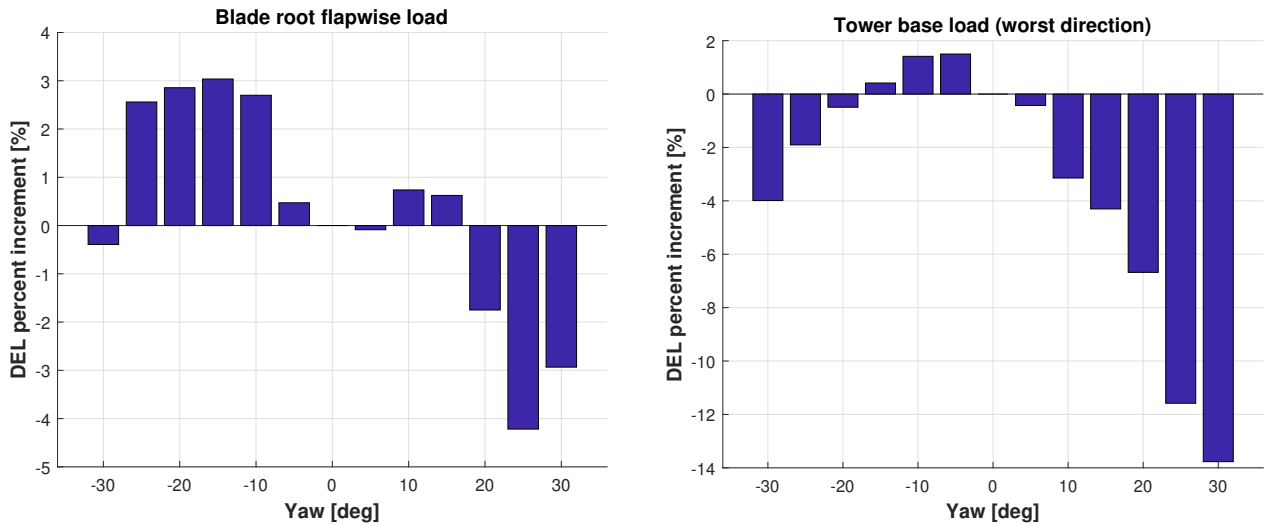[121]removed: have been considered: $m = 10$ for the

[122]removed: $m = 3$ for the steel tower. It's

[123]removed: baseline and the

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[125]removed: , for instance,

[126]removed: In this case these DELs have been computed looking for the worst direction as typically done for axial-symmetric structures.

**Figure 3.** Comparison of blade root flap-wise DEL (left) and tower base maximum directional DEL (right).

By looking at these results, one may also conclude that avoiding operating at very high misalignment (i.e. at 30 deg) may
295  be beneficial. In fact, up to $\pm15$ deg, the increment of [..[127] ]ultimate loads and blade deflections seems essentially limited.
[..[128] ]The sensitivity analysis shown in this section allows [..[129] ]the designer to also estimate the extreme parameters of this
wind farm control [..[130] ]technique to be applied to already existing wind farms. These limits are defined by the design loads
of the single wind turbine: the wind farm operators may apply [..[131] ]a specific farm controller as far as the [..[132] ]induced
loads do not exceed the design ones.

300  Clearly, this last consideration is not utterly new. In fact, most of the field testings, which have been conducted so far (cf.
Fleming et al. (2019)), considered only one-sided wake steering. This practice can be useful to cope with the increased
loading expected for specific range of misalignment angles. In a broader sense, one may even think that the conditions,
to be avoided because considered critical in terms of loading, might comprise complex combinations of speeds, TI levels,
yaw angles and shear layers.

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[132]removed: loads induced by this technology do not overtake

## 4.2 Evaluation of the impact of dynamic induction control

### 4.2.1 Review of dynamic induction control

Another interesting means of increasing the total wind farm power consists in the so-called Dynamic Induction Control (DIC). Specifically, the upstream wind turbine, when its wake impinges on a downstream machine, modulates the thrust in a periodic way. The modulation can be performed by pitching collectively or cyclically the blades at a specific frequency or by changing the rotor speed. Clearly, the most effective action is to enforce a Periodic Collective Motion (PCM) of the blade pitch angles. The effect of the PCM is to dynamically vary the induction of the rotor and, hence, to increase the mixing level inside the wake. The wake itself results to be energized by such fluctuating induction and recovers in a faster way. [..[133]]DIC was recently studied through CFD simulations (Munters and Meyers, 2017, 2018) and validated in a scaled wind tunnel experimental campaign (Frederik et al. (2020b)).

The DIC technique studied here is a pure PCM at a single frequency, as described by

$$\beta_{\mathrm{PCM}} = A_{\mathrm{PCM}} \sin\left(2\pi f_{\mathrm{PCM}} t + \varphi_{\mathrm{PCM}}\right), \tag{1}$$

where $\beta_{\mathrm{PCM}}$ is the pitch setting imposed by PCM to be summed up to the pitch of the trimmer, $A_{\mathrm{PCM}}$ is the related amplitude, $f_{\mathrm{PCM}}$ the frequency, $t$ the time and $\varphi_{\mathrm{PCM}}$ the possible phase.

Despite the limited number of studies devoted to PCM, especially if compared with the amount of literature available about wake redirection technique, it is already possible to highlight some important concepts:

- PCM seems effective in increasing the total wind farm power output by some percent, as demonstrated by both simulations and wind tunnel experimentation.

- The increase in wind farm power depends strongly on the amplitude and frequency of the rotor thrust variation.

- Rather than in terms of frequency $f$, the effect of the PCM technique is to be viewed in terms of the dimensionless Strouhal number $S_t$, defined as

$$S_t = \frac{f_{\mathrm{PCM}} D}{U_\infty}, \tag{2}$$

  being $D$ the rotor diameter and $U_\infty$ the undisturbed wind velocity.

- The optimal Strouhal number was found to be 0.25 in CFD simulation (see Munters and Meyers (2018)), whereas in wind tunnel it was possible to verify significant power increases in a wider range between 0.17 and 0.45 (see Frederik et al. (2020b)).

### 4.2.2 Effect of PCM amplitude and Strouhal number on turbine loading

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[133]removed: This technique

[..[134] ]In order to perform a detailed analysis concerning the ultimate loads, different combinations of amplitude $\beta_{\mathrm{PCM}}$ and Strouhal number $S_t$ were considered: the range in amplitude was set between 1 and 4 deg, whereas the range of Strouhal between 0.2 and 0.5, according to the findings of an experimental campaign in wind tunnel (see Frederik et al. (2020b)).

335     It was primarily observed that the phase of the oscillation $\varphi_{\mathrm{PCM}}$ is of paramount importance. Consider for example the set of DLCs including extreme conditions. By chance, it is possible that [..[135] ]a particular extreme event, like a gust or a fault, occurs at a time in which the PCM control is increasing the collective pitch, thereby reducing the rotor loading. In this case, the peak of the load involved by the extreme event could be smoothed. Conversely, if the extreme event had occurred in correspondence of a decrease of the collective pitch, the effect of the control would have been that of increasing the load. This

340 is due to the difference between the characteristic time of these extreme events (a few seconds) with respect to the PCM period (tens of seconds). For this reason, in order to find the worst case, i.e. that condition which maximizes the increase of the load, 8 different 45-deg-spaced phases have been considered. Consequently, the full set of DLCs in Table 1 were simulated, for each couple of amplitude-Strouhal, eight times, by varying the [..[136] ]phase $\varphi_{\mathrm{PCM}}$.

    [..[137] ]Following the same analyses of Section 4.1, it is possible to quantify the effects of this control technique, extract-

345 ing, for each combination of Strouhal number and pitch amplitude, the maximum loads in the wind turbine sub-components of interest.

    Figure 4 shows the ranking of DLC generating the highest peak load (including the related safety factor as reported in Tab. 1) for blade root flap-wise moment without PCM (left) and with a PCM control characterizing by $S_t = 0.5$ and $\beta_{\mathrm{PCM}} = 2$ deg (right). The ultimate loads is generated in a DLC1.3 (extreme turbulence conditions) at 15 m/s and the PCM has the effect of

350 increasing this load of about 6%.

    A different situation is experienced for tower base combined load, reported in Fig. 5. The two subplots are organized as in the previous case. The first place in the ranking is taken by a case in which the PCM is not active, DLC6.2 (right plot). When the PCM is active (right plot), the DLC1.4 at $V_r$ increases its position in the ranking, from the $4^{th}$ to the $3^{rd}$ but it is not enough to get to the first position. From this discussion one can conclude that the effect of PCM is null in terms of tower base fore-aft

355 ultimate load.

    Figure 6 shows the percentage increment for different combinations of Strouhal number and amplitude for blade root combined moment (up left) and tower base combined moment (up right) and hub combined moment (bottom). Above each bar, a text indicates the DLC which has generated that maximum load. Significant increases are only associated to blade loads, whereas hub and tower result to be not affected by PCM.

360     A sensitivity analysis was also conducted so as to compute the variation of maximum blade tip displacement. An increase up to $12\%$ is measured for $\beta_{\mathrm{PCM}} = 4$ deg, as shown in Fig. 7. This indication is extremely important as the maximum tip deflection

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[134]removed: In order to perform a detailed analysis concerning the ultimate loads,

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[137]removed: Following the same analyses of Section 4.1, i.e. extracting for each combination of Strouhal number and pitch amplitude, the maximum loads in the wind turbine sub-components, it is possible to quantify the effects of this control technique.
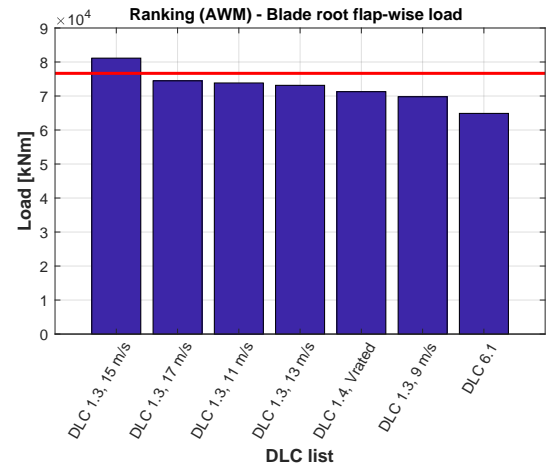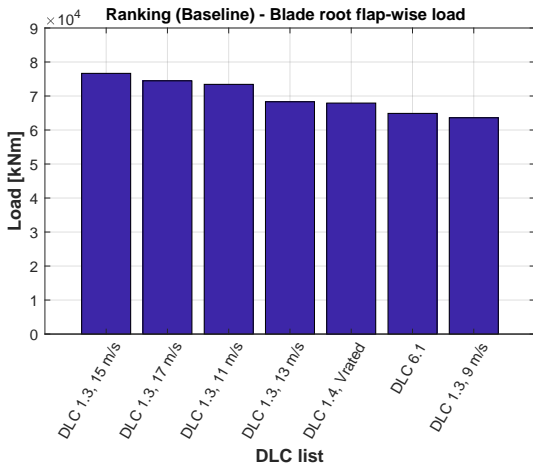
**Figure 4.** Ranking of ultimate loads for blade root flap-wise load for baseline, right, and PCM, left, in the case of $S_t = 0.5$ and $\beta_{\mathrm{PCM}} = 2$ deg. Red line: baseline ultimate load.
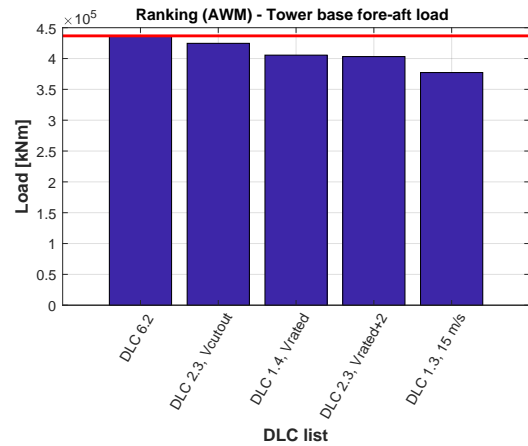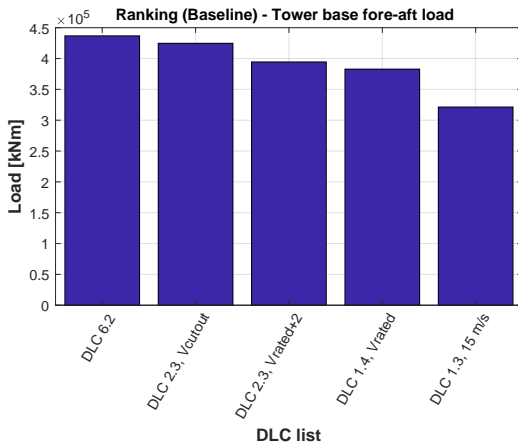


**Figure 5.** Ranking of ultimate loads for blade root flap-wise load for baseline, right, and PCM, left, in the case of $S_t = 0.5$ and $\beta_{\mathrm{PCM}} = 2$ deg. Red line: baseline ultimate load.

typically enters as an active constraint into the design of the blade, affecting the thickness of its structural elements[..[138] ], as already seen for the wake redirection technique. If one excludes the highest PCM amplitude (i.e. 4 deg), the maximum tip deflection increases only of 3% which may correspond to a lower impact on blade design.

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[138]removed: , as already seen for the wake redirection technique
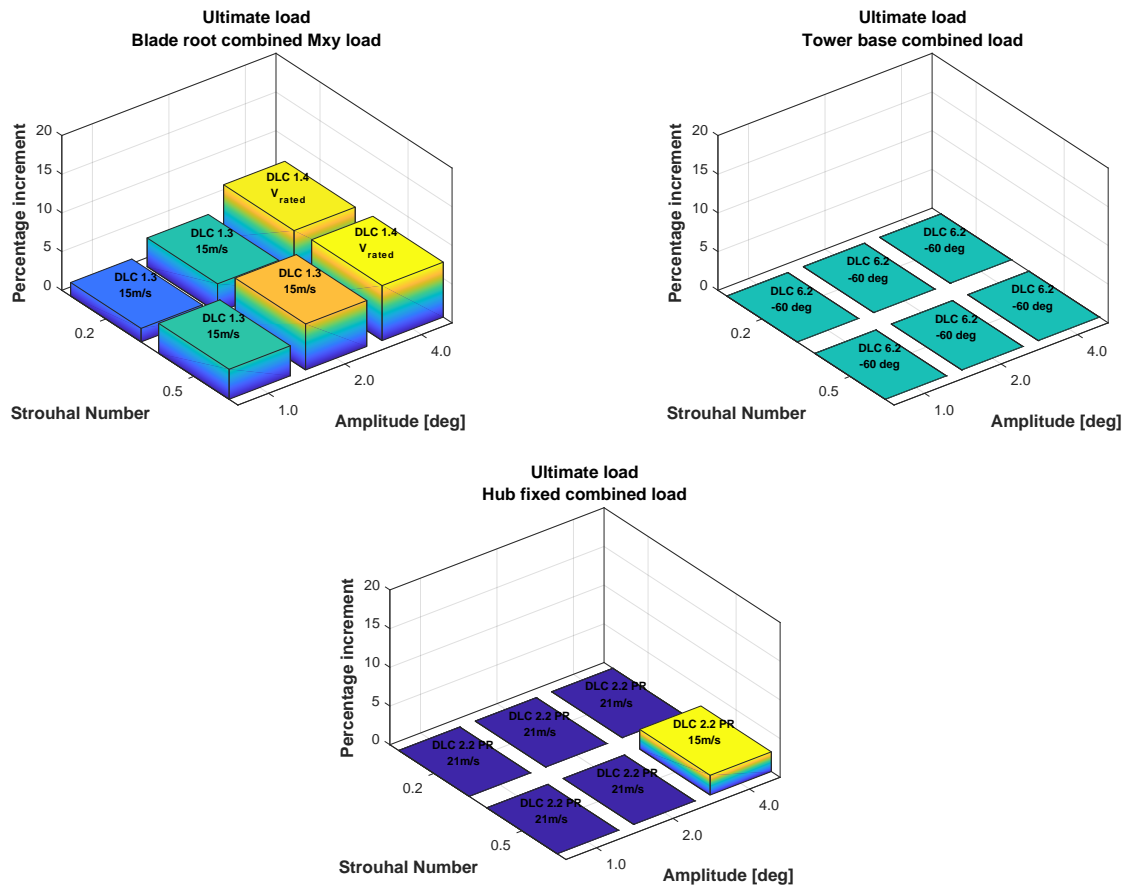
**Figure 6.** Maximum load increases as function of amplitude and Strouhal number. Up-left: blade root combined moment. Up-right: tower base combined moment. Bottom: hub combined moment.

365    [..[139] ]

[..[140] ]From DLC1.2 it is also possible to estimate the Actuator Duty Cycle (ADC) [..[141] ]and the impact that PCM may have on it. Especially in the context of PCM, this indicator is important as the pitch ADC may be a driving input for the actuator design. Considering $S_t = 0.5$ and full year operation, the increase of the ADC results equal to 77% and 143% respectively for $\beta_{\mathrm{PCM}} = 2$ and $\beta_{\mathrm{PCM}} = 4$ [..[142] ]deg. Such numbers appear rather high but, since they refer to full year

370    operation with farm control, they have to be considered as maximum limits. Clearly, a turbine is expected to operate only

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[139]removed: From DLC1.2 it is possible to estimate AEP, ADC and fatigue loads, again under the assumption that PCM is active only below 15 m/s. The loss of AEP of the upstream wind turbine results very low. As example, the case of $\beta_{\mathrm{PCM}} = 2$ deg and $S_t = 0.5$ is associate to a loss of AEP equal to 0.5%. On the other hand, considering a higher amplitude, $\beta_{\mathrm{PCM}} = 4$, the decrease of AEP results 2.2%.

[140]removed: Dealing with the

[141]removed: , the effect of PCMis way more significant. In particular, considering

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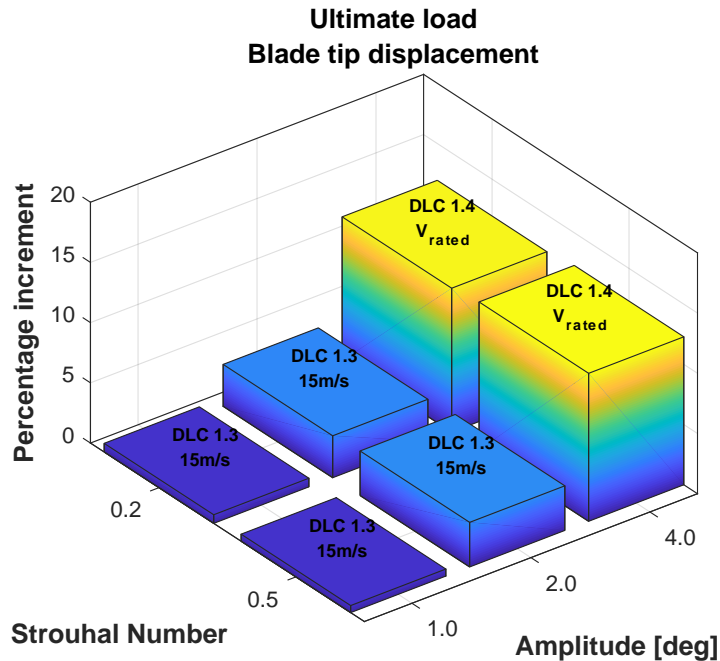
**Figure 7.** Blade tip maximum displacement increase as function of amplitude and Strouhal number.

part of its life following wind farm control inputs. Consequently, the increase in ADC is to be scaled down according to the actual time spent with PCM active.

Finally, figure 8 shows the percentage DEL increment for the different combination of Strouhal number and amplitude for blade root flap-wise (left) and tower base (right). As expected, the highest increases are associated to larger pitch amplitudes and higher Strouhal numbers.

For both blade flap-wise and tower base, the effects are significant and may amount to 20% and 30%, respectively, in the worst cases ($\beta_{\mathrm{PCM}} = 4$ and $S_t = 0.5$). However, if one excludes the highest amplitude limiting the authority of PCM to 2 deg, the detrimental effect of PCM in terms of fatigue seems acceptable, being equal to about 10% for both loads.

Particular attention should be devoted to the impact of PCM on downstream rotor loading. The change of thrust, in fact, results in a higher in-wake velocity, but also creates a low frequency flow travelling downwind. The impact of such a pulsating flow with downstream machines can be significant in terms of turbine loads and aero-servo-elasticity. This particular study, out of the scope of the present paper, is currently under investigation, and preliminary results are available in Cacciola et al. (2020).

## 4.3 Comparison between periodic collective motion and wake redirection for the 10 MW INNWIND.EU turbine
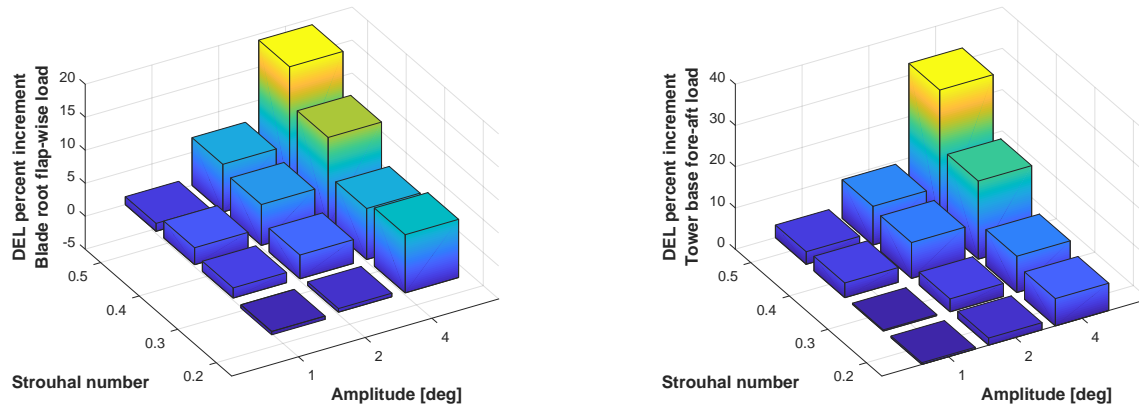
**Figure 8.** Weibull weighted DEL increases as function of amplitude and Strouhal number. Left: blade root flap-wise moment. Right: tower base F-A moment.

385  [..[143] ]To summarize the previous results, Table 2 shows a comparison between the worst cases of WR control and PCM for this 10 MW INNWIND.EU turbine.

**Table 2.** Comparison of worst cases (PCM vs WR)

| | PCM | | WR |
|---|---|---|---|
| | $A_\mathrm{PCM} = 2$ deg | $A_\mathrm{PCM} = 4$ deg | |
| Ultimate blade root combined | +5.9 % | +7.1 % | +1.0 % (at 30 deg) |
| Ultimate tower base combined | 0 % | 0 % | +7.9 % (at 30 deg) |
| Ultimate hub combined | 0 % | 2.5 % | 0 % |
| Max tip deflection | 3 % | 12.3 % | 5.8 % (at 15 deg) |
| [..[144] ][..[145] ][..[146] ][..[147] ][..[148] ][..[149] ][..[150] ][..[151] ]DEL blade flap (full year operations) | +7.2 % | +19.9 % | +3.5 % (at 30 deg) |
| DEL tower base fore-aft (full year operations) | +9.4 % | +32.9 % | +0.7 % (at 30 deg) |
| DEL hub (full year operations) | +1 % | +1 % | $\approx 0$ % (at 30 deg) |

At first sight, PCM control with amplitude of 4 deg appears to be extremely impacting in terms of ultimate loads and blade deflections, with an increase of more than 10% in the maximum tip displacement which could be considered excessive, at least for the present machine whose design is constrained by this value. [..[152] ]Excluding the previous case, the impact in terms

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[143]removed: To summarize the previous results,

[152]removed: Excluding the previous case, the impact in terms of fatigue, computed for the first-raw wind turbine, appears limited for both control techniques, especially if one considers the assumption that the wind farm control is always active no matter of the wind direction and TI. As noted in Zalkind and Pao (2016), in realistic farms, the amount of time spent with non-null inputs coming from the farm control layer can be rather small, yielding an even lower impact on fatigue.

390 of fatigue, computed for the first-row wind turbine, appears limited for both control techniques, especially if one considers the assumption that the wind farm control is always active no matter of the wind direction and TI. As noted in Zalkind and Pao (2016), in realistic farms, the amount of time spent with non-null inputs coming from the farm control layer can be rather small, yielding an even lower impact on fatigue.

If one considers, on the other hand, only the PCM with amplitude of 2 deg, the impact of PCM and WR becomes comparable,
395 even though the latter seems less impacting especially for fatigue. In terms of ultimate loads, PCM has a higher impact on blade loads and null on tower, while the opposite happens for blade redirection.

Maximum tip deflection needs a special attention as both control techniques entail a significant increase in this quantity. In fact, for a typical glass-fiber blade, the blade-to-tower clearance is often an active constraint of the structural design (Sartori, 2019; Bortolotti et al., 2019; Sartori et al., 2020). Moreover, [..[153] ]the load case [..[154] ]associated to this ultimate displacement
400 is DLC1.4 [..[155] ](ECD), that is a deterministic wind case. This suggests that an ECD may happen regardless of the turbulence intensity which justifies, at least for the present study, the initial choice of neglecting a dependency between the TI and the activation of the wind farm controller.

## 4.4 Evaluation of the impact of wind farm control on rotor design

In the previous sections, different wind farm control strategies have been analyzed with the aim of computing the related effect
405 on wind turbine ultimate loads, as well as on other important design parameters, such as the maximum blade deflection and actuator duty cycles. The performed analyses showed that WR and PCM have an impact on [..[156] ]both ultimate loads and maximum tip deflection[..[157] ]. The latter, in particular, is a typical [..[158] ]driver for blades [..[159] ]design, meaning that the maximum blade tip displacement is severely enforced in the design process in order to maintain a suitable clearance between [..[160] ]the tip of the blades and the tower.

410 For this reason, this Section on the design can be considered as the subsequent step with respect to the previous sensitivity [..[161] ]analysis. The goal here is to quantify the possible modifications on the structural design of the blade when the wind farm control is considered. Possible increase in blade mass and turbine cost will be considered as concise indicators of the impact of wind farm control on blade design. Since the focus of this study is on the macroscopic impact of wind farm controllers on the design rather than to provide a fully-feasible structural layout, we limited our analysis to the aero-elastic optimization
415 loop of Fig 1. Moreover, in order to perform a [..[162] ]fair comparison where the effects of the sole wind farm control are highlighted, all redesigned rotors should be "optimal", in the sense that they should be all coming from an equal optimal

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[162]removed: neat

design process characterized by the very same cost function and constraints, otherwise, it would be impossible to split the effects of the wind farm controller from those of the specific optimization strategy in the final comparison. To this end, the reference INNWIND.EU 10 MW wind turbine is firstly redesigned with `Cp-Max` following the procedure described in Sec. 3, yielding the "baseline" rotor. Then, the baseline configuration will be updated by the same optimization process but including this time the presence of the wind farm control.

[..[163] ]

The design process of the baseline generated an optimal solution compliant to all optimization constraints, with a structure mildly different with respect to the nominal INNWIND.EU. [..[164] ]

Fatigue loads deserve also a special attention. It is well known that fatigue loads are critical to the design of a wind turbine and hence are included in the design of the "baseline" rotor, resulting in a blade whose sub-components (especially reinforcements and shear webs) are also sized for fatigue. When one has to consider also the wind farm controllers, as discussed in the previous sections, the fatigue load analysis depends heavily on the wind direction, on the TI, and other factors. Additionally, the sensitivity analyses performed previously for the front-row wind turbine have shown that the impact in terms of fatigue appears limited, even if considering that the wind farm control is always active. In realistic farms, the amount of time spent with non-null inputs coming from the farm control layer can be rather small, yielding an even lower impact on fatigue. For these reasons, in the process of rotor re-design, the fatigue loads, usually included and updated in the `Cp-Max` environment, are kept frozen and equal to those of the baseline case. Again, this approach allows for better highlighting the impact of the sole ultimate loads due to wind farm controllers on rotor design.

In this section, only the PCM [..[165] ]with $S_t = 0.5$ and $\beta_{\mathrm{PCM}} = 2$ deg [..[166] ]will be considered for the redesign. In Sartori et al. (2020) is reported a rotor design comparison which includes also the WR control.

Focusing only on the $\beta_{\mathrm{PCM}} = 2$ deg seems reasonable, since $\beta_{\mathrm{PCM}} = 4$ deg is associated to an excessive increment in the turbine loading status, as reported in Tab. 2. Moreover, this choice is further justified by the results of a previous experimentation in wind tunnel with a simple three-turbine farm (Frederik et al., 2020b). In that campaign, the amplitude of the PCM associated to the highest increase of overall farm power output resulted equal to 1.7 deg, value rather close to that used in the present work.

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[163]removed: Fatigue loads deserve also here a special attention. It's well known that fatigue loads are fundamental for the design of a wind turbine and hence are included in the design on the "baseline" rotor according to the Standards, thus obtaining a blade whose sub-components (especially reinforcements and shear webs) are also sized for fatigue. When one has to consider also the wind farm controllers, as discussed in the previous sections, these fatigue load analysis depend heavily on the wind direction, on the TI, etc.. Moreover, the above sensitivity analyses computed on the front-row wind turbine under the hypothesis the wind farm control is always active, have showed that he impact of these fatigue loads appear limited. In realistic farms, the amount of time spent with non-null inputs coming from the farm control layer can be rather small, yielding an even lower impact on fatigue. For these reasons, in this re-design of the rotor, the fatigue analysis is also simplified and the fatigue loads, usually included in the `Cp-Max` environment, are kept frozen and equal to those of the baseline case. Again, this approach allows for better highlighting of the impact on just the ultimate loads generated by the wind farm controllers on the rotor design.

[164]removed: Hence, for the sake of brevity, the related detailed analysis is not reported in this manuscript. For the same reason,

[165]removed: , characterized by

[166]removed: , as been considered here, while in

The structural optimization was then [..[167] ]performed by taking into account both the standard DLCs set from Table 1 and all the DLCs in which the turbine is controlled with the PCM. Different phase angles of the PCM were included in the ultimate loads/displacements analysis. Once again, the entire set of DLCs was re-computed at each structural iteration to make sure that, as the structural design evolves, the loads are updated accordingly.

The main results of the redesigned rotor with the PCM are summarized in Table 3. As shown, the introduction of the wind farm controller leads to an overall deterioration of all key performance indicators. It must be stressed, however, that all indicators refer to the individual, front-row, turbine as the current release of `Cp-Max` implements a turbine-specific cost model and a proper assessment of the impact of the PCM on the cost of energy should be evaluated at wind farm-level.

**Table 3.** Comparison between the KPIs of the Baseline 10 MW and the redesigned rotor.

| Performance | Baseline 10 MW | Redesign PCM | Variation |
|---|---|---|---|
| Blade mass | 40643 kg | 45436 kg | +11.8% |
| Single wind turbine [..[168] ][..[169] ][..[170] ][..[171] ][..[172] ]CoE | 89.42 EUR/MWh | 90.22 EUR/MWh | +0.89% |

[..[173] ]

A complete comparison of the ultimate loads of the Redesign PCM rotor against the Baseline 10MW is also given in Fig. 9[..[174] ], in witch all the loads are made [..[175] ]dimension-less through the corresponding values of the Baseline 10MW. Here, `flp` identifies flap-wise, `edg` is edgewise, `trs` is torsion, `thr` is thrust, `nod` is nodding, `yaw` is yawing, `FA` and `SS` are, respectively, fore-aft and side-side loads, and, finally, the tag *cmb* identifies multi-directional combined loads. From the diagram it is possible to notice how the blade loads are globally increased by the combination of PCM and higher blade mass. When it comes to the other sub-components, however, the impact is mixed. On one side, the side-side and the torsion at the tower base are slightly increased, while the fore-aft is significantly reduced. Based on this limited analysis, then, it is possible to conclude that the introduction of the PCM as a wind farm controller would require a redesign of the rotor but, likely, would not affect the structural integrity of [..[176] ]hub and tower.

[..[177] ]

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[167]removed: repeated

[173]removed: Concerning the aerodynamic performance, Table 3 shows that only a slight deterioration of the AEP is expected when the PCM is used. This is mainly due to the collective pitch motion imposed in the partial-loading range of the power curve, which results in the collective pitch of the blades being cyclically driven away from their theoretical optimum value. This is confirmed by looking at the time-averaged turbulent power curve given in Fig. **??** (left) and the corresponding power coefficient (right). However, this detrimental influence is partially compensated by the increased stiffness of the blades which contribute to preserve the AEP by reducing the deformations experienced by the rotor. Another important feature of the PCM is the increase of Actuator Duty Cycle (see Fig. 9 (left)), which is a direct consequence of the increased service time required to the pitch actuators.
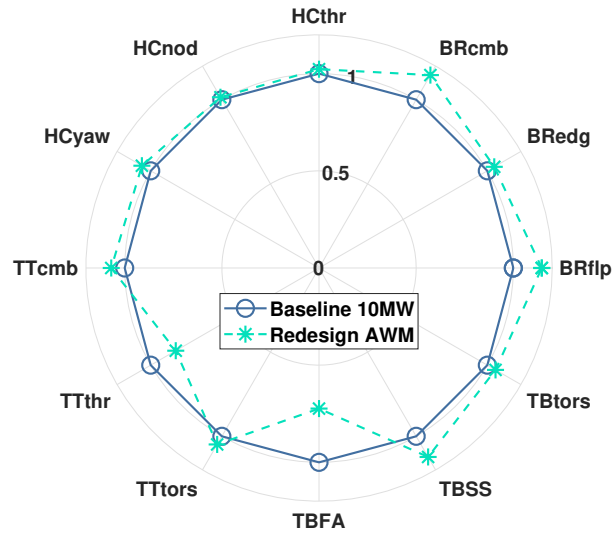
[174]removed: (right)

[175]removed: non-dimesional with

[176]removed: the hub and the

[177]removed: Redesign process including PCM. Left plot: time-averaged turbulent power curve. Right plot: power coefficient.

**Figure 9.** [..[178] ]Ultimate loads resulting after the redesign process including PCM. [..[179] ]'BR' is blade root, 'HC' is hub center, 'TT' is tower top and TB is tower base

From a structural perspective, as expected, the introduction of the PCM resulted in an about 12% higher blade mass. This result comes from a combination of the above higher loads and higher displacements introduced by the wind farm controller. Specifically, the increased blade deflection required a heavy redesign of the spar caps in order to avoid the violation of the constraint [..[180] ]related to the maximum blade tip displacement. The optimal distribution of spar cap thickness is shown for both the baseline and the redesigned rotor in Fig. 10. It is worth [..[181] ]mentioning that, due to the increased flap-wise stiffness, at the end of the optimization, the maximum displacement of the redesigned rotor is almost identical to that of the Baseline and, most importantly, it does not exceed the allowed [..[182] ]blade-tower clearance.
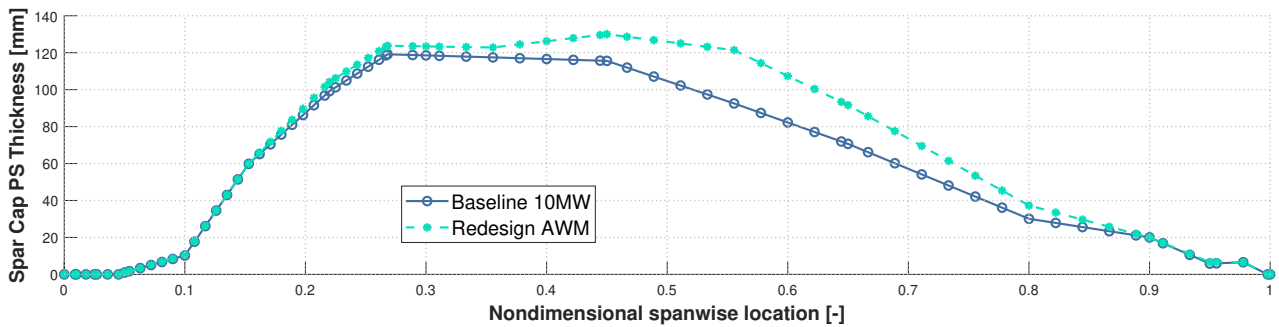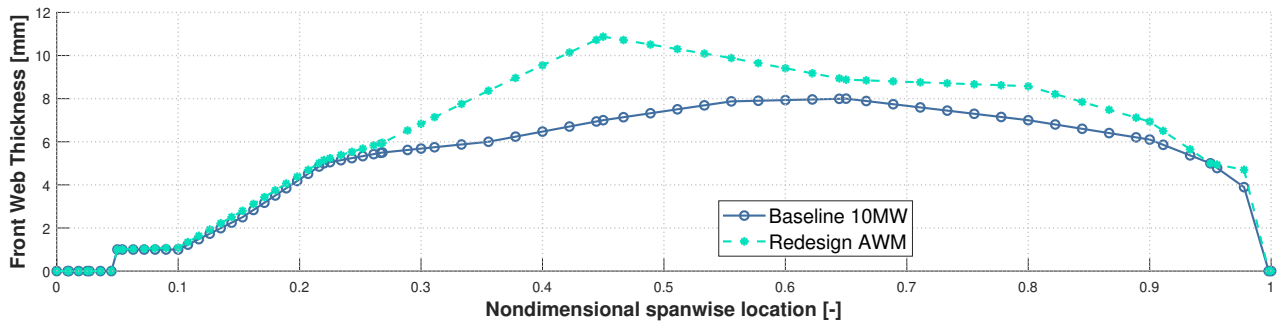


**Figure 10.** Redesign process including PCM: thickness distribution of the spar caps.

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[180]removed: on the maximum

[181]removed: to mention

[182]removed: tower

**Figure 11.** Redesign process including PCM: thickness distribution of the shear webs.

Qualitatively similar results have been obtained in the redesign process for the WR case, which was performed in
Sartori et al. (2020). The blade redesigned under the WR control was characterized by thicker spars and webs, and,
in turn, blade mass increased by 12.6%. Also in this case, the update of the structural elements was mainly needed to
compensate for the increase in the maximum tip deflection, which was experienced in DLC 1.4 for very high misalignment
angles (cf. Fig. 2).

## 5 Conclusion and Outlook

In this paper, a procedure to evaluate the effects of wind farm control techniques on a single wind turbine has been developed.
Two different control methods (dynamic induction control and the wake redirection) have been considered and tested on a
reference 10 MW wind turbine. The study is conducted by simulating [..[183] ]the main Design Load Cases prescribed by
the Standards with the inclusion of the chosen wind farm control. In this strategy, an explicit dependency of the wind farm
control on the turbulence intensity was neglected, whereas the value of turbulence intensity was always defined according to
the turbine's class. Although this limits the validity of the conclusions to the turbine under investigation, it allows to obtain
results which are compatible with current Standards, and which are not site-specific.

The study has been performed through two steps. At first, the impact of the controls is evaluated in terms of the turbine KPIs
(maximum loads, maximum blade tip deflection, AEP, ADC). The study has been conducted as a sensitivity analysis where all
indicators are computed as functions of the wind farm control parameters. At this step, we were able to quantify the impact
of the control techniques on the performance of an existing turbine and, at the same time, to define the operational limits of
the wind farm controller to not exceed the original load spectra. In a second step, a dedicated structural redesign of the rotor
has been performed in order to quantify how much the design would have changed if a wind farm control had been considered
from the beginning.

From the analyses performed in this work the following conclusions can be derived:

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[183]removed: the main Design Load Cases prescribed by the Standards with the inclusion of the

- The most impacting control seems to be the one based on the dynamic induction, especially if higher amplitudes of the blade pitch angles are considered. However, if the amplitude is maintained below 2 deg, the potential increase in fatigue is limited.

- Tower ultimate loads are particularly affected by wake redirection, with the ECD condition being the most impacting DLC.

- The blade loads, on the other hand, are mostly affected by dynamic induction control.

- Both controls lead to an increase in the maximum tip displacements. Since the turbine considered in this study is heavily constrained by tip deflection, this results in a significant mass increase when the rotor is redesigned. It must be noticed that different design concepts (or materials) could result in different sizing loads and, therefore, to different impacts on the redesign.

- The redesign process, due to the above mentioned higher blade deflection, led to an increased rotor mass. [..[184] ]

- In this study, focused on maximum loads, a simplified fatigue load assessment was also made. The impact of these fatigue loads, computed for the first-row wind turbine under the hypothesis the wind farm control is always active, no matter the wind direction and TI, is limited but not negligible. However, in realistic farms, the amount of time spent with non-null inputs coming from the farm control layer can be rather small, yielding an even lower impact on fatigue.

It is important to stress that these findings only apply to the considered 10 MW wind turbine, and may be different for other machines. The parametric analyses and the design process have considered only the front-row wind turbine and, hence, the obtained results cannot be viewed as conclusive unless downstream turbines, together with the wind farm layout and wind rose, are included in the procedure. However, the proposed design provides an important indication on the potential impact of farm controls on the the sizing of those turbine components, whose design is driven by ultimate rather then fatigue loads. [..[185] ]Moreover, the hypothesis that the wind farm controllers are always active, no matter the wind direction and TI, is surely severe for the fatigue loads, but not for the ultimate ones. In fact, even if the wind farm controls may be activated only for a very short period of time, it is essential to consider that in this time-frame extreme events may occur.

Future developments of this work will try to investigate this aspect by considering different turbine classes, design concepts and materials. In addition, it would also be interesting to include in the redesign of the rotor the aerodynamic shape together with the internal structure. Connected to the design, it could be also interesting to consider a different dynamic induction

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[184]removed:

- In this study, focused on maximum loads, a simplified fatigue load assessment was also made. The impact of these fatigue loads, computed for the first-raw wind turbine under the hypothesis the wind farm control is always active, no matter the wind direction and TI, is limited but not negligible. However, in realistic farms, the amount of time spent with non-null inputs coming from the farm control layer can be rather small, yielding an even lower impact on fatigue.

[185]removed: Moreover, the above hypothesis the wind farm controllers are always active, no matter the wind direction and TI, is surely severe for the fatigue loads, but not for the ultimate ones. In fact, even if the wind farm controls may be activated only for a very short period of time, it is essential to consider that in this timeframe the extreme event that induces these maximum loads may occur.

control strategy based on individual pitch control, which entails a lower variation of thrust and which could have in turn a milder impact on blade loading (Frederik et al., 2020a).

In terms of extensions of the present research, the evaluation of the impact of farm control on ultimate and fatigue loads of downstream turbines is certainly an interesting topic, which deserves dedicated analyses with more sophisticated tools than those used in the present work to simulate the wind farm flow, e.g. CFD or dynamic wake models (Cacciola et al., 2020).

Additionally, the analyses conducted in this work considered that a possible failure of wind farm control laws does not affect significantly the ultimate loads of the single wind turbines, because turbine controller as priority over the farm one. Clearly, such an assumption, reasonably for the goal of this paper, would deserve a dedicated treatment.

Another important direction for future works deals with the assessment of the economic impact of wind farm control at wind-farm level. To this end, specific studies will be done to consider not only the impact of the chosen wind farm control on the turbine loads but also the beneficial effects that the chosen wind farm control have on the wind farm power production and, possibly, on its cost of energy.

*Author contributions.* All authors provided fundamental input to this research work through discussions, feedback and analyses of the state of the art. AC and SC conducted the sensitivity analysis with the WR control, SC conducted the sensitivity analysis with the PCM, LS performed the structural design, AC developed the main idea behind this work and supervised the research activities. SC, AC and LS wrote the manuscript.

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