

Wind Energy Science Discussion

Date: April 29, 2021  
Subject: WES-2021-9 Final Response

Dear Referees,

We would like to express you our gratitude for taking the time to review our manuscript and for the careful feedback you have provided. We truly think your comments have helped us improving our work, that has been enriched and is now clearer and more attractive for the wind energy community.

In the rest of this document, you can find the detailed response to your comments, and the new version of the article that has been revised according to your suggestions.

On behalf of all Authors,  
yours sincerely,

Alessandro Fontanella

Attached documents:

- Response to Anonymous Referee #1
- Response to Farid Khazaeli Moghamad (Referee #2)
- Manuscript changes

# Response to Anonymous Referee #1

Dear Referee, thank you very much for your comments and feedback.

Much of the work about floating wind turbine control carried out so far focus on the interaction between blade pitch controller and platform pitch motion, and how to avoid the negative-damping issue. The Authors are grateful to Referee #1 for introducing this topic in the discussion and believe that clarifying how the pitch controller tuning relates with wave disturbance rejection makes the research more interesting for both the scientific community and industry.

**RC1.1** Line 63: Does this tuning [of the feedback pitch controller] imply that the bandwidth of the blade pitch controller is reduced below the natural frequency of the floater pitch motion? (Arriving at 0.0186Hz) If yes, could you elaborate on the effect of this tuning which seems to give a controller bandwidth that is reduced with a factor  $\sim 4-5$  compared to a conventional controller for bottom fixed wind turbines. With respect to aerodynamic loads within the bandwidth of a conventional controller but not within the bandwidth of the tuned controller, and with respect to the effectiveness of the proposed wave disturbance rejection.

**AC1.1** We appreciate the Referee's comment because it helps clarifying why the industry-standard speed-regulation control strategy is not effective in rejecting the wave disturbance. In case of original gains, wind loads are inside the collective-pitch controller (CPC) bandwidth: at the controller cut-off frequency the wind spectrum is around 3% of its maximum value. Wave loads are just above the cut-off frequency (how much above depends on the sea state). The CPC with original gains rejects the wind disturbance but is ineffective against wave. In case of detuned gains, the bandwidth is shorter: the wind spectrum is 18.6% of its maximum value at the controller cut-off frequency. Moreover, the disturbance sensitivity in the controller bandwidth is increased, as rotor-speed tracking performance is degraded. Hence the controller is less effective against the wind disturbance. The capability or rejecting wave loads is not influenced much by detuning.

This is exemplified by the figure below, where the typical PSD of wind and waves (rescaled) is compared to the sensitivity of the feedback pitch controller with original and detuned gains. The feedforward controller complements the feedback CPC, and targets wave loads. Therefore, its benefits are weekly related to the tuning of the feedback controller.

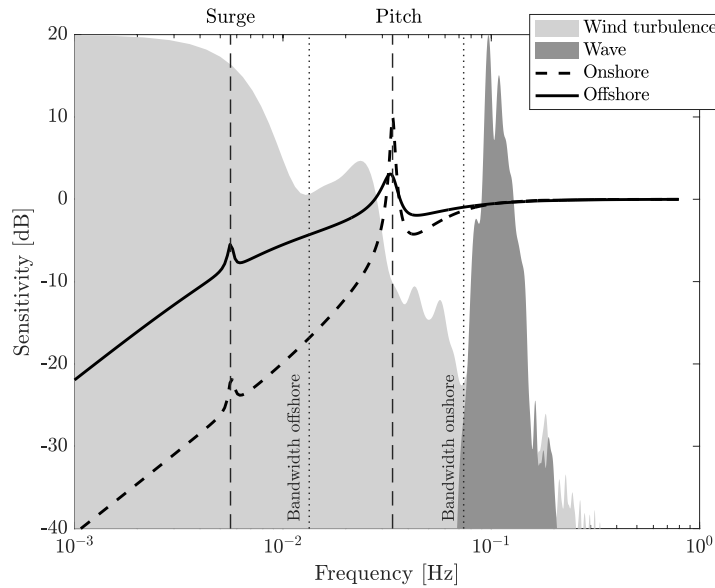


Figure 1. The sensitivity function of the feedback (FB) controller for onshore and offshore tuning, and of the feedback-feedforward (FBFF) in 16 m/s wind is compared to the typical PSD of wind and waves (magnitude has been rescaled to ease the comparison with sensitivity functions). The vertical dashed lines are the frequency of the platform surge and pitch modes, the dotted lines mark the bandwidth of the FB controller with onshore and offshore gains.

The reasoning above has been included in the section “The wave-feedforward control strategy – Disturbance rejection analysis”.

**RC1.2** Line 84: Something seems to be wrong with the reference.

**AC1.2** We agree with Referee that reduced-order modelling of an FOWT rotor is not addressed sufficiently well by the paper cited in the manuscript (“Robust gain scheduling baseline controller for floating offshore turbines”, F. Lemmer, 2020). A more appropriate reference about the topic is “Multibody modelling for concept-level floating offshore wind turbine design” (F. Lemmer, 2020).

**RC1.3** Line 390: “As it has been shown, a large part of rotor speed oscillations is caused by wind turbulence” Could some of these variations and associated DELs have been reduced if a conventional (bottom fixed) controller bandwidth had been applied?

**AC1.3** We appreciate this comment because allows us to discuss the synergy between the feedforward control strategy we propose, and the feedback collective-pitch controller (CPC) currently used in commercial wind turbines. The effectiveness of CPC with detuned gains is decreased, but detuning is needed to make the floating system stable without modifying the structure of the FB controller. The bandwidth of the FB controller, and hence its effectiveness against wind turbulence, could be increased by means of NMPZ-compensation (B. Fischer, 2013), where pitch control is used in combination with dynamic generator-torque. Another possibility is to replace the FB controller with a more complex multivariable controller, as done in “Control design methods for floating wind turbines for optimal disturbance rejection” (F. Lemmer, 2016). Both these techniques can be used in synergy with feedforward control to further improve the floating wind turbine response to environmental loads.

# Response to Farid Khazaeli Moghamad (Referee #2)

Dear Farid, thank you very much for your accurate comments. We tried to answer all of them at our best, because we are sure it will improve the quality of the article. From the level of detail of the comments we are sure you spent a good amount of time in critically reviewing our manuscript and we would like to thank you for that.

**RC2.1** 2- The proposed feedforward approach seems to be very sensitive to the wave elevation prediction and wave disturbance model. Have you checked the influence of uncertainties in the wave elevation prediction and wave disturbance model on the proposed controller performance?

**AC2.1** Thank you, Farid, for this comment: sensitivity to disturbance measurement and model uncertainties is very important in feedforward control in general. As you correctly pointed out, the wave-feedforward controller is sensitive to accuracy of wave-elevation prediction, and to fidelity of the wave disturbance model. The focus of this work is about development of the wave-feedforward control strategy and did not address the topic of uncertainties. In the present work, uncertainties in the wave measurement are only due to the preview algorithm and, as it is shown, the prediction error is small. Larger errors are expected when using a realistic measurement of upstream waves. Model uncertainties are mostly related to identification of the wave-excitation model. The linear-model we consider here has been assessed against a medium-fidelity model in a previous work and was deemed sufficiently accurate for control-design. In-depth analysis of the controller robustness with respect to model and measurement uncertainties should be addressed in future works.

**RC2.2** 3- The methodology employed for damage equivalent load estimation in Section 7.4 needs to be explained in more detail. How are the equivalent loads and stresses estimated?

**AC2.2** Fatigue loads were evaluated in terms of damage-equivalent loads (DEL) computed with the standard tool `mLife` based on aggregated 10-minutes time series of six different seeds. We added this clarification to the article. The authors refer readers interested in the algorithm used by `mLife` to the software guide, rather than including (partial) information about it in the article.

**RC2.3** 4- Please provide more details about the simulation studies in Section 7.4. How long is the time duration of the data set associated to the results in fig. 14? Is it enough to capture the wave and wind dynamics? Are the estimated DEL and standard deviation only based on a single data block of each operating speed?

**AC2.3** Thank you for this comment: information about the simulation setup were needed to understand results about loads and motions. As the Referee pointed out, the wind turbine loads may depend significantly on the simulation time. For every operating condition considered in the analysis (Tab. 1), six independent wind-wave realizations, each 10-minutes long, were considered, following the recommendation of the IEC 61400 standard. An initial pre-simulation time of 1000s was included at the beginning of simulations and cut-out from results so to exclude initial transients. Power spectral densities were computed from the aggregated time series of the six seeds relative to the same

operating condition. Also, damage-equivalent loads and standard deviations were computed for every operating condition based on the aggregated time series of six seeds. This information has been reported in the article section "Results – Turbulent wind". Moreover, PSDs reported in the manuscript were based on a single wind/wave seed (10-min data). New PSDs were computed based on six seed and the result is statistically more significant.

**RC2.4** 5- Why are the platform motions increased in case of using FBFF with scheduling compared to FB? have you also been looking into the platform rolling?

**AC2.4** Thank you for this comment. We appreciated it because it allows us to discuss better the working principle of the feedforward controller and, maybe more importantly, the coupled rotor-platform dynamics that is very significant for the response of any floating turbine. The low-speed shaft (LSS) torque depends on the aerodynamic and generator torque. The wave-feedforward reduces the aerodynamic torque oscillations caused by waves and so the fatigue loads for the LSS. The lower dynamics of LSS-torque is reflected in the platform roll-motion which is reduced as well. As demonstrated in the input-output analysis of section 4 "FOWT response to controls, wind and waves", aerodynamic torque and rotor thrust are both effected by collective pitch. The modification of the thrust force induced by wave-FF impacts the along-wind platform motions, surge and pitch, that are increased with FBFF compared to FB.

**RC2.5** 6- The gain scheduling algorithm is tuned based on different intervals of wind speed as one of the system exogenous inputs, but what about wave elevation as the other disturbance input?

**AC2.5** The FOWT dynamics (the response for a given input) depends on the mean wind speed. The turbine is more sensitive to variations of blade pitch angle in high winds, and this is visualized in the input-output of section 4. As shown in Fig. 1, sensitivity to waves remains constant, and does not depend significantly on wind speed. The control effort required to counteract a given wave is different depending on wind speed, because the wind turbine responds in a different way to blade-pitch angle variation. Intuitively, the pitch action required to reject the effects of a given wave is lower in high winds. To have the maximum possible reduction of the wave disturbance, the FF controller needs to consider how the FOWT dynamics are modified with operating condition, and a gain-scheduling strategy is introduced for this purpose. The FOWT input-output dynamics does not depend on the magnitude of the wave elevation, thus the scheduling strategy considers wind but not wave.

**RC2.6** 7- Could you please use labels for the curves in fig. 6?

**AC2.6** The figure has been updated according to the Referee's suggestion.

**RC2.7** 8- If the support substructure type is changed, how can it influence the control design? Which control parameters should be adapted? Please explain about it in the paper text.

**AC2.7** The control-synthesis procedure described in the paper is applied to one platform typology, but it is valid for any platform type. We explained how the platform typology affects the wave-feedforward controller in Section 5. In detail: when a different platform is considered, the disturbance model changes,

because forcing produced by waves depends on the platform geometry and the way waves interact with it. The FF controller responds to wave, and acts in the frequency range where most of the wave energy is. In this frequency range, the amplitude of the controller transfer function is increased if the platform is more exposed to wave excitation, that means a larger control effort is required for wave loads rejection. The platform modes are expected to change. However, these are usually outside the wave-frequency range, and have little influence on the wave-FF action. In future works, it would be nice to implement the wave-FF control strategy in FOWTs based on different platform typologies, so to reduce uncertainty about its benefits.

**RC2.8** 9- Authors' statement "Reducing rotor speed oscillations also results into a lower fatigue damage for the wind turbine shaft and tower"

Comment> Could you elaborate more on this statement in the paper text? How is rotor speed oscillation connected to fatigue damage for the wind turbine shaft and tower?

**AC2.8** The answer to this comment is strictly connected to comment RC2.4, and, for this reason we decided to address them together in the revised paper. As said for RC2.4, we are grateful to Farid for this comment because it gives us the possibility to discuss more in detail the coupled rotor-platform dynamics of floating turbines. Concerning RC2.8, similarly to what we commented in AC2.4, the wave-feedforward controls the blade pitch angle to reduce the aerodynamic torque fluctuations. The pitch angle modification also affects the thrust force and, consequently, the tower-FA loads.

**RC2.9** 10- Authors' statement "The proposed FB-FF controller, that keeps into account the above- mentioned movement of the LIDAR, can reduce power and rotor speed fluctuations up to 80% and tower, rotor-shaft, and blades fatigue loads of 20%, 7% and 9%, respectively"

Comment> I cannot find the results that confirm these numbers in Section Results. These numbers should match the simulation results presented in the paper.

Authors should also explain in simulation studies about those quantified results and how they are obtained.

**AC2.9** The results mentioned in the comment pertain to a paper about LIDAR-based wind feedforward "Collective Pitch Feedforward Control of Floating Wind Turbines Using Lidar". This paper is cited in the introduction because wave-feedforward is loosely inspired to wind-feedforward control strategies. Results achieved by means of wave-feedforward are different, as the two control strategies target different disturbances.

**RC2.10** 11- Authors' statement "Wave disturbance is responsible of a large fraction of the fatigue loads experienced by a floating wind turbine"

Comment> could you please provide reference for this statement? Which failure modes are you specifically focusing on?

**AC2.10** We agree with you that the sentence was quite broad, and some clarification was needed. First, we want to point out that the effect of wave is not limited to fatigue loads: wave provides a considerable fraction of the dynamic excitation

experience by an FOWT, and this has several effects. The effects of wave excitation are analyzed in the work of J. Jonkman "Dynamics Modeling and Loads Analysis of an Offshore Floating Wind Turbine" (2007). Wave increases rotor-speed, and generator power, oscillations because of increased platform motion. Tower shear forces and bending moments are increased as well, and the increment is proportional to the severity of waves. The suggested article "Stochastic dynamic load effect and fatigue damage analysis of drivetrains in land-based and TLP, spar and semi-submersible floating wind turbines" shows that wave is also responsible of increased fatigue damage for the drivetrain.

**RC2.11** 12- Authors' statement "The platform motion caused by waves, turns out into a variation of the apparent wind speed, which affects rotor torque, and then speed."

Comment> Could platform motions like rolling directly influence the rotor speed. Could you explain it in the text to complement the above statement?

**AC2.11** We agree appreciate this comment because it helps clarifying the assumptions we used in the analysis. The platform motion caused by waves produces a variation of the apparent wind speed, which affects rotor-torque, and then rotor-speed. Our analysis considers the case of zero-degree waves, that do not excite lateral motions (sway, roll, yaw). For non-zero-degree waves, also the response of these DOFs is significant and contributes to oscillations of the wind inflow.

Manuscript changes  
(latexdiff)



# Model-based design of a wave-feedforward control strategy in floating wind turbines

Alessandro Fontanella<sup>1</sup>, Mees Al<sup>2</sup>, Jan-Willem van Wingerden<sup>3</sup>, and Marco Belloli<sup>1</sup>

<sup>1</sup>Mechanical Engineering Department, Politecnico di Milano, Milano, Via La Masa 1, 20156, Italy.

<sup>2</sup>Sowento GmbH, Donizettistraat 1A, 70195 Stuttgart, Germany.

<sup>3</sup>Delft Center for Systems and Control, Delft University of Technology, Delft, 2628 CD, The Netherlands.

**Correspondence:** Alessandro Fontanella (alessandro.fontanella@polimi.it)

**Abstract.** Floating wind turbines rely on feedback-only control strategies to mitigate the negative effects of wave excitation. Improved power generation and lower fatigue loads can be achieved by including information about ~~the~~ incoming waves into the ~~wind~~-turbine controller. In this paper, a wave-feedforward control strategy is developed and implemented in a 10MW floating wind turbine. A linear model of the floating wind turbine is established and utilized to show-understand how wave excitation affects ~~the wind turbine rotor speed output, and rotor speed, and so power, as well as to show~~ that collective-pitch is ~~an effective control input to reject the wave disturbance. Based~~ suitable for reducing the effects of wave excitation. A feedforward controller is designed based on the inversion of the ~~same model, a feedforward controller is designed, and its performance is examined by means of linear analysis. A~~ linear model, and a gain-scheduling algorithm is proposed to adapt the feedforward action as ~~the~~ wind speed changes. ~~Non-linear~~ The performance of the novel wave-feedforward controller is examined first by means of linear analysis, and then with non-linear time-domain simulations ~~prove that the proposed feedforward control strategy is an effective way of reducing rotor speed oscillations and structural fatigue loads caused by waves in FAST. This paper proves that including some information about incoming waves into the turbine controller can play a crucial role in improving power quality and the turbine fatigue life. In particular, the proposed wave-feedforward control strategy achieves this goal complementing the industry-standard feedback pitch controller. Together with the wave-feedforward control strategy, this paper provides some~~ insights about the response of floating wind turbines respond to collective pitch control and waves, that can be useful in future control-design studies.

## 1 Introduction

Floating offshore wind turbines (FOWTs) are currently operated without any real-time information about ocean conditions. Industry-standard controllers are ~~feedback-only~~ feedback (FB) only: the wind turbine controller reacts to the external disturbance of wind and waves as ~~it occurs~~ this occurs. One possibility to improve the current floating wind technology is to include real-time information about the marine environment into the ~~wind~~-turbine controller and to design new control logics based on ~~it~~ that.

Concerning wind turbulence, feedforward (FF) control has recently drawn the attention of the research community, as it can effectively reduce ~~the~~ fatigue loads and improve power production. Research has been mainly driven by ~~the~~ improve-

ments in the LIDAR (light detection and ranging) technology that enables ~~the~~ measurement of the wind field upstream the wind turbine. ~~The potential of~~ One of the first studies about LIDAR-assisted control ~~were investigated in Harris et al. (2006)~~ was carried out by Harris et al. (2006), that explored the potentialities of this new control strategy, and found it can reduce blade fatigue loads approximately of 10% in turbulent wind conditions. Since then, several control logics were developed ~~Laks et al.; Dunne et al. (a,b,c); Schlipf et al. (2013)~~ based on the inclusion of LIDAR signals in the turbine controller, for example by Laks et al.; Dunne et al. (a,b,c); Schlipf et al. (2013), demonstrating positive effects for the blade loads and the turbine components. Very few are the studies about LIDAR-assisted ~~FF~~ wind-FF control in floating wind turbines: in the paper of Schlipf et al. (2015), a collective-pitch FF controller is designed ~~in order to reduce the~~ to reduce rotor speed oscillations caused by inflow turbulence. The LIDAR moves with the floating ~~wind~~ turbine and measurements need to be corrected for that. The proposed FB-FF controller, that keeps into account the above-mentioned movement of the LIDAR, can reduce power and rotor speed fluctuations up to 80% and tower, rotor-shaft, and blades fatigue loads of 20%, 7% and 9%, respectively.

~~Applying the wind-feedforward concept to waves is an attractive perspective, as the wave disturbance is responsible of a large fraction of the fatigue loads experienced by a floating wind turbine. However, the idea is still~~ Wave disturbance is responsible of a considerable fraction of dynamic excitation experienced by an FOWT. This was first shown in the work of Jonkman (2007), where the response of NREL 5-MW turbine installed on land is compared to the same turbine mounted on the floating ITI Energy barge, in the presence of wind and waves. The rotor-speed excursions in the floating turbine are increased of 60% because of the oscillations in wind speed caused by platform motion. Consequently, fluctuations in the generator-power are larger as well. Tower shear forces and bending moments are increased. The analysis of Jonkman (2007) also shows that offshore-to-onshore ratios decrease with decreasing severity of the wave conditions, suggesting that a large part of the increments is due to wave excitation. More specifically for the drivetrain, Nejad et al. (2015) assessed the loads in a 5MW wind turbine mounted on four platform concepts for different wind and wave conditions. The analysis suggests an increment of the fatigue damage, which is mainly caused by the large wave-induced thrust force.

Applying the same idea behind wind-FF control to wave is therefore an attractive perspective, but the idea is largely unexplored. In ~~Ma et al. (2018)~~ Raach et al. (2014) introduced an NMPC strategy that uses a perfect preview of a reduced wave disturbance to mitigate the turbine structural loads. Promising improvements over an industry-standard FB controller are shown, at the expense of a significant increase in the controller complexity. Moreover, most of the performance gain is seen for blade loads, that are caused by wind turbulence rather than wave, so it appears the NMPC does not effectively counteract waves. Ma et al. (2018) developed and validated two algorithms for real-time forecasting of wave forces ~~are developed and validated~~. Based on the predicted wave forces, a finite-horizon LQR controller is designed and applied to a TLP-FOWT to minimize the tower-base fore-aft bending moment, achieving mixed results. ~~In~~ Al et al. (2020) Al et al. (2020) introduced an inversion-based feedforward control strategy ~~is introduced~~, showing it is an effective way of reducing wave-induced rotor speed oscillations.

The present paper further develops the concept of ~~wave-feedforward-exploiting-the~~ wave-FF exploiting tools of model-based control. The ~~wave-feedforward-wave-FF~~ control strategy is enabled by ~~the use of~~ an integrated model of the ~~floating~~

60 ~~wind turbine that captures all its~~ FOWT that captures its most relevant physics. Hence, this work proves the effectiveness of multidisciplinary analysis as a mean to advance the current floating wind technology.

All the reasoning is made with reference to a floating wind turbine ~~in particular~~, but it is deemed valid for any FOWT. The floating wind turbine of reference is based on an open-source concept and is defined in Section 2. The idea is to use ~~the~~ tools of multivariable systems control to gain insight about the effects of waves on the FOWT response and ~~to~~ assess which is the best control input (generator torque or collective pitch) to mitigate them. Then, to leverage this knowledge to design a feedforward controller that reduces ~~the~~ power fluctuations caused by waves. A control-oriented linear model of the FOWT is required first for the multivariable analysis, and later for the synthesis of the feedforward controller. The control-oriented linear model is briefly introduced in Section 3. Section 4 deals with the input-output analysis. The feedforward controller is designed in Section 5. Again, linear analysis is utilized to assess the controller performance, which is shown to be highly dependent on the wind turbine operating point. Hence, a gain-scheduling law is introduced to have the maximum performance in any wind condition. The wave-feedforward controller requires as input a preview of the incoming waves, which is obtained based on the algorithm presented in Section 6. In Section 7, the feedforward controller and the wave prediction algorithm are implemented in a nonlinear, medium-fidelity model of the floating wind turbine, and numerical simulations are carried out in realistic environmental conditions to evaluate the benefits of the feedforward control strategy. Section 8 draws the conclusion and gives some recommendations for future work.

## 75 2 Definition of a reference floating wind turbine

This section defines the floating system that is considered in this study. The FOWT is formed by the DTU 10MW ~~Bak et al. (2013)~~ (Bak et al. (2013)) wind turbine and the INNWIND.EU TripleSpar platform ~~Azeona et al. (2017); Lemmer et al. (2020a)~~ (Azcona et al. (2020)). The characteristics of this FOWT concept are similar to those of the current commercial projects ~~and~~ are publicly available.

80 The floating wind turbine is regulated with an industry-standard generator-speed controller. In below-rated winds the controller maximizes the extracted power by keeping the blade pitch angle  $\theta$  constant and varying the generator torque  $Q_G$  as a function of generator speed  $\omega_G$  squared:

$$Q_G = k_G \omega_G^2, \quad (1)$$

with  $k_G = \frac{1}{2} \rho \pi R^5 (C_{p,max} / \tau^3 \lambda_{opt}^3)$ , where  $\rho$  is the air density,  $R$  the rotor radius, and  $\tau$  the transmission ratio.  $C_{p,max}$  is the maximum power coefficient, which is achieved for zero pitch angle and the optimal tip-speed-ratio  $\lambda_{opt}$ .

85 In above-rated winds, the controller regulates the extracted power to its rated value setting the generator torque to a constant value, equal to rated. Generator speed oscillations are directly reflected by the wind turbine power output. ~~The rotor~~ Rotor speed is regulated to its rated value  $\omega_{G,r}$  by the ~~CPC~~ collective-pitch controller (CPC), which reacts to the generator speed feedback as:

$$\theta = k_P (\omega_G - \omega_{G,r}) + k_I \int (\omega_G - \omega_{G,r}) dt, \quad (2)$$

90 where  $k_P$  and  $k_I$  are the proportional and integral gains, ~~which are~~ tuned following the model-based approach of Fontanella et al. (2018) to achieve the maximum damping for the platform pitch mode and for the drivetrain mode. A gain scheduling factor is introduced to adjust the PI controller gains as ~~the~~ wind speed varies. The generator-speed feedback controller constitutes the baseline configuration against which the benefits of ~~feedforward-wave-FF~~ are assessed.

### 3 The control-design model

95 ~~Feedforward control is a~~ The wave-FF control strategy we want to develop is model-based ~~control strategy~~, and its development requires a linear model of the floating wind turbine. The control-design model is derived based on linear first-principle equations of the most important physics of the FOWT, rather than from the linearization of a higher-order model. The main features of the model are recalled below, while a detailed description is ~~found in~~ reported in the article of Fontanella et al. (2020).

~~The model is built to describe~~ The model describes the global dynamics of the FOWT ~~and neglects~~, neglecting the dynamics  
100 of single components. It considers the rigid-body platform motions and the rotor dynamics about a steady-state configuration (operating-point) set by an average wind speed, ~~static displacement of the platform~~ platform motion, rotor speed, collective-pitch and generator torque. The inputs are generator torque and collective blade-pitch angle, which are the main control variables for the FOWT, in addition to wind turbulence and wave elevation. The model equations are cast in state-space form and are valid only for small perturbations about the operating-point.

105 The structural dynamics builds on the theory of multibody systems. The model considers the FOWT components as rigid bodies: this simplification is deemed acceptable in a control-oriented model, as the bandwidth of an FOWT controller is usually lower than the flexible modes of the tower, blades, and drivetrain. Moreover, the focus of the control-oriented model is the coupled rotor-platform response induced by waves more than the dynamics of the flexible components.

Rotor aerodynamics are introduced in the model with a simplified approach. The aerodynamic model does not consider the  
110 single blade, but computes the integral rotor forces. This simplification is valid because the ~~global dynamics of the FOWT~~ FOWT global dynamics is determined by the integral rotor loads, rather than the loads of the single blades ~~Lemmer et al. (2020e)~~. This assumption is reasonable for a reduced-order model of the FOWT, as noticed by Lemmer et al. (2020b). Only the rotor torque and thrust force are ~~taken into account~~ considered because they drive the global dynamics of the floating turbine: aerodynamic torque sets the wind turbine power production and thrust force the motion of the floating platform. Torque and  
115 thrust are modeled by means of the quasi-steady approach, based on the derivatives of the torque and thrust curves of the wind turbine. The formulation of the control-oriented model enables the inclusion of ~~the~~ unsteady aerodynamic effects associated with the ~~motion of the FOWT~~ FOWT motion, which may have an influence on the ~~dynamics of the platform modes~~ platform response. In this respect, a similar approach to the one presented ~~in~~ by Bayati et al. (2017) could be used.

#### 3.1 Frequency-dependent hydrodynamic loads

120 Hydrodynamic radiation and first-order-wave forces are modeled by means of linear-time-invariant parametric models.

~~The frequency-dependent~~ Frequency-dependent radiation forces are approximated by a parametric model in state-space form, from the added mass and damping matrices of panel code pre-calculations. In this work, the frequency domain identification method of the MATLAB toolbox developed ~~in by~~ Perez and Fossen (2009) is used, but other methods are available in literature, for example the one by Janssen et al. (2014).

125 Also the first-order-wave excitation is introduced in the model with a parametric model in state-space form, which connects the wave elevation to the wave forces. This choice allows to have the wave elevation, rather than wave forces, as input to the model. The wave excitation model is obtained based on the wave-force coefficients, which are usually computed at discrete frequencies through a panel code (e.g. ~~WAMIT ?WAMIT~~). In the present case, the parametric model is defined by means of system identification of the impulse response function of the force coefficients ~~Jonkman et al. (2018); Lemmer et al. (2020e)~~  
 130 ~~whereas~~. This approach was firstly applied to floating turbines by Lemmer et al. (2020c), and it is currently available to model wave excitation in OpenFAST (Jonkman et al. (2018)). Identification of the parametric model from frequency-domain data (i.e. the force coefficients) ~~are used for identification in~~ is also a possibility, that was for example used by Al et al. (2020). The wave-force model of panel code data is non-causal, which means a force is developed before the wave reaches the center of the platform. The panel code data, in the form of impulse response functions, are causalized before system identification  
 135 by introducing a time delay  $t_d$  (with  $t_d > 0$ ) to have zero response for negative times. The time delay is embedded inside the identified parametric model and, consequently, into the linear model of the FOWT. The response obtained from the linear model is delayed of a time  $t_d$  with respect to the input wave elevation.

#### 4 ~~Input-output analysis~~ FOWT response to controls, wind and waves

An input-output analysis is carried out to gain insight into the FOWT response to the available controls, generator torque and  
 140 collective-pitch, and to the wave disturbance. The analysis answers the question of which is the best combinations of controls to ~~be used to reject the detrimental~~ reject the negative effects of waves. This information is used later ~~on~~ to support the synthesis of the ~~feedforward~~ wave-FF control strategy. Moreover, the analysis gives a picture of the FOWT dynamics that may prove to be useful also for other purposes.

The analysis starts from the control-design model in a transfer function representation

$$145 \quad \mathbf{y} = \mathbf{G}\mathbf{u} + \mathbf{G}_d\mathbf{d}. \quad (3)$$

The system has two outputs, rotor speed and tower-top motion, ~~which are~~ collected in  $\hat{\mathbf{y}} = [\omega_r, x_{tt}]^T$ ; two control inputs, collective-pitch and generator torque, collected in  $\hat{\mathbf{u}} = [\theta, Q_g]^T$ ; and two disturbance inputs, ~~the~~ variation from average of the hub-height wind speed and ~~the~~ wave elevation,  $\hat{\mathbf{d}} = [v, \eta]^T$ . The model of Eq. (3) is used to compute the ~~deviation of the outputs~~ outputs deviation from their steady-state value, ~~because of~~ due to a change in the control and disturbance inputs.

150 To ~~make it easier to interpret the results of the MIMO analysis~~ facilitate the interoperation of MIMO analysis results, the model of Eq. (3) needs to be scaled. This ensures that inputs and outputs are of the same importance. The scaled model is obtained by dividing any variable by its maximum expected (for ~~the~~ disturbances) or allowed (for ~~the~~ control inputs) change.

The output, input and disturbance scaling matrices ( $D_y$ ,  $D_u$  and  $D_d$  respectively) are

$$D_y = \begin{bmatrix} 0.15\omega_0 & 0 \\ 0 & 5 \end{bmatrix}, \quad D_u = \begin{bmatrix} 5\pi/180 & 0 \\ 0 & 0.1Q_{g,0} \end{bmatrix}, \quad D_d = \begin{bmatrix} 0.1U & 0 \\ 0 & 4 \end{bmatrix}, \quad (4)$$

155 where  $\omega_0$  is the rated rotor speed,  $Q_{g,0}$  the rated generator torque, and  $U$  the mean wind speed. The scaled model is

$$\hat{y} = \hat{G}\hat{u} + \hat{G}_d\hat{d}, \quad (5)$$

with

$$\hat{G} = D_y^{-1}GD_u, \quad \hat{G}_d = D_y^{-1}GD_d. \quad (6)$$

Given an input between 0 and 1, where 0 is no input and 1 is the maximum expected value, the outputs of the model of Eq.  
160 (5) take a value between 0 and 1, where 0 is no output and 1 corresponds to the maximum expected or allowed value for the output.

#### 4.1 Control inputs

The model without disturbances  $\hat{y} = \hat{G}\hat{u}$  is considered first. The transfer function matrix  $\hat{G}$  has two couples of input and output directions, each with an associated gain. For any selected frequency, the directions and gains of matrix  $\hat{G}$  are obtained  
165 from its singular value decomposition (SVD) ~~Levine (1996)~~ (Levine (1996))

$$\hat{G} = U\Sigma V^H. \quad (7)$$

The column vectors of  $V = [\bar{v}, \underline{v}]$  are the input directions, the column vectors of  $U = [\bar{u}, \underline{u}]$  the output directions, and the respective singular values are along the diagonal of  $\Sigma = \text{diag}(\bar{\sigma}, \underline{\sigma})$ . When the input vector  $\hat{u}$  has the same direction of vector  $\bar{v}$ , the output  $\hat{y}$  is along the direction  $\bar{u}$ , the gain is equal to  $\bar{\sigma}$  and it is the largest possible for that frequency. The input produces  
170 the most effect on the output, and the directions of  $\bar{v}$  and  $\bar{u}$  are named the *strongest*. Conversely, when the input is directed as  $\underline{v}$ , the gain is  $\underline{\sigma}$ , and the input has the least effect on the output, which is along  $\underline{u}$ . The directions of  $\underline{v}$  and  $\underline{u}$  are named the *weakest*.

The steady-state (i.e. zero frequency) plant model of the FOWT in a 16 m/s wind is

$$\hat{G}(j\omega = 0) = \begin{bmatrix} -2.736 & -0.311 \\ -1.216 & 0.097 \end{bmatrix}. \quad (8)$$

175 The (1,1) element of  $\hat{G}$  is much larger than the (1,2) element, so ~~the~~ rotor speed is a lot more sensitive to a steady-state (i.e. ~~a~~ very slow) change in collective-pitch, the first input, than in generator torque, the second input. Collective-pitch ~~effects~~ has an effect both rotor speed, the first output, and tower-top motion, the second output, in the same direction. If collective-pitch is increased, the rotor is slowed because of the decreased aerodynamic torque, and the nacelle moves upwind, because of the

lower thrust force. The plant model is decomposed into its SVD

$$180 \quad \mathbf{U} = \begin{bmatrix} -0.916 & -0.401 \\ -0.401 & 0.916 \end{bmatrix}, \quad \mathbf{\Sigma} = \begin{bmatrix} 3.004 & 0 \\ 0 & 0.214 \end{bmatrix}, \quad \mathbf{V} = \begin{bmatrix} 0.997 & -0.082 \\ 0.082 & 0.997 \end{bmatrix}. \quad (9)$$

The strongest and weakest input directions are obtained by different combinations of collective-pitch and generator torque (e.g. the strongest is given by 0.997 of collective-pitch and 0.082 of generator torque). The ratio between the gain in the strongest and weakest direction (i.e. the condition number) is  $\text{CN} = \bar{\sigma}/\underline{\sigma} = 14.0$ . The system is said to be *ill-conditioned*. At steady-state, the input combinations with prevailing collective-pitch have a much stronger effect on the FOWT than the input combinations with prevailing generator torque. The strongest and weakest output directions are given by different combinations of rotor speed and tower-top motion. From  $\bar{\mathbf{u}} = [-0.916, -0.401]^T$ , it is seen ~~that~~ the effect of the strongest input combination, an increase of collective-pitch, is to slow down the rotor and to move the nacelle upwind. This is in agreement with the result of the inspection of  $\hat{\mathbf{G}}(j\omega = 0)$  and makes sense from a physical point of view.

The SVD of the plant model  $\hat{\mathbf{G}}(j\omega)$  is computed for several frequencies up to 0.3 Hz, and for seven operating points ~~for~~ of wind speeds between 12 and 24 m/s. The top plot of Fig. 1 shows the magnitude of the two component of  $\bar{\mathbf{u}}$ , that is the fraction of collective-pitch and generator torque in the strongest input combination; the middle plot, the magnitude of the first and second component of  $\bar{\mathbf{v}}$ , the fraction of rotor speed and tower-top motion in the strongest output direction; the bottom plot the corresponding singular values, the gain. Collective-pitch is the most effective input, at any frequency and in any above-rated wind speed. ~~Collective-pitch-effects~~ Pitching blades affects both rotor speed and tower top motion, because it modifies at the same time the aerodynamic torque and thrust. At the platform modes frequencies, the response is almost only tower-top motion, and the gain is increased. ~~It~~ it takes a small collective-pitch action to move the nacelle, because the resulting rotor thrust variation excites the resonant response of the platform. Controlling rotor speed is hard. In the wave frequency range, the gain is decreased so it becomes more difficult to control the system, and rotor speed is easier to control than tower-top motion.

In summary, collective-pitch is the most effective control in above-rated winds. It ~~effects~~ has an effect both rotor speed and tower-top motion. In the frequency range where wave is active, collective-pitch becomes less effective, so it is harder to control the wind turbine.

## 4.2 Disturbances

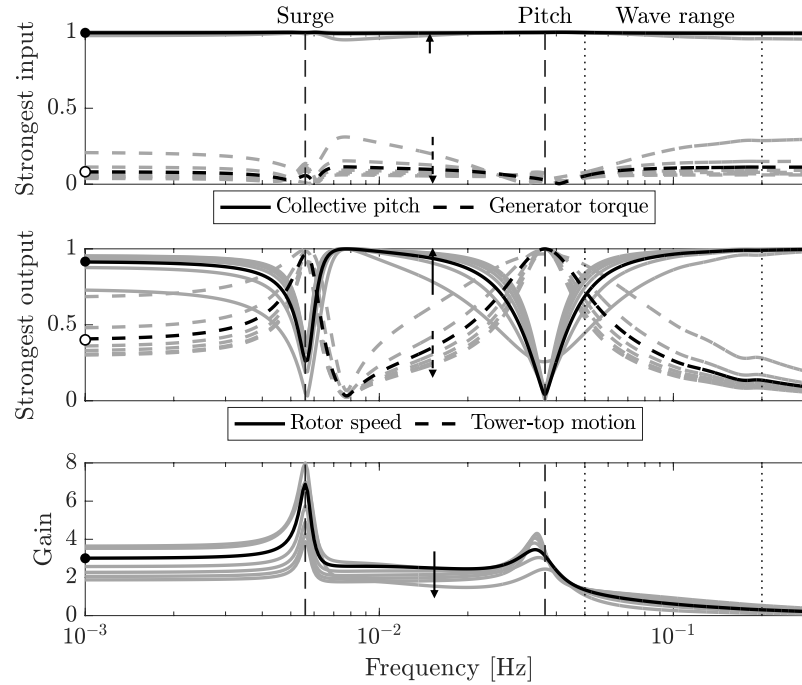
The wind and waves disturbances are here considered separately. The direction of a disturbance is

$$205 \quad \mathbf{y}_d = \frac{1}{\|\hat{\mathbf{g}}_d\|_2} \hat{\mathbf{G}}_d, \quad (10)$$

where  $\hat{\mathbf{g}}_d$  is the appropriate column of  $\hat{\mathbf{G}}_d$  (the first for wind, the second for wave). The disturbance condition number is

$$\text{DCN} = \bar{\sigma}(\hat{\mathbf{G}}) \bar{\sigma}(\hat{\mathbf{G}}^{-1} \mathbf{y}_d), \quad (11)$$

where  $\bar{\sigma}(\cdot)$  is the maximum singular value. The DCN measures the control effort required to reject a given disturbance, relative to rejecting a disturbance with the same magnitude but aligned with the strongest output direction (i.e. the direction where



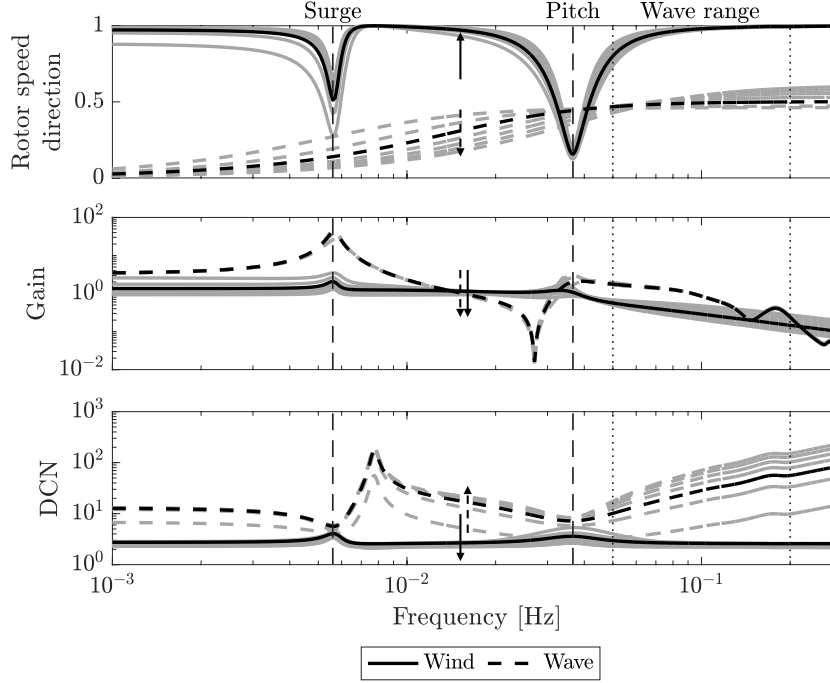
**Figure 1.** Singular value decomposition of the floating wind turbine plant for several above-rated operating points (grey, [arrows for increasing wind](#)), and for the 16 m/s wind case (black) [with values](#). Values for the zero-frequency case [are](#) displayed by the marks  $\bullet$  and  $\circ$ . The vertical dashed lines are the frequency of the platform surge and pitch modes, the frequency range where waves are active is enclosed by the vertical dotted lines.

controls are effective the most) [Skogestad and Postlethwaite \(2005\)](#); [Skogestad and Postlethwaite \(2005\)](#)). The higher the DCN  
 210 is, the harder it is to reject the disturbance with the available controls.

The [effects of the wind and waves](#) [effect of wind and wave](#) disturbance in the frequency range up to 0.3 Hz is assessed in Fig. 2, [for considering](#) seven operating points of wind speed between 12 and 24 m/s. Wind turbulence acts directly on the rotor causing [, first,](#) a variation of the aerodynamic torque, which affects rotor speed. Wind turbulence also acts on the platform, through the rotor thrust, but this excitation mechanism is less effective than wave forcing. The wind disturbance is  
 215 aligned to the rotor speed output direction. Collective-pitch is very effective for controlling rotor speed, and rejecting the wave disturbance with collective-pitch does not require a large effort. This is visualized by the DCN. Wave is aligned to tower-top motion, and partially shifts towards rotor speed for increasing frequency. Waves act on the platform, but also excite [rotor speed](#) [the rotor response](#). The platform motion caused by waves [, turns out into produces](#) a variation of the apparent wind speed, which affects [rotor torque](#) [rotor torque](#), and then [speed](#) [rotor speed](#). This mechanism of excitation is more effective above the  
 220 platform pitch frequency [, because most of the wave energy is concentrated here.](#) The analysis considers zero-degree waves, [that do not excite lateral motions \(sway, roll, yaw\)](#). For non-zero-degree waves, also the response of these DOFs is significant and contributes to oscillations of the wind inflow. The gain of [waves is maximum at the platform modes frequencies](#) [wave is](#)



maximum where wave produces the largest platform motions, so at the frequencies of platform modes, where wave excites the FOWT in resonance causing large motions, and in the wave range, and above the platform pitch frequency, where the strength of wave forcing is the maximum. The wave disturbance is not aligned to the rotor speed output direction, and the DCN shows that it is very hard to counteract the wave disturbance by means of the wind turbine controls.

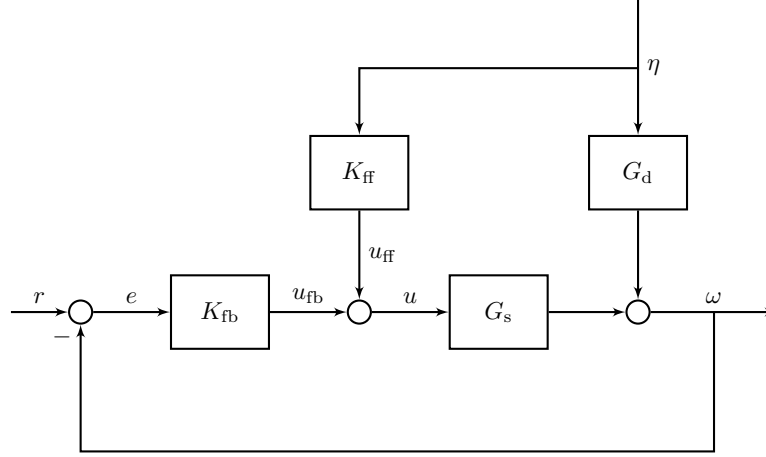


**Figure 2.** The direction with respect to the rotor speed output direction, the singular value (gain) and the disturbance condition number (DCN) associated to with wind and waves. Grey lines correspond to the above-rated operating points (arrows for increasing wind) and the black line to the one of 16 m/s wind speed. The vertical dashed lines are the frequency of the platform surge and pitch modes, the frequency range where waves are active is enclosed by the vertical dotted lines.

To sum up, waves effect rotor speed, because waves drive the platform motion which result into an apparent wind speed at rotor. The wave excitation is stronger at the platform frequencies, where the FOWT is excited in resonance, and in the wave range, where it is concentrated most of the wave energy. above the platform pitch frequency. Moreover, it is quite hard to counteract the wave disturbance by means of controls available in the wind turbine controls. Lemmer et al. (2016) carried out a similar MIMO analysis for the same floating turbine system, but based on a different linear model. They equally found that wave has a significant effect on rotor-speed and tower-top motion, and that it is difficult to counteract wave excitation by means of the control inputs available in the wind turbine. All this shows that new control strategies specific to FOWTs are needed to deal with waves. The wave-feedforward control strategy leverages the knowledge of the FOWT dynamics to improve the performance of the traditional wind turbine controller with respect to the mitigation of the wave effects.

## 5 The wave-feedforward control strategy

The feedforward (FF) controller is designed to cancel the effect of the wave disturbance on wave-FF controller cancels the oscillations of rotor speed, end-hence on the power output of the wind turbine. The FF controller regulates rotor speed producing an additional collective-pitch request which and hence of the turbine power output, that are caused by waves. The additional collective pitch command it produces, is summed to the pitch signal of the existing generator-speed feedback (FB) controller. The FBFF control strategy is shown in 3.



**Figure 3.** Block diagram of the feedback-feedforward controller.

For wave-disturbance rejection, the reference signal  $r$  is zero and the closed-loop rotor speed output  $\omega$  is

$$\omega = (I + G_s K_{fb})^{-1} (G_s K_{ff} + G_d) \eta, \quad (12)$$

where,  $G_s$  is the collective-pitch to rotor-speed plant,  $G_d$  the wave disturbance model,  $K_{fb}$  the FB controller,  $K_{ff}$  the FF controller,  $\eta$  the wave disturbance. In the model-inverse approach, the FF controller  $K_{ff}$  is designed to cancel the effect of  $\eta$  on  $\omega$ , thus the transfer function of the controller transfer function is

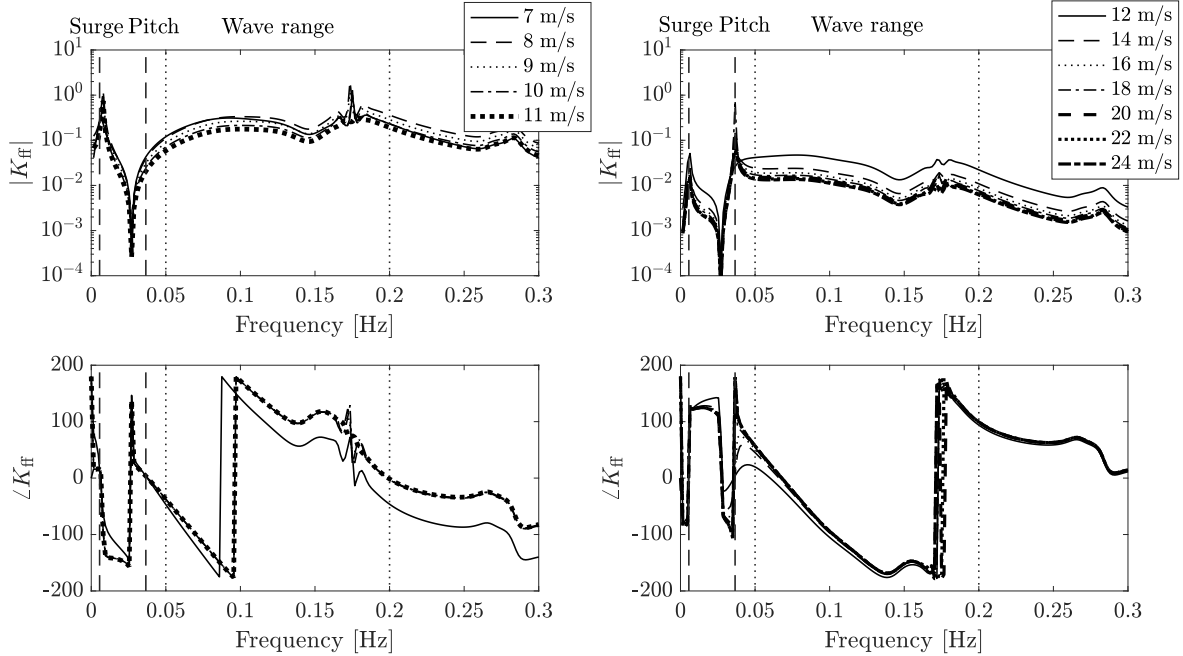
$$K_{ff} = -G_s^{-1} G_d. \quad (13)$$

$K_{ff}$  is the transfer function between the input wave elevation measurement and the collective-pitch command. In general,  $G_s$ ,  $G_d$ , and  $K_{ff}$ , depend on the wind turbine operating condition and so, on the mean wind speed.

The transfer function of the FF controller obtained based on FF controller transfer function obtained from Eq. (13), which was evaluated for different wind conditions, is shown in Fig. 4 for different operating conditions. There is a significant difference between the generic shape assumed by  $K_{ff}$  in below-rated and above-rated conditions. The amplitude is increased in

below-rated winds because collective-pitch is not effective for controlling rotor speed. ~~There~~Here, a variation of ~~the~~ collective-pitch produces a smaller variation of rotor torque than in above-rated winds. For this reason, it is decided to confine the action of the FF controller to the above-rated region: when the mean pitch angle falls below a threshold, the FF action is ~~switched-off~~ ~~switched-off~~ in order to prevent ~~an~~ excessive pitch actuators usage.

The above-rated controller  $K_{ff}$  has a peak at the platform pitch natural frequency which is not present in below-rated winds. In above-rated winds, the platform pitch mode damping is decreased and ~~the~~ wave excitation leads to a large response at this frequency. This causes significant oscillations of the ~~tower-top~~nacelle, with consequently large variations of the apparent wind speed, ~~and of aerodynamic torque~~. A high control effort is therefore required to balance the wind fluctuations.



**Figure 4.** The feedforward controller transfer function  $K_{ff}$  for below-rated (left) and above-rated (right) operating conditions. The vertical dashed lines are the frequency of the platform surge and pitch modes, the frequency range where waves are active is enclosed by the vertical dotted lines.

The control-synthesis procedure described above is valid for any platform typology. When a different platform is considered, the disturbance model changes, because forcing produced by waves depends on the platform geometry and the way waves interact with it. The FF transfer function  $K_{ff}$ , the product between the inverse of the plant model and the disturbance model, changes accordingly. The FF controller responds to wave, and acts in the frequency range where most of the wave energy is. In this frequency range, the amplitude of  $K_{ff}$  is increased if the platform is more exposed to wave excitation, that means a larger control effort is required for wave loads rejection. The platform modes are expected to change. However, these are usually outside the wave-frequency range, and have little influence on the wave-FF action.

## 5.1 Disturbance rejection analysis

270 Considering the FBFF controller of Fig. 3, and the closed-loop disturbance response of Eq. (12), the FB, the FF and the FBFF sensitivity function is defined respectively as

$$\begin{aligned} S_{fb} &= (1 + G_s K_{fb})^{-1} , \\ S_{ff} &= 1 + G_s K_{ff} G_d^{-1} , \\ S_{fbff} &= S_{fb} S_{ff} . \end{aligned} \tag{14}$$

The sensitivity function of the FBFF controller is computed for different above-rated wind speeds  $U_i$  to account for the different behavior of the wind turbine

$$\begin{aligned} S_{fbff}(U_i) &= S_{fb}(U_i) S_{ff}(U_i) , \\ S_{fb}(U_i) &= (1 + G_s(U_i) K_{fb}(U_i))^{-1} , \\ 275 \quad S_{ff}(U_i) &= 1 + G_s(U_i) K_{ff}(\bar{U}) G_d^{-1}(U_i) , \end{aligned} \tag{15}$$

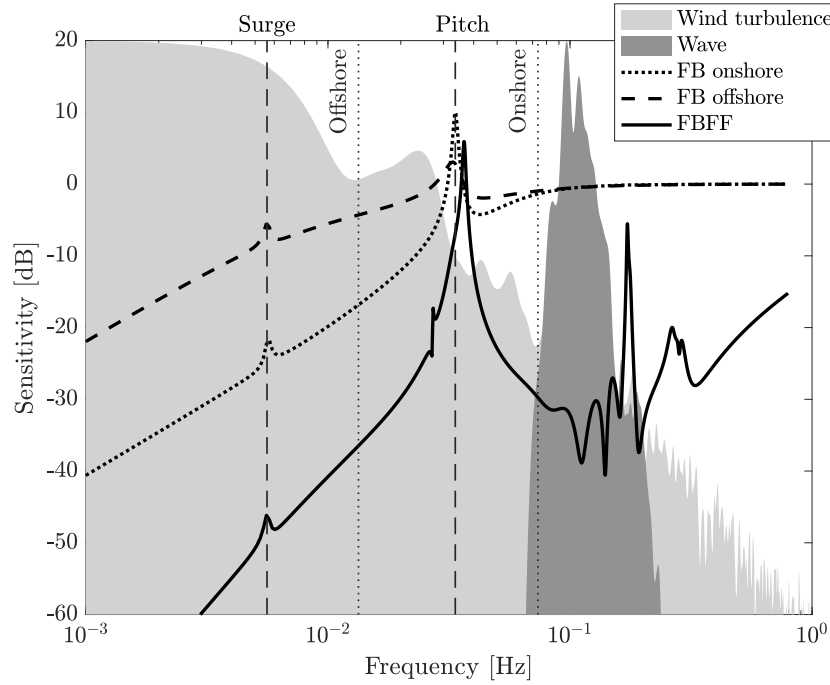
with  $U_i = 12, 13, \dots, 24 \text{ m/s}$  and  $\bar{U} = 16 \text{ m/s}$ . The sensitivity function tells how the disturbance is propagated to the FOWT response through the FB, FF and FBFF controllers. The lower the magnitude of the sensitivity function, the lesser the disturbance effect on the FOWT response. Figure 5 reports the sensitivity function of the FB and FBFF controllers, and compares is to the typical PSD of wind and waves (rescaled). Two curves are shown for the FB controller: one is with gains for the onshore DTU 10MW Hansen and Henriksen (2013), and one with detuned gains. In case of original gains, wind turbulence is inside the CPC bandwidth (0.074 Hz): at the controller cut-off frequency the wind spectrum is around 3% of it's maximum value. Wave loads are just above the cut-off frequency (how much above depends on the sea state). The FB controller with original gains rejects the wind disturbance, but is ineffective against wave. In case of detuned FB, the bandwidth is shorter (0.019 Hz): the wind spectrum is 18.6% of its maximum value at the controller cut-off frequency. Moreover, the disturbance sensitivity in the controller bandwidth is increased as the rotor-speed tracking performance is degraded. Hence the controller is less effective against the wind disturbance. The effectiveness of CPC with detuned gains is decreased, but detuning is needed to make the floating system stable without modifying the structure of the FB controller. As it has been shown by Larsen and Hanson (2007); van der Veen et al. (2012); Lackner (2009) when onshore tuning is utilized CPC may lead to unstable response of the platform pitch mode. Bandwidth of the FB controller, and hence its effectiveness against wind turbulence, could be increased by means of NMPZ-compensation (Fischer (2013)) where pitch control is used in combination with dynamic generator-torque. Another possibility is to replace the FB controller with a more complex multivariable controller, as done by Lemmer et al. (2016). Both techniques can be used in synergy with feedforward control to further improve the floating wind turbine response to environmental loads. Interestingly, the capacity of the FB controller of rejecting wave loads is not influenced much by detuning. Comparison of the sensitivity function for the FB and FBFF controller (notice that  $S_{fbff}$  is defined with respect to wave disturbance, whereas  $S_{fb}$  is valid for any disturbance), shows that sensitivity to waves is greatly reduced by addition of wave-FF.

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**Figure 5.** The sensitivity function of the feedback (FB) controller for onshore and offshore tuning, and of the feedback-feedforward (FBFF) in 16 m/s wind is compared to the typical PSD of wind and waves (magnitude has been rescaled to ease the comparison with sensitivity functions). The vertical dashed lines are the frequency of the platform surge and pitch modes, the dotted lines mark the bandwidth of the FB controller with onshore and offshore gains.

The disturbance-rejection function is derived from the sensitivity function and it directly relates the wave disturbance to the closed-loop rotor speed. For the FB and the FBFF controllers it is defined respectively as

$$\begin{aligned} T_{fb} &= S_{fb} G_d , \\ T_{fbff} &= S_{fbff} G_d . \end{aligned} \tag{16}$$

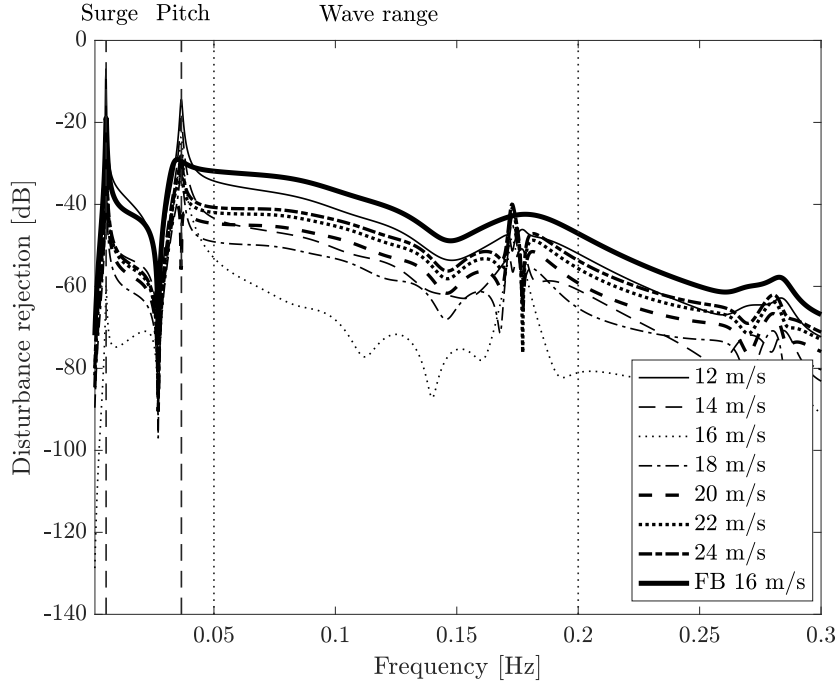
300 The disturbance-rejection function of the FB and FBFF controllers at 16 m/s wind speed is shown in Fig. 6 (thick solid line and thin dotted line). The magnitude of  $T_{fb}$  is increased in correspondence of the platform pitch mode and at higher frequencies. Collective-pitch-FB control results into a decreased damping of the (closed-loop) pitch mode Larsen and Hanson (2007); van der Veen et al. and consequently, to a large resonant response, which translates into large fluctuations of the apparent wind speed at the platform pitch frequency. The bandwidth of the FB controller is 0.0186 Hz. This low value is the consequence of the gain detuning required to stabilize the FOWT van der Veen et al. (2012); Lackner (2009); Fontanella et al. (2018); Lemmer et al. (2020c)

305 Above this frequency the controller does not react to the wind speed fluctuations associated to the wave disturbance.  $T_{fbff}$  is higher than  $T_{fb}$  around the platform pitch natural frequency. Combining the FB controller with the FF controller strengthens the coupling between platform pitch and rotor speed.

The disturbance-rejection function of the FBFF controller is computed for different above-rated wind speeds  $U_i$

$$T_{\text{fbff}}(U_i) = S_{\text{fbff}}(U_i)G_d(U_i) . \quad (17)$$

with  $U_i = 12, 13, \dots, 24 \text{ m/s}$  and  $S_{\text{fbff}}(U_i)$  already obtained in Eq. (15). The magnitude of  $T_{\text{fbff}}(U_i)$  is shown in Fig. 6. The disturbance-rejection function, and so the performance of the FBFF controller, is sensitive to the mean wind speed. This is due to the rotor aerodynamics which changes for different operating conditions. The benefit of ~~the additional FF-controller~~ wave-FF is maximum at 16 m/s, the operating point considered for model inversion, lower elsewhere, and minimum in 12 m/s wind.  $T_{\text{fbff}}$  is higher than  $T_{\text{fb}}$  around the platform pitch natural frequency. Combining the FB controller with the FF controller strengthens the coupling between platform pitch and rotor speed.



**Figure 6.** Disturbance-rejection function of the feedback-feedforward controller in above-rated winds. The feedback controller (FB) in 16 m/s wind is reported for comparison. The vertical dashed lines are the frequency of the platform surge and pitch modes, whereas the frequency range where waves are active is enclosed by the vertical dotted lines.

## 5.2 Gain scheduling

The ~~wave disturbance effect on the FOWT is sensitive to the mean~~ FOWT dynamics (i.e. the response for a given input) depends on the mean wind speed. The turbine is more sensitive to variations of blade pitch angle in high winds, and this is visualized in the input-output analysis of Fig. 1. As shown in Fig. 2, sensitivity to waves remains constant, and does not depend significantly

on wind speed. The control effort required to counteract a given wave is different depending on wind speed, because the wind turbine responds in a different way to blade-pitch angle variation. Intuitively, the pitch action required to reject the effects of a given wave is lower in high winds. To have the maximum possible reduction of the wave disturbance, the FF controller needs to take into account consider how the FOWT dynamics are modified with the operating condition operating condition, and a gain-scheduling strategy is introduced for this purpose.

Based on the procedure introduced above, a linear model of the FOWT is computed for several above-rated wind speeds and, by means of Eq. (13), an FF controller is obtained for each of them. The transfer function of the FF controllers is shown in Fig. 7. From visual inspection of the figure, it is evident that the effort required to cancel the wave disturbance is maximum in near-rated winds and decreases in high winds. If the FF controller obtained from the 16 m/s model is used at any wind speed, the FF action would be less-than-ideal for wind speeds between rated and 16 m/s, and higher-than-ideal for greater wind speeds, leading to a decreased performance, as highlighted by the disturbance rejection analysis of Fig. 6.

Figure 7 also reveals the shape of the FF controller does not change much with wind speed except for the static gain. Based on this consideration, the performance of the FF controller is improved by adjusting the static gain based on the actual wind turbine operating condition. In other words, a single FF controller is computed for the 16 m/s condition and the static gain is modified as the wind speed changes, to reflect the different changed dynamics of the FOWT. The actual collective-pitch angle is chosen as the scheduling variable. The gain-scheduling law is obtained fitting a quadratic function to the DC-gain of the  $K_{ff}(j\omega)$  computed for different above-rated winds. The scheduled FF controller is

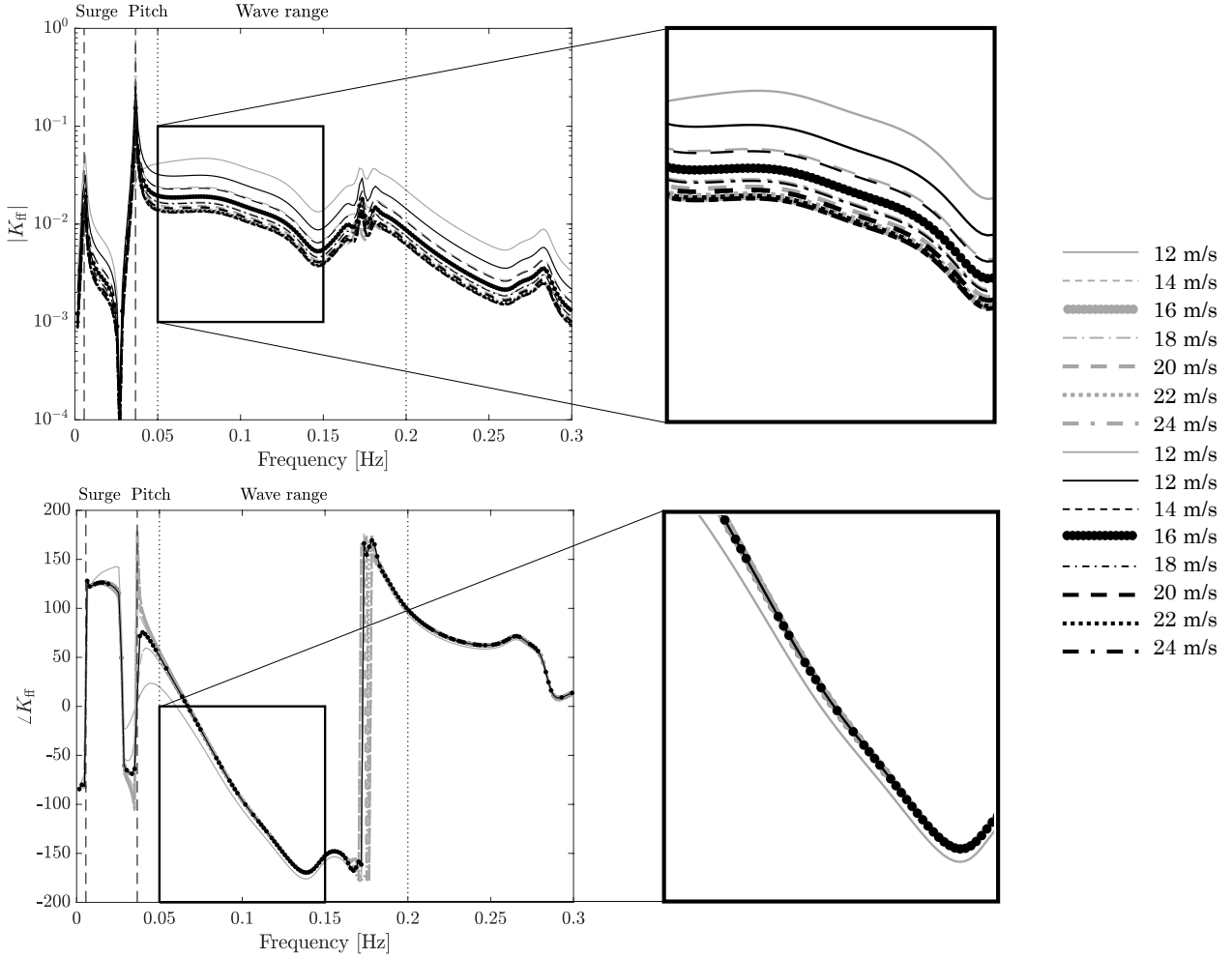
$$\begin{aligned} K_{ff}(\beta) &= c_{ff}(\beta) K_{ff}(\bar{U}) , \\ c_{ff}(\beta) &= p_2 \beta^2 + p_1 \beta + p_0 , \end{aligned} \tag{18}$$

where  $p_2, p_1, p_0$  are the coefficients of the quadratic best-fit function,  $\beta$  is collective-pitch, and  $K_{ff}(\bar{U})$  is the FF controller for 16 m/s wind speed.

In Fig. 7, the scheduled FF controllers  $K_{ff}(\beta) = c_{ff}(\beta) K_{ff}(\bar{U})$  are compared to the model-inversion FF controllers obtained from the evaluation of Eq. (13) for different above-rated wind speeds. The scheduled controller is a good approximation of the ideal case. The proposed scheduling strategy leaves the phase of  $K_{ff}(j\omega)$  unchanged, but this is acceptable since the phase does not change much with wind speed.

The disturbance rejection function of the FBFF controller with scheduling is obtained by replacing  $K_{ff}(\bar{U})$  with  $K_{ff}(\beta)$  in Eq. (15) and Eq. (17) and it is shown in Fig. 8. The disturbance rejection in the wave frequency range is lower for any wind speed, as the controller action is adjusted based on the wind turbine operating condition.

The FF controller for implementation is obtained as in Eq. (18). The order of the transfer function  $K_{ff}(\bar{U})$  is too high for practical usage: a reduced-order approximation is utilized in place of the original transfer function. The low-pass filtered collective-pitch angle measurement is used for scheduling.



**Figure 7.** The scheduled feedforward controllers  $K_{ff}(\beta) = c_{ff}(\beta)K_{ff}(\bar{U})$  (black) obtained from the scheduling of the 16 m/s controller  $K_{ff}(\bar{U})$  (dasheddotted line) are compared to the model inversion controllers  $K_{ff}(U_i)$  (grey) for different above-rated wind speeds  $U_i = 12, 13, \dots, 24$  m/s. Magnitude (lefttop) and phase (rightbottom). Wave range is the frequency range where linear wave is active.

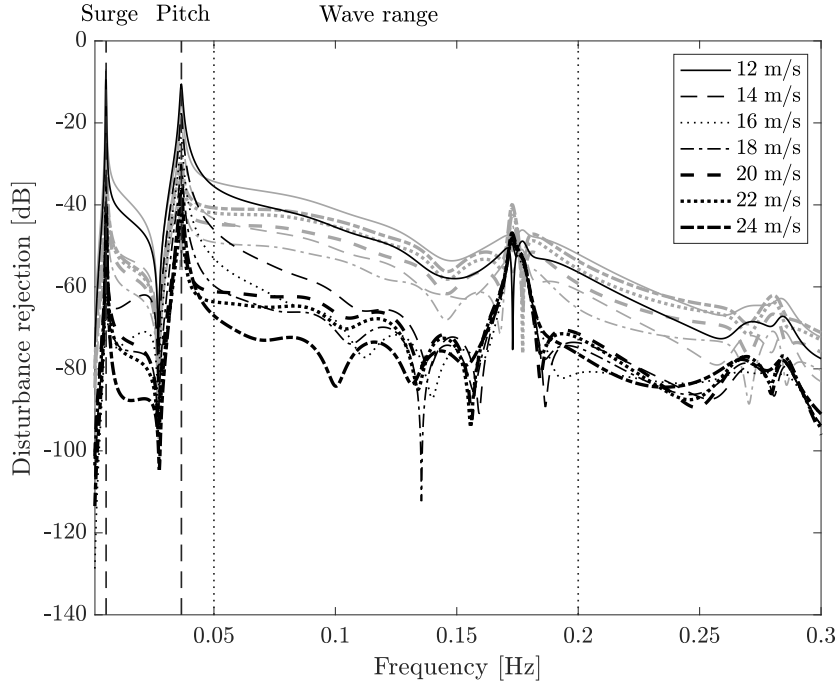
## 6 Wave measurement and prediction

The transfer function of the FF controller has an intrinsic delay of  $t_d$ . A suitable wave elevation measurement is required to compensate the intrinsic delay of the FF controller: it is required to know the wave  $t_d$  before it arrives at the platform. The wave prediction is obtained from a measurement of the surface elevation in a point at a distance  $l$  upstream the platform. The measurement is propagated downstream in space and forward in time.

The wave elevation in two points along the wave propagation direction is related by the frequency response function

$$H_l = e^{-jkl}, \quad (19)$$





**Figure 8.** Disturbance rejection of the FBFF controller with scheduling (black) and without (grey), for several above-rated operating conditions. The vertical dashed lines are the frequency of the platform surge and pitch modes, the frequency range where waves are active is enclosed by the vertical dotted lines.

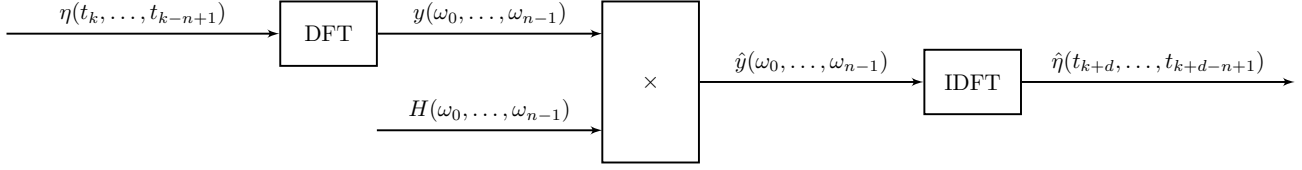
where  $k$  is the wave number, and, for gravity waves on deep-water,  $k \approx \omega^2/g$ .

The frequency response function that relates the upstream wave measurement to the wave prediction at the FOWT is

$$H(j\omega) = e^{j\omega(t_d - \frac{\omega l}{g})}. \quad (20)$$

For a given distance  $l$  and a preview time of  $t_d$ ,  $H(j\omega)$  behaves as a pure negative-delay operator only for  $\omega > gt_d/l = \omega_t$ . The wave spectral components with a frequency greater than  $\omega_t$  are successfully predicted. Prediction of the wave components with a lower frequency is not possible, because the wave arrives at the platform location in a time lower than the preview time  $t_d$ . It is possible to predict the lower-frequency harmonics by measuring the wave elevation far upstream the FOWT or by decreasing the preview time.

For real-time control purposes, the wave prediction model of Eq. (20) is implemented as it is shown in Fig. 9. The wave elevation  $\eta$  is continuously measured in  $l$  meters upstream the floating wind turbine with a sample rate  $T_s$ . At any time instant  $t_k$ , the discrete Fourier transform (DFT) of the last  $n$  samples is computed to obtain the complex spectrum  $y$ . The element-wise product between  $y$  and the transfer function  $H$ , evaluated at  $n$  discrete frequencies  $\omega_i = (2\pi i/nT_s)$ ,  $i = 0, \dots, n-1$ , gives the spectrum of the predicted wave elevation at platform location  $\hat{y}$ . The Inverse DFT of  $\hat{y}$  gives  $\hat{\eta}$ , which is the wave elevation that is going to be experienced by floating wind turbine  $d = t_d/T_s$  time samples ahead in time.



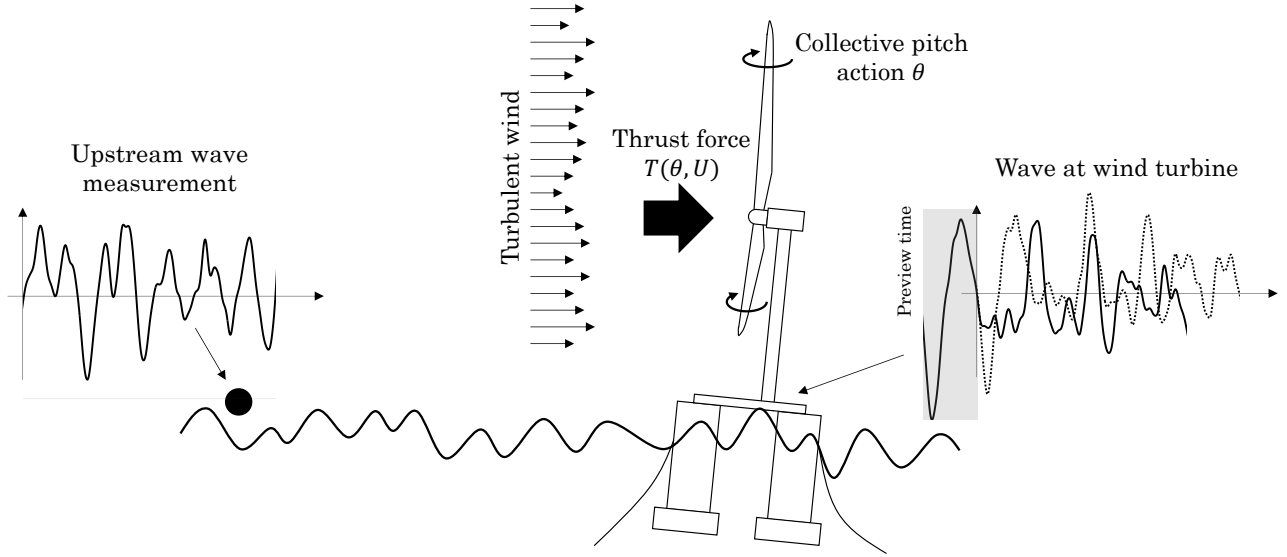
**Figure 9.** Scheme of the wave prediction algorithm.  $\eta$  is the wave elevation measurement upstream the floating wind turbine and  $\hat{\eta}$  is the wave elevation at platform location,  $d = t_d/T_s$  time samples ahead in time.

Several technologies are available to measure the surface elevation. Some examples are wave-rider buoy, radar, airborne or satellite. The radar technology is particularly attractive because it scans a large area, it detects waves far from its location (up to 4 km) and it is capable of fully autonomous operation. The X-band radar, commonly used by ships for navigation, received a lot of attention as a remote wave sensor. Images of the wave field are obtained from the radar as radar beams are reflected and shadowed by the crests of the wave fronts. An example of this technology is the wave monitoring system WaMoS II ~~presented in~~ [introduced by](#) Ziemer and Dittmer (1994) and at the base of the real-time wave-prediction system developed [by Reichert et al. \(2010\)](#) within the On board Wave and Motion Estimator (OWME) ~~Reichert et al. (2010).~~ ~~In Naaijen and Wijaya (2014) a~~. A methodology based on 2D-FFT is proposed [by Naaijen and Wijaya \(2014\)](#) to obtain a directional phase-resolved prediction of the wave elevation from radar data (additional information about the directional energy spectrum is required, e.g. from a wave buoy). A similar measurement could be used in wave-FF control.

## 7 Results

The wave-FF control strategy is evaluated by means of numerical simulations in the servo-aero-hydro-elastic code FAST ~~Jonkman and Marshall (2005)~~ [\(Jonkman and Marshall \(2005\)\)](#). The FAST model has 7 DOFs: platform motions (surge, sway, heave, roll, pitch and yaw) and the rotor rotation. The drivetrain is rigid as well as the tower and blades. The hydrodynamic model is based on linear potential flow theory with viscous effects. The radiation and the first-order wave forces are computed prior to the simulation based on the same WAMIT data that are used to build the control-design model. The calculation of the frequency-dependent radiation loads is based on the convolution integral of the retardation functions matrix. Second-order wave loads are modeled by means of ~~Newman's approximation~~ [the approximation technique introduced by](#) Newman (1974).

The wave-FF control strategy considered for the verification is displayed in Fig. 10. Three cases are considered: a baseline case with only FB control, the FBFF control without gain scheduling, and the FBFF control with gain scheduling. In the simulations, an ideal upstream wave measurement is used and the accuracy of the wave measurement system (e.g. radar) is not taken into account. Results are therefore indicative of the upper performance limit of wave-FF control.



**Figure 10.** Schematics of the wave-feedforward control strategy. Wave excite the floating platform and generate a varying apparent wind speed for the rotor. The oscillating wind results into rotor speed fluctuations which are only partially rejected by the standard feedback controller. The feedforward action is based on the wave elevation measured upstream the wind turbine. This measurement is used to obtain a preview of the wave elevation at the floating platform, which is the input of the controller. The resulting collective-pitch action, which is summed to the pitch request from the feedback controller, counteracts the wave disturbance, modifying the aerodynamic torque and the rotor thrust force.

## 7.1 ~~The environmental~~ Environmental conditions

395 ~~The floating wind turbine is subjected to three~~ Three realistic turbulent wind and irregular wave combinations (see table 1), representative of an offshore site with moderate-severity met-ocean conditions, are selected for assessing the performance gains of the wave-FF control strategy. The reference offshore site is part of the Gulf of Maine (North Atlantic ocean), about 25 km southwest of Monhegan Island ~~and~~ 65 km east of Portland, and the mean water depth is 130 m. Met-ocean data for the site are reported by Gonzalez et al. (2015). Three above-rated winds ~~were selected and, for any of them, the are considered,~~ that are defined by the parameters of Tab. 1. For any condition, wave was defined ~~from~~ according with the Pierson-Moskowitz spectrum. The significant-height  $H_s$  and peak-period  $T_p$  were selected as the most probable combination of values for ~~any the~~ assigned wind speed. ~~For wind, a power-law profile with exponent 0.14 is assumed, turbulence is modeled according to the Kaimal spectrum and turbulence intensity is selected for each wind speed based on the IEC-61400, considering a wind turbine of class IC.~~ Wind and waves are aligned to the zero-degree direction.

400

**Table 1.** ~~Met-ocean~~Met-ocean conditions considered for the verification of the wave-FF control strategy.

Hub-height mean wind speed [m/s]	Turbulence intensity [%]	Significant wave height [m]	Wave peak period [s]
16	12	1.5	10.0
18	11	2.5	10.0
22	10	3.5	8.0

405     ~~The FB and the two FF control strategies are simulated for all the metocean conditions of table 1. For any load case, six simulations are carried out with wind and waves generated from different random seeds. Each simulation lasts 1600 s, and only the last 600 s worth of data are considered for the analysis.~~

**7.2   Wave prediction**

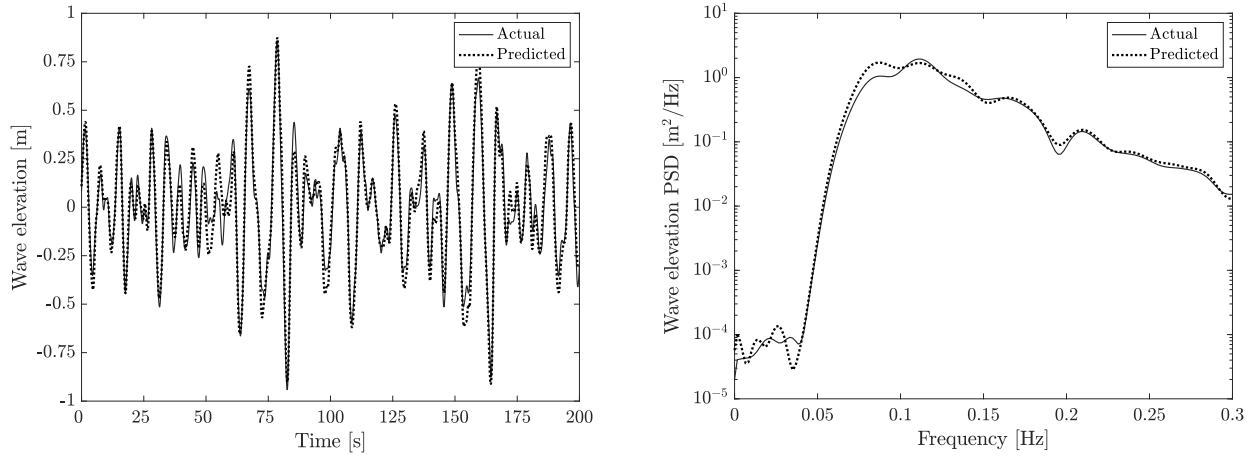
The wave prediction algorithm presented in section 6 is tested in the met-ocean conditions corresponding to the 16 m/s mean  
410     wind speed case of table 1. The wave elevation is sampled every 0.1 s at distance of 200 m upstream the FOWT. The wave  
elevation at platform location is computed based on the last 1000 samples and a preview time of 7.5 s is requested. The wave  
elevation preview is compared to the wave at platform in Fig. 11. The overall quality of the estimate is good. The PSD of  
the two signals reveals that the largest error is introduced in the low-frequency harmonics. The error is due to the intrinsic  
characteristics of the transfer function on which the wave prediction algorithm is based. For the present case, the transfer  
415     functions correctly predicts the wave harmonics above a threshold frequency of 0.058 Hz.

**7.3   Steady wind**

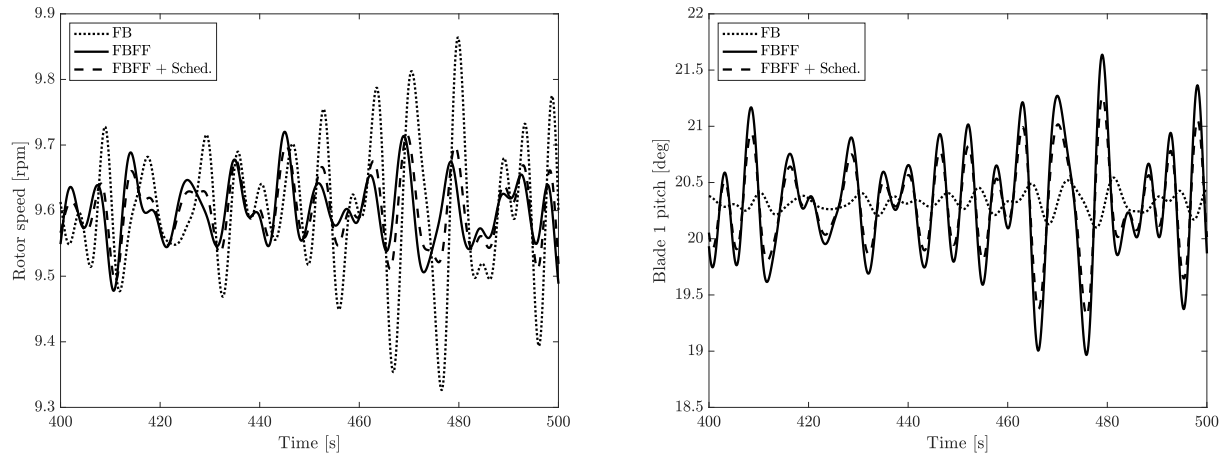
The effect of the FF control strategy is first demonstrated considering a steady wind without shear. With this assumption, the  
wave is the only disturbance acting on the FOWT. Sample time series of the rotor speed and blade pitch command for a 22  
m/s wind speed case are shown in Fig. 12. The amplitude of rotor speed oscillations caused by the wave disturbance is reduced  
420     with FBFF control with respect to the FB case, and this is achieved at the expense of an increased pitch activity. The pitch  
effort required by the scheduled FBFF is less than without scheduling for a comparable disturbance rejection performance.

**7.4   Turbulent wind**

The FBFF control is evaluated in more realistic power production conditions. Turbulent wind fields were generated in turbsim  
(Kelley and Jonkman (2007)) with Kaimal spectrum, a power-law profile with exponent 0.14, and turbulence intensity selected  
425     for each mean wind speed according with the IEC-61400 (class IC turbine). For every condition of Tab. 1, six independent  
wind-wave realizations, each 10-minutes long, were considered, as recommended by the IEC 61400 standard (IEC (2005)) to



**Figure 11.** Left: the wave preview obtained by means of the prediction algorithm is compared with the wave at platform location (in the plot, the preview is delayed of the preview time  $t_d = 7.5\text{s}$  to ease the comparison). Right: the wave preview and measurement are compared based on their PSD.

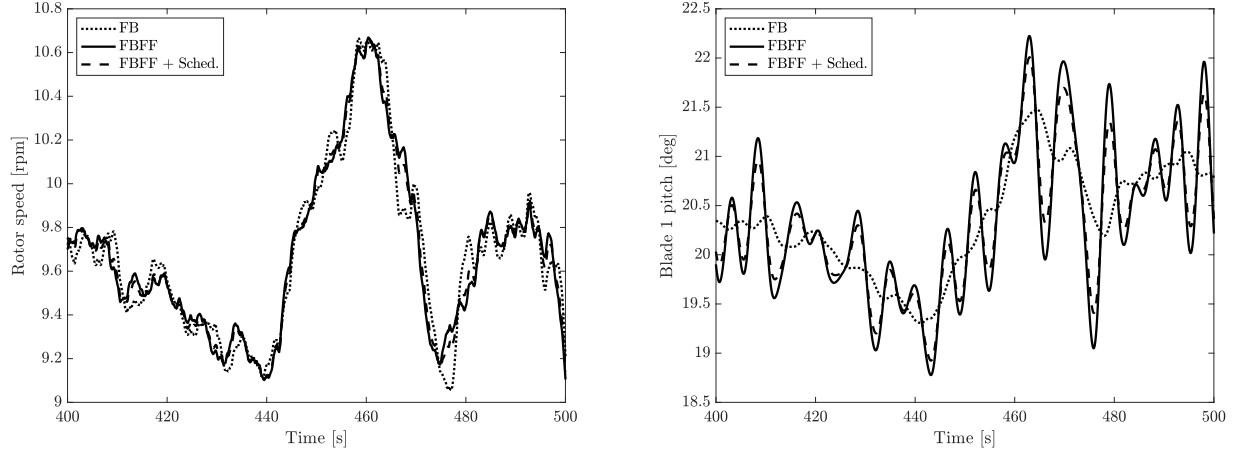


**Figure 12.** Time series of the rotor speed (left) and blade 1 pitch angle command (right) for the 22 m/s steady wind case.

get statistically-significant data. An initial pre-simulation time of 1000s was included at the beginning of each simulation and cut-out from results to exclude initial transients.

Sample time series of rotor speed and ~~blade-pitch~~blade-pitch angle for the 22 m/s case are shown in Fig. 13. As visible  
 430 looking at the FB case, the largest fraction of rotor speed oscillations is ~~set-by~~due to wind turbulence. This is in agreement  
 with the MIMO disturbance analysis of section 4. The FF control reduces the part of rotor speed oscillations caused by waves,

but it does not compensate for the effect of wind turbulence. The pitch actuation is increased with any FBFF compared to the FB case.



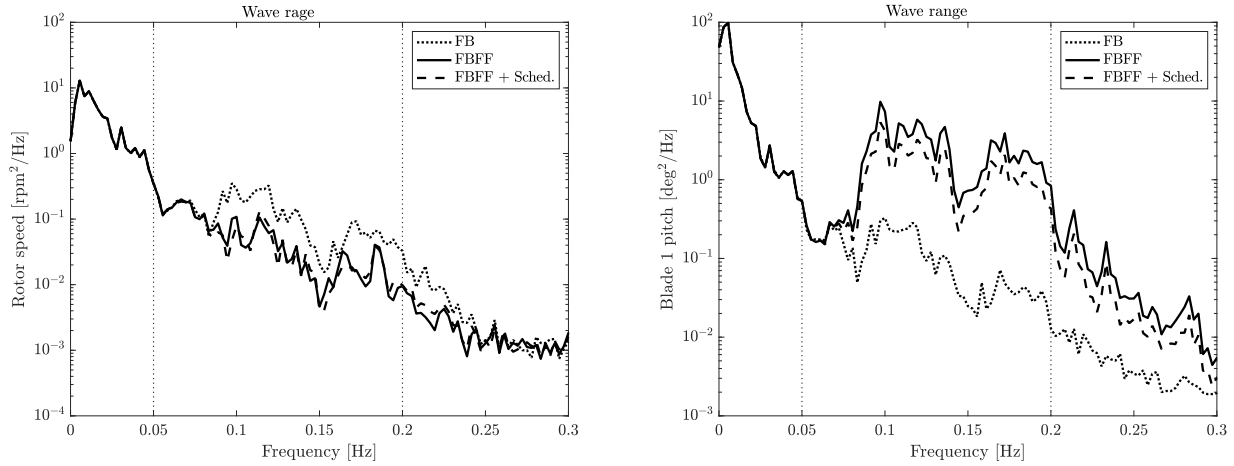
**Figure 13.** Time series of the rotor speed (left) and blade 1 pitch-angle-command (right) for the 22 m/s turbulent wind case.

The power spectral density (PSD) of the rotor speed and pitch-angle-command is computed from the aggregated time series of Fig. 13 is shown the six seeds relative to the same operating condition. Results for the 22 m/s case are reported in Fig. 14. The FBFF achieves a clear reduction of the rotor speed dynamics in the frequency range where wave is active (FBFF clearly reduces the energy content of rotor speed associated with wave excitation (wave range, 0.05 Hz–0.2 Hz–0.2 Hz), but it has a small impact has a negligible effect at lower frequency, where the rotor speed oscillations are largely set by in large part due to wind turbulence. Scheduling slightly improves the disturbance rejection and significantly lowers the control effort. The FF action results into an additional blade-pitch command which energy content is concentrated in the wave range. Rejection of wave disturbance is slightly improved by the addition of scheduling (FBFF + Sched.), which requires also a lower blade-pitch effort compared with FBFF.

The FF control Wave-FF is designed to reduce the wave disturbance effect on rotor speed effects of wave disturbance and improve rotor speed regulation. However, it is expected it affects to affect also the structural loads for the different wind turbine components and the motion of floating platform. The fatigue loads are studied turbine components. Fatigue loads for each operating condition are evaluated in terms of damage-equivalent loads (DEL), which are calculated by means of Rainflow counting with an equivalent load frequency of 1 Hz and a Whöler exponent of 10 for the steel components (shaft, tower and mooring line) and 3 for the blades. The DEL percentage variation that is achieved with FBFF compared to FB is computed as

$$\Delta \text{DEL} = \left( 1 - \frac{\text{DEL}_{\text{FB}}}{\text{DEL}_{\text{FBFF}}} \right) \cdot 100 ,$$

where  $\text{DEL}_{\text{FB}}$  and  $\text{DEL}_{\text{FBFF}}$  are the 1 Hz damage equivalent computed with mLife (Hayman and Buhl (2012)). Wave-FF is also expected to affect platform motions, and this is quantified by the standard deviation of platform surge, roll and pitch.



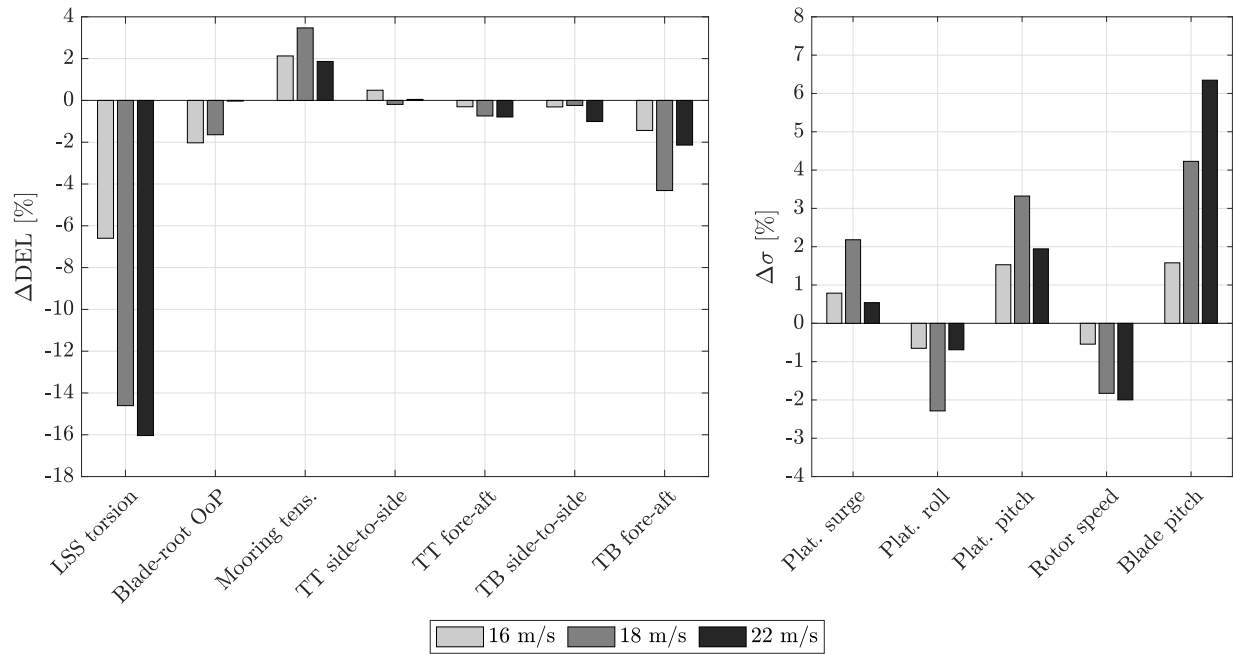
**Figure 14.** Power spectral density of ~~the~~ rotor speed (left) and blade 1 pitch angle command (right) aggregated time series of six seeds for the 22 m/s turbulent wind case. Wave range is the frequency range where linear wave is active.

DEL and standard deviations are computed for every operating condition based on the aggregated time series of six seeds. Variation of DEL and standard deviations with FBFF + Sched. compared with FB is examined in Fig. 15 for the three load cases. The LSS-torsion DEL is reduced up to 16%. The LSS-torque depends on the aerodynamic and generator torque. The  
 455 wave-FF reduces the aerodynamic torque oscillations caused by waves and so the fatigue loads for the ~~FB and the FBFF.~~

~~The DEL the FOWT components and the standard deviation of platform motions, rotor speed and blade pitch is examined in Fig. 15 for the three load cases. Only the case of FBFF with scheduling is considered. Reducing rotor speed oscillations also results into a lower fatigue damage for the wind turbine shaft and tower; platform motions are slightly increased LSS. The lower dynamics of LSS-torque is reflected in the platform roll-motion which is reduced as well. The highest LSS-torsion~~  
 460 DEL reduction is achieved in high winds when waves are the strongest. Blade pitch is increased because of the additional wave-FF command, and ~~this is reflected into the mooring line loading~~ the increment is proportional to the strength of waves. As demonstrated in the input-output analysis of §4, aerodynamic torque and rotor thrust are both affected by blade-pitching. The modification of the thrust force induced by wave-FF impacts the along-wind platform motions and the tower-FA loads. Platform surge and pitch motions are increased, with consequently higher fatigue loads for the mooring system, and lower  
 465 loads for the tower. It is counterintuitive, but larger motions imply lower tower loads. As noticed by Fleming et al. (2016), a smooth motion of the nacelle releases the energy introduced by waves, which therefore is not put into tower bending.

## 8 Conclusions

This paper investigated a model-inversion feedforward control strategy for ~~the~~ mitigation of wave ~~disturbance-excitation~~ in floating offshore wind turbines. A linear control-design model is utilized to carry out an MIMO analysis of the floating wind



**Figure 15.** ~~The damage~~ Damage equivalent load (DEL) and standard deviation ( $\sigma$ ) with FBFF + Sched. for three above-rated power production conditions. ~~Statistics for every operating conditions were obtained from aggregated time series of six seeds.~~ A negative  $\Delta$  means a reduction with respect to ~~feedback-only~~ FB-only control. LSS stands for low-speed shaft, OoP for out-of-plane, TT for tower-top and TB for tower-base.

470 turbine. Collective-pitch is more effective than generator torque for ~~rotor-speed-control~~ controlling rotor-speed in above-rated winds. Above the platform natural frequencies, wave equally affects rotor and platform motions, with ~~a strength comparable to wind speed~~ the same strength of wind turbulence. Based on linear analysis, a model-inversion feedforward controller is designed for canceling the wave-induced ~~rotor-speed (and generator power)~~ rotor-speed (and generator-power) oscillations using collective-pitch. The feedforward controller is added to an industry-standard feedback controller. ~~The and the~~ performance

475 improvement is demonstrated by means of linear analysis. A gain-scheduling algorithm is devised to improve the controller performance by adapting the feedforward action as the wind turbine operating condition changes. The control strategy is finally verified by means of time-domain simulations in a non-linear aero-servo-hydro-elastic model. It is found that feedforward control can reduce the standard deviation of rotor speed up to 2%. It also has a positive side effect on the ~~damage-equivalent load~~ fatigue loads of several wind turbine components: the shaft torsion is reduced ~~of 15~~ up to 16%, the tower-base fore-aft

480 bending ~~of up to~~ 5%. Platform motions are ~~however slightly increased~~ slightly increased, and this is reflected into the mooring line loads. ~~The blade-pitch actuator usage is increased.~~ Wave-FF control improves the dynamic response of the floating turbine without requiring the replacement of the industry-standard feedback controller. A wave-measurement and forecast system must be implemented, but this is feasible to get with technologies already used in the maritime industry. The extra cost of



the wave-measurement system, and fatigue of the blade-pitch actuators is likely to be offset by the lower cost of the turbine generator and tower, which can be redesigned in reason of the reduced overspeed and fatigue loads, respectively.

The following suggestions should be considered in future work about wave-based and wave-feedforward control in floating wind turbines:

- the wave-feedforward controller is sensitive to accuracy of wave-elevation prediction and to fidelity of the wave disturbance model. The focus of this work is about development of the wave-feedforward control strategy and did not addressed the topic of uncertainties In the present work, uncertainties in the wave measurement are only due to the preview algorithm and, as it is shown, the prediction error is small. Larger errors are expected when using a realistic measurement of upstream waves. Model uncertainties are mostly related to identification of the wave-excitation model. The model we consider here has been assessed against a medium-fidelity model in a previous work (Fontanella et al. (2020)) and was deemed sufficiently accurate for control-design. In-depth analysis of the controller robustness with respect to model and measurement uncertainties should be addressed in future works. Implementing the wave-FF control in FOWTs based on different platform typologies may reduce uncertainty about the benefits of this control strategy;
- the proposed feedforward controller is linear and compensates only for first-order wave loads. Recent numerical and experimental studies proved, for example the one of Roald et al. (2013), prove that second-order wave loads have a noticeable effect on the response of the floating wind turbine Roald et al. (2013) a floating turbine response. Thus, a first possible research suggestion is to investigate non-linear controllers and to include second-order hydrodynamics in the controller design;
- in the control-design model, rotor aerodynamics are modeled based on the quasi-steady theory. Thus, the controller obtained from the model does not account for unsteady aerodynamic effects, which may be significant for the response in the upper wave-frequency range Mancini et al. (2020) (Mancini et al. (2020)). It is therefore suggested to develop a control-oriented model of the unsteady rotor aerodynamics and to include it in the control-design model, so to investigate how unsteadiness affects the response of the controlled FOWT;
- in the case at hand, the feedforward controller is designed to regulate rotor speed, and the reduction of fatigue tower loads is obtained as a positive side effect. As it has been shown, a large part of rotor speed oscillations A large fraction of tower loads is caused by wind turbulence; the wave disturbance drives platform motions and, consequently, it is cause of increased tower fatigue loads. It is therefore wave, so it is advisable to use the wave information to control the platform motions and use another controller, that also includes the wind measurement, to reduce rotor speed and power fluctuations reduce tower fatigue loads;
- the wave prediction model may find application in several control-related tasks, which are not envisioned here. Waves drive the rigid-body motion of the floating platform, which in turn turbine, and this is likely to have an effect on the wind turbine wake affect the turbine wake (Wise and Bachynski (2020)). Wave prediction may be included in future floating wind farm control strategies;

- single-input single-output feedback controllers remain the default choice in floating wind turbines and advanced controllers are still far from reaching commercial projects. Tighter relationships between industry and academia are advisable to promote the adoption of advanced control strategies.

520 *Author contributions.* AF and MA developed the wave feedforward control methodology in all its aspects. MB and JWvW supervised the research activity mentoring AF and MA. Finally, AF prepared the manuscript of this article with contribution from all co-authors.

*Competing interests.* The authors declare that they have no conflict of interest.

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