

1 Current status and grand challenges for small wind turbine 2 technology

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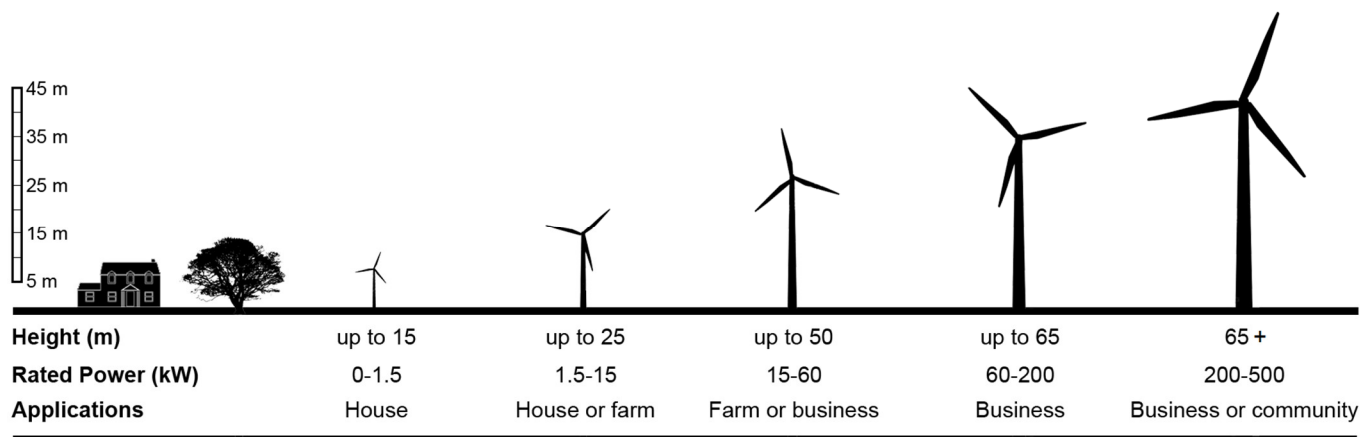
25 **Abstract.** While modern wind turbines have become by far the largest rotating machines on Earth with further upscaling
26 planned for the future, a renewed interest in small wind turbines is fostering energy transition and smart grid development.
27 Small machines have traditionally not received the same level of aerodynamic refinement of their larger counterparts, resulting
28 in lower efficiency, lower capacity factors, and therefore a higher cost of energy. In an effort to reduce this gap, research
29 programmes are developing worldwide. With this background, the scope of the present study is twofold. In the first part of this
30 paper, an overview of the current status of the technology is presented in terms of technical maturity, diffusion, and cost. The
31 second part of the study proposes five grand challenges that are thought to be key to fostering the development of small wind
32 turbine technology in the near future, i.e.: (1) improve energy conversion of modern SWTs through better design and control,
33 especially in the case of turbulent wind; (2) better predict long-term turbine performance with limited resource measurements
34 and prove reliability; (3) improve the economic viability of small wind energy; (4) facilitate the contribution of SWTs to the
35 energy demand and electrical system integration; (5) foster engagement, social acceptance, and deployment for global

36 distributed wind markets. To tackle these challenges, a series of unknowns and gaps are first identified and discussed. Based
 37 on them, improvement areas are suggested for which ten key enabling actions are finally proposed.

38 **1 Introduction**

39 A major portion of today's installed wind power is in the form of large wind power plants, which mainly consist of multi-MW
 40 machines (GWEC, 2020), while a clear trend in further upscaling of both rated power and dimension is ongoing (Veers et al.,
 41 2019). Small wind turbines (SWTs) are, however, still visible around the world for a variety of applications, including electric
 42 power generation for households, industrial centres, farms, and isolated communities; combining with other energy sources
 43 and storage in hybrid energy systems for electricity to support remote monitoring and telecommunications; and providing
 44 direct energy services for applications such as water pumping, desalination, and purification (Chagas et al., 2020). The use of
 45 wind turbines in rural areas is of particular relevance for some countries; for example, around the horn of Africa, small wind
 46 systems are the most viable solution in the scarcely electrified parts of those countries (Gabra et al., 2019). (Karekezi, 2002)
 47 reported that South Africa has more than 100,000 wind pumps in operation used over 45,818 farms. SWTs are a subset of a
 48 larger distributed wind market segment that can include large turbines installed in distributed applications. Figure 1 associates
 49 typical distributed turbine sizes to their main types of application.

50



51

52 **Figure 1 - Small and distributed wind turbine dimensions and rated power outputs as a function of various applications.**

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54 When SWTs are used for a variety of ancillary purposes other than electricity production such as ventilation or water pumping,
 55 different turbine concepts can come to play. These applications may use the Savonius vertical-axis turbine (Akwa et al., 2012)
 56 or the multi-blade American windmill (Baker, 1985), which constitute a small space in the market. Although these machines
 57 are in all respects SWTs, they are not discussed in the present study, which instead focuses on SWTs for electricity production.

58 Before moving forward, a key element of this study is defining what is meant by “small wind turbine.” A universal consensus
59 on this has not been reached, with the International Electrotechnical Commission (IEC) Standards (IEC: International Standard,
60 2019b) defining SWTs as turbines with a maximum rotor swept area of 200 m²; the same threshold is applied to eligible
61 turbines for certification by the AWEA Small Wind Turbine Performance and Safety Standard 9.1-2009; however, a new
62 American National Standards Institute consensus standard, ACP 101-1, is being developed by the American Clean Power
63 Association (ACP), the successor to AWEA. ACP 101-1 is intended to eventually supersede the AWEA 9.1-2009 standard
64 (Summerville et al., 2021). Several countries use rated power as the key differentiator, and ACP 101-1 thus defines SWTs as
65 having a peak power of 150 kW or less and microturbines as having a peak power up to 1 kW. In Brazil, small wind systems
66 are categorized as power stations (which could be composed of one or many wind turbines) with a total rated capacity below
67 100 kW, according to Resolution 438/2012 of the Brazilian Electricity Regulatory Agency (ANEEL) (Chagas et al., 2020).
68 The importance of having a more comprehensive definition of “small wind” has been recently put in the spotlight. For example,
69 it has been suggested by the Small Wind Turbine Technical Committee of the European Academy of Wind Energy (EAWE)
70 that many problems and technical challenges of SWTs are common to the majority of the rotors up to 500 kW (EAWE, 2020),
71 i.e., also extending to distributed wind turbines (DWTs). As will be further discussed in the present study, it is important to
72 more clearly define those characteristics that make SWTs unique from utility-scale turbines. However, this is not an easy task
73 because significant variability in wind turbine design is also apparent, with no specific size-based design threshold.
74 Additionally, there are a variety of “alternative” configurations available on the open market (Bianchini, 2019), such as
75 vertical-axis turbines (Aslam Bhutta et al., 2012), diffuser augmented wind turbines (Evans et al., 2020), or first prototypes of
76 airborne wind energy (AWE) converters (Meghana et al., 2022). Even though SWTs may still represent a niche application
77 within the wind energy market, they have recently been exhibiting a notable rate of growth concomitant with the diffusion of
78 smart energy systems (Tzen, 2020). This diffusion, however, is still hindered by the typically higher costs of small wind
79 systems. These increased costs are driven by several factors, including a lack of development and system optimization and
80 issues related to those cost items (i.e., electrical connection, resource assessment expenses, installation cost, etc.) that are not
81 proportionally lower for smaller projects (Simic et al., 2013). The growth of the SWT sector is further notable in light of the
82 several published reports showing that SWT installations have failed to reach their expected energy yield, resulting in
83 underperforming turbines. This is particularly true in the case of installations in the urban or built environment (WINEUR
84 project, 2005; Fields et al., 2016). Development in highly complex areas, such as urban locations, is complicated due to the
85 wind conditions in the city's canopy layer, which typically have low intensity, high variability, high levels of turbulence, and
86 inclined or even reversed air flows. While several studies have shown a theoretically good potential for urban wind (Balduzzi
87 et al., 2012; Toja-Silva et al., 2013), a number of challenges still need to be tackled to effectively fit wind energy converters
88 to this environment, as recently discussed by (Micallef and Bussel, 2018) (Stathopoulos et al., 2018). In the present study, the
89 authors decided not to include a specific technical analysis of the needs for urban wind, although future work on the topic has
90 to be encouraged (Battisti, 2018).

91 Even so, projections of SWT deployment in future scenarios of distributed energy production within smart grids (thus in
92 proximity to populated areas) are considered promising. In this sense, SWTs are expected to provide a significant contribution,
93 especially in combination with other renewable energy sources. However, the higher levelized cost of energy (LCOE) of
94 SWTs, especially compared to residential solar photovoltaics (PV), still hampers the massive diffusion of this technology.

95

96 **1.1 A guide to this article**

97 The present study has two main focuses. First, it provides an overview on the status of SWT technology. We present the market
98 diffusion and economics of SWTs (Sections 2–3) with the goal of placing the technology in the current energy market and
99 defining some important threshold values. We then provide a description of the main technical features of SWTs (Section 4)
100 and compare them to those of their utility-scale counterparts. Section 5 pursues the second focus of the work, defining five
101 grand challenges that—per the authors’ assessment—are key to fostering the development of SWTs in the near future. More
102 specifically, a series of unknowns and gaps for SWTs is first defined, and then main improvement areas and prospects are
103 proposed to address those gaps. Finally, Section 6 synthesizes the main outcomes of the study into concluding remarks and
104 defines 10 key enabling actions for achieving the grand challenges in the near future.

105 **2 Diffusion of small wind turbines**

106 There is at least ~1.8 GW of installed small wind capacity globally from over 1 million turbines (Orrell et al., 2021). The
107 global spread of this electrical capacity, including all types of turbines and based on available reports from some key surveyed
108 countries, is shown in Table 1 (asterisks denote a lack of validated data for that specific year). Figure 2 provides a more focused
109 insight into several of those countries, which showed notably different trends in the first years of the last decade, where SWT
110 technology saw one of its more interesting phases. While Denmark, the United Kingdom, and the United States have a long-
111 recorded history of small wind installations, China has added larger amounts of small wind capacity more consistently in recent
112 years. On the other hand, Italy, and the United Kingdom, which saw many installations in the first decade of the century, both
113 experienced recent decreases due to feed-in tariff (FIT) policy changes. FITs provide payments to owners of small-scale
114 renewable generators at a fixed rate per unit of electricity produced, verifying that the cost of the installation is recovered over
115 the lifetime of the generator. In the case of Italy, in particular, the significant increase in installations seen around 2016–2017
116 was due to a special programme of incentives for turbines under 60 kW. The FIT rate in Italy declined over time before expiring
117 in 2017. It was replaced by the FER1 Decree in 2019 (Dentons, 2020). In line with these changes, an estimated 77.46 MW of
118 wind projects using turbines sized up through 250 kW were installed in Italy in 2017, no installation reports were available for
119 2018 and 2019, and 0.65 MW of projects were reported for 2020. The United Kingdom closed its FIT programme to new
120 applicants in 2019 and introduced the Smart Export Guarantee programme. Under that programme, applicants now receive a
121 tariff determined by the buyer rather than a fixed price determined by the government (Ofgem, 2021). Consequently, small
122 wind deployment went from 28.53 MW in 2014 to only 0.43 MW in 2019 (Orrell et al., 2021). In a scenario of decaying

123 government incentives, an outlier case in Europe is Greece (Greek Government Gazette, 2021), which still offers an FIT for
 124 SWTs. At the time of writing this paper, the programme was for 20 MW installed capacity, starting with a tariff of 157 €/MWh
 125 (181 \$/MWh) that will be automatically reduced based on the cumulative contracted power of the projects. A bonus with
 126 respect to the tax break is also in place, which brings the FIT to 163€/MWh (187 \$/MWh).

127

128 **Table 1 - Small wind turbine installations through 2020. Data from (Orrell et al., 2021) and (Chagas et al., 2020). Underlined**
 129 **values refer to years/countries having FIT schemes in place.**

	Installations (MW)										Cumulative (MW) installations	Cumulative Year Range
	Before 2012	2013	2014	2015	2016	2017	2018	2019	2020			
Brazil	0.00	0.03	0.02	0.11	0.04	0.11	0.09	*	*	0.40	2013–2018	
China	280.01	72.25	69.68	48.60	45.00	27.70	30.76	21.40	25.65	610.61	2007–2020	
Germany	24.55	0.02	0.24	0.44	2.25	2.25	1.00	*	*	30.75	As of 2018	
Denmark	*	*	*	*	14.61	2.58	0.40	0.18	0.05	610.88	1977–2020	
Italy	20.99	7.00	<u>16.27</u>	<u>9.81</u>	<u>57.90</u>	<u>77.46</u>	*	*	0.65	190.08	As of 2018	
South Korea	<u>2.99</u>	0.01	0.06	0.09	0.79	0.08	0.06	*	*	4.08	As of 2018	
United Kingdom	77.98	<u>14.71</u>	<u>28.53</u>	<u>11.64</u>	<u>7.73</u>	<u>0.39</u>	<u>0.42</u>	<u>0.43</u>	*	141.51	As of 2019	
United States	130.73	5.60	3.70	4.30	2.43	1.74	1.51	1.30	1.55	152.65	2003–2020	
Other countries	*	1.65	1.32	6.23	5.40	3.39	13.23	*	*	33.72	mixed ranges	
TOTAL										1774.68		

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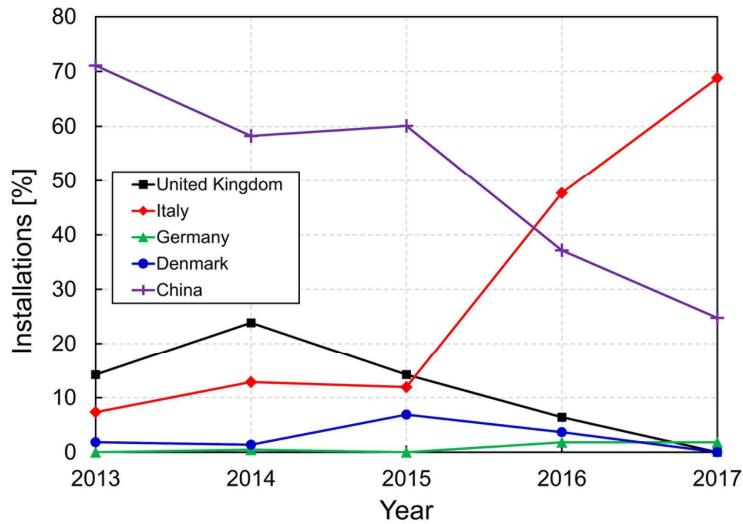


Figure 2 - Evolution of the country's share in the newly installed SWT capacity for that year for a number of key European countries and China. Data from (Orrell et al., 2021).

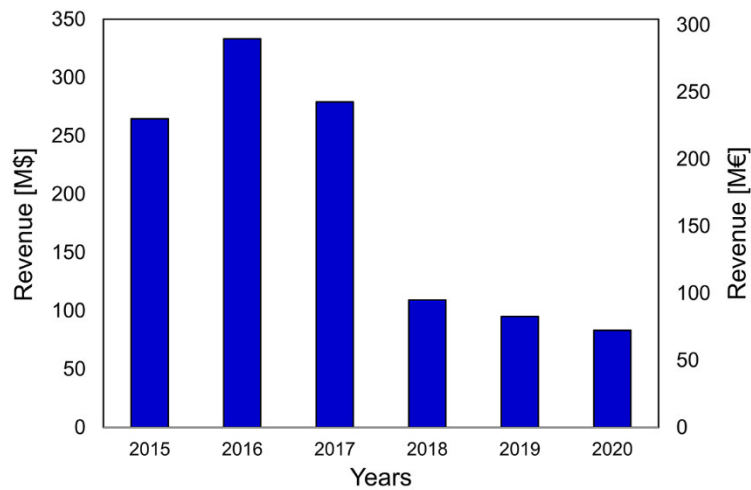
Other examples of these tariffs include those in Japan and the Republic of Korea. Japan's FIT programme was established in the wake of the Fukushima Daiichi nuclear disaster. Its rates have steadily declined, from a peak of ¥55 per kWh in 2015 to ¥19 (approximately¹ 0.125 € or 0.175 \$) per kWh as of 2019 for turbines less than 20 kW (Orrell et al., 2021). The Republic of Korea also had an FIT programme, but it was ended in 2012 and replaced with a renewable portfolio standard (Lo, 2018). While the switch from the FIT programme increased capacities in some renewables in the Republic of Korea, such as biomass co-firing and fuel cell deployment, small wind installations dropped (Orrell et al., 2021).

The discontinuous nature of incentives and national programmes makes it difficult for manufacturers to stay on the market, even in those countries where SWT technology is more present, as in the UK, Italy, and the United States. Six small wind manufacturers in the United States reported international exports in 2015, with just three doing so in 2020 (Orrell et al., 2021). Similarly, sales in China and exports from China have fluctuated with the number of Chinese small wind manufacturers in that market. In 2017, only 15 Chinese small wind turbine manufacturers reported sales, a decrease from 28 in 2014 (Duo, 2017), corresponding to a 60% drop in sales from 2014 to 2017 (Orrell et al., 2021).

From a global perspective, at the time of writing this paper, the largest market for small wind still came from Europe, United States, and China. SWTs are most commonly used for off-grid applications, such as telecommunication towers and farming. They are also used to power individual homes and small businesses, which can be tied to the grid. In 2019, 94% of SWT sales went to off-grid applications (Global Info Research, 2021). Unfortunately, 2020 saw only about 30 MW worth of units being sold around the world (Orrell et al., 2021), with a global market in terms of revenues (Figure 3) still on a flat trend. Regarding

¹ Conversion rates used in the paper at the time of writing: 1¥ = 0.008€; 1€ = 1.15\$ (USD).

152 future perspectives (Global Info Research, 2021), no clear agreement on future perspectives was found at the time of writing,
153 mainly as a consequence of the financial crisis connected to the global COVID-19 pandemic in 2020. Global Info Research
154 (Global Info Research, 2021) predicted the SWT global market would reach 190 million USD (165 million EUR) in 2025 with
155 a compound annual growth rate of 11.45% from 2020 to 2025. The market could thus become promising again, especially in
156 connection with the increasing attention on the transition toward cleaner energy systems. Regarding the future share by region,
157 Europe, Asia-Pacific, and the United States are expected to remain the key players in this sector. In particular, the Asia-Pacific
158 market will lead the total worldwide SWT sales, while the European market will show a reduction in the global relative share
159 (Figure 4). In Asia, Japan is expected to deploy renewable energy generation at large scales following the Fukushima Daiichi
160 nuclear disaster, whereas other countries such as Malaysia—which represents an untapped market with suitable conditions for
161 SWTs (Wen et al., 2019)—might also see significant deployment.
162



163 **Figure 3 - Global SWT market status in terms of revenues (Global Info Research, 2021).**
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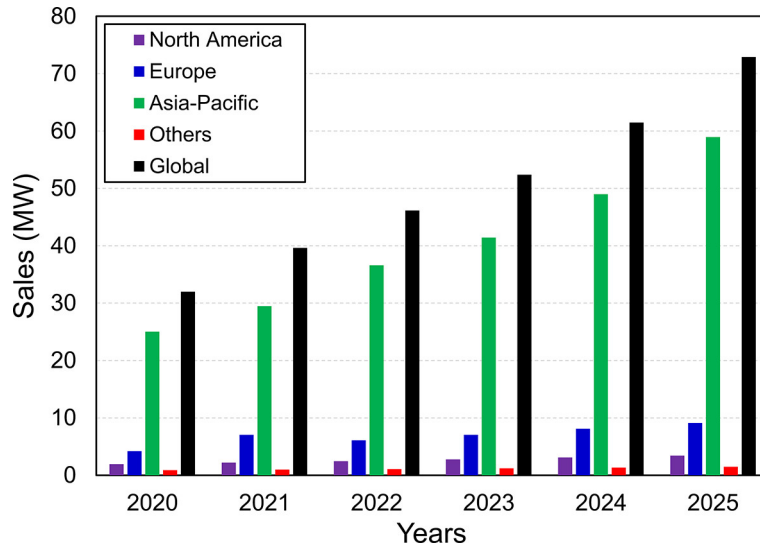


Figure 4 – Global SWT sales forecast by region (2020–2025). Data from (Global Info Research, 2021).

3 Economic aspects

As described in Section 2, the diffusion of SWTs has often gone hand-in-hand with dedicated financial incentive programmes from individual countries. This is unfortunately because the high LCOE of SWTs has represented the main obstacle hampering wider deployment of SWT technology (Predescu, 2016).

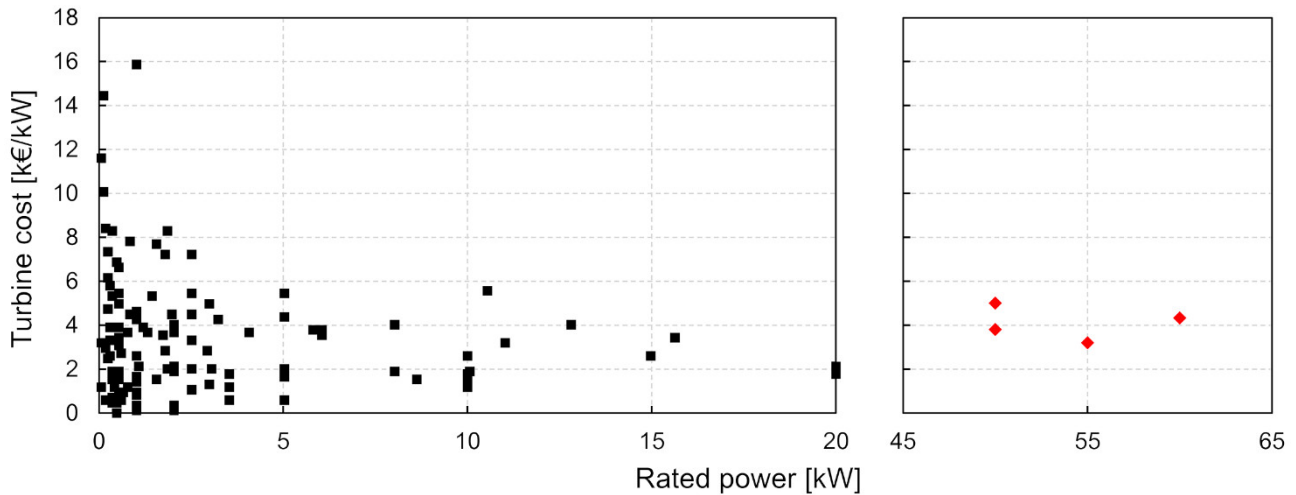
The economic evaluation of small wind systems is particularly critical for three main reasons: (1) the capital investment is strongly dependent on the specific turbine and country, (2) the correct selection of the installation site has a much higher impact on actual annual energy production (AEP) than in the case of turbines with large rotors, and (3) as discussed, the real viability of a project may depend completely on the incentives ensured by the specific country.

To give the reader an overview on the aforementioned issues, the main cost factors are analysed in the following subsections to facilitate the comparison of costs by country or region for the same technologies and to enable the identification of the key drivers in any cost differences. The four key indicators are: total installation cost, operation and maintenance cost, capacity factors, and LCOE.

3.1 Total installation cost

The total investment for installation can be expressed as the sum of the purchase cost and installation cost. The purchase cost for an SWT is notably variable not only as a function of the turbine size but also over time, depending on the attention given to the technology. (Kaldellis and Zafirakis, 2012) present a survey on 142 SWT models up to 20 kW, showing—as expected—a turbine cost reduction as a function of the rated power (black square markers in Figure 5). Recent data from the authors’ direct experience are also added as red diamonds in Figure 5 for the SWTs with rated power outputs around 50 kW. As seen

186 in the figure, the decreasing cost trend for lower rated power values is somehow stopped for rated power outputs around 50
 187 kW. This can be explained considering that, from this size up, turbines become more complex, requiring specific features (e.g.,
 188 the yawing system) and a manufacturing quality higher than that of smaller turbines. Finally, (Bortolini et al., 2014) provide a
 189 more up-to-date market survey considering several producers located worldwide and confirm that purchasing costs are not so
 190 highly correlated to the plant sizes because of aspects related to the specific producer, e.g., producer country, producer cost
 191 structure, and market policies. Having direct information on how the global, or total installed, cost comes together is very rare.
 192 In this study, thanks to support from Eunice Energy Group, a cost breakdown is presented in Table 2 for the 60-kW machine
 193 EW16 Thesis (Eunice Energy Group, 2021).
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195
 196 **Figure 5 - Turbine purchase cost survey for rated power lower than 20 kW (Kaldellis and Zafirakis, 2012) and around 50 kW**
 197 **(authors' experience).**

198
 199 **Table 2 – Capital cost breakdown of a 60-kW turbine (courtesy of Eunice Energy Group).**

	Cost	% of the total
Tower	≈7 k€/ton (≈7 k\$/ton)	18%
Generator	≈13 k€/ton (≈15 k\$/ton) (permanent magnets)	21%
Gearbox (1:20)	8-10,000 € (9-11,500 \$)	5%
AC-DC-AC converter	0.23 €/W (0.265 \$/W)	7%
Blades	20 €/kg (23 \$/kg)	4%
Rest of machinery	12 €/kg (14 \$/kg)	5%
Rest of materials	13-15 €/kg (15-17 \$/kg)	15%
Labour cost and standard industrial profit	-	25%

200

(Wood, 2011) reported a similar breakdown for a smaller machine (10 kW), showing how—in that case—the relative cost for blades becomes more relevant (7%), while that of the generator becomes less significant (6%) due to the lower power output.

The installation cost is probably the most critical parameter to evaluate and includes seven primary factors:

- 1) Raw material cost, i.e., expenditures to purchase the materials required for the turbine installation as well as to lay the foundation. All these elements are correlated to the wind turbine’s weight and height and to the rotor diameter
- 2) Earthworks’ cost, i.e., foundations, grounding, etc. to enable SWT’s operation. This is more crucial for countries with higher seismic activity that require more expensive foundations and is dependent on the type of soil
- 3) Installation labour cost, i.e., workers’ salary, crane rental, stand-by times on windy days
- 4) Engineering cost, i.e., expenditures for the preliminary and executive drawings, feasibility study and engineering, and site assessment and wind resource assessment activities to estimate expected AEP; documentation of all deliverables
- 5) Land purchase cost, i.e., cost for the required ground surface. Considering the tower height, a surface area of the same swept radius is assumed to be necessary. Additional cost for access roads, where not present, may be necessary
- 6) Grid connection cost, i.e., cables, power unit, and control system, including licence fees
- 7) Transportation costs, i.e., the expenditures necessary to get the turbine to the installation site. Transportation costs can include two different types of trips. In the case of imported turbines, both transportation by sea (e.g., to reach the EU mainland) and by land (i.e., to reach the final site) are needed.

The relative impact of these factors has been quantified by (Bortolini et al., 2014) and reported in Table 3.

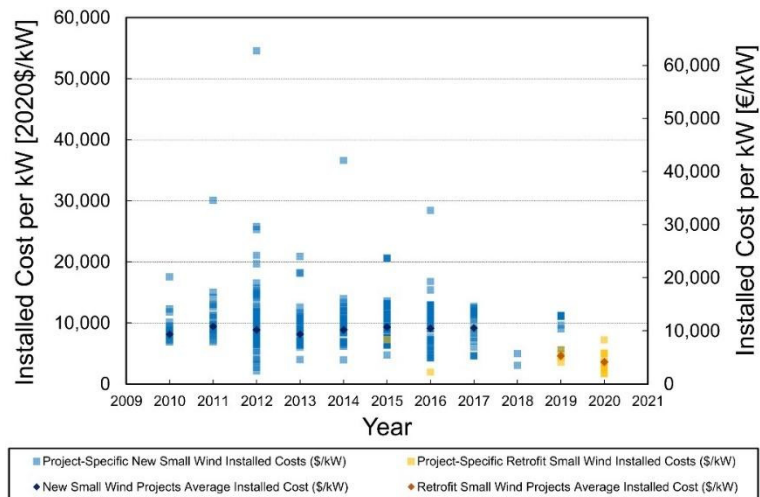
Table 3 – Impact of different cost factors on an SWT project.

Cost Factor	Impact [% of Global Cost]
Purchase	76%
Building material	7%
Labor	2%
Engineering	1%
Land purchase	10%
Grid connection	2%
Transportation	2%

The Engineering cost in Table 3 includes the wind resource and site assessment activities conducted to estimate a SWT’s expected AEP. The low percentage of total cost for this cost factor is in line with similar research that found many small wind installers do only minimal wind resource and site assessments (Orrell and Poehlman, 2017). This is partly because of the challenges involved in achieving a low-cost and accurate wind resource assessment. First, there are not many tools available and appropriate for small wind assessments. Next, for those installers who do attempt assessments, the tools regularly do not provide accurate AEP estimates because they mischaracterize the wind resource and perform poorly in areas of complex terrain

227 well (Sheridan et al., 2022). Based on the experience of some of the authors, the cost for a resource assessment for a SWT
 228 project may be in the order of 15 k€ (17.2 k\$), although this price is strongly variable from case to case, especially as a function
 229 of the site topography. In addition, one should also remember that the complexity of the terrain also affects accessibility to the
 230 grid, roads, price of the land, foundations and the excavation works needed, thus also impacting the other items of the table.
 231 Referring again to the 60 kW EW16 Thetis machine by Eunice Energy Group, even though real costs are strictly project-
 232 dependent, the foundation cost can be broken down into approximately 3,000 € (3,450 \$) for the excavation (23%), 8,000 €
 233 (9,200 \$) for the concrete (61%), and 2,000 € (2,300 \$) for civil works (16%). The transportation cost is approximately 5,000
 234 €/day (5,750 \$/day) (up to two trucks, and up to 600 km), while the crane costs for a 50 t, 40 m crane are about 6,000 €
 235 (7,200 \$).

236 An overview of the overall average annual and project-specific small-wind installed cost (in 2020 USD) in the United States
 237 for 2010 through 2020 is presented in Figure 6 (data from Orrell et al., 2021). Only new and retrofit projects with reported
 238 installed costs that use turbines with known rated capacities are included. Annual average capacity-weighted installed costs
 239 for new U.S. small wind projects range from around 3,480 €/kW (4,000 \$/kW) to nearly 9,565 €/kW (11,000 \$/kW). The small
 240 sample sizes and high variance in project-specific costs both contribute to this wide cost range. With the exception of 2018,
 241 the overall annual average capacity-weighted installed cost for this U.S. dataset has remained relatively flat at approximately
 242 9260 €/kW (9,500 \$/kW) (Orrell et al., 2021). This cost trend is in contrast with residential solar PV costs, which have been
 243 steadily dropping over several years (Barbose and Darghouth, 2015).



244 **Figure 6 - Installed cost per kW for new installed or retrofit installed projects in the United States (Orrell et al. 2021).**

246

247 **3.2 Operations and maintenance cost**

248 Operations and maintenance (O&M) are conventionally clustered into a single cost term, but operation costs differ from
249 maintenance costs, and not all distributed wind projects experience them equally. Operation costs for wind projects may include
250 land lease payments, remote monitoring, various operations contracts, insurance, and property taxes. Operations are a
251 significant expense for wind farms and large distributed wind projects; however, they typically are not substantial, or even
252 present, for small, distributed wind projects. On the other hand, all wind projects, distributed or otherwise, require a significant
253 maintenance cost (Orrell et al., 2021). For small wind systems, and especially in the case of complex areas, experience shows
254 that usually an investor does not opt for installation sites with more than two SWTs in the same field/owner. This consequently
255 decreases the available room for the economy scaling on the O&M costs.

256 In most cases, the project installer or developer performs the maintenance for the system owner. Maintenance costs include
257 labour, travel to the site, consumables, and any other related costs. Therefore, small wind maintenance costs can depend on
258 the maintenance provider's proximity to the project site (i.e., travel costs), the availability of spare parts, and the complexity
259 of maintenance and repairs. Maintenance costs can be categorized as scheduled or unscheduled. Scheduled maintenance
260 activities can include inspecting the turbine, controller, and/or tower; adjusting blades; checking production meter and
261 communications components; and providing an overall annual scheduled maintenance visit per the manufacturer's manual.
262 Unscheduled maintenance activities can include a wide variety of activities, ranging from responding to a customer's complaint
263 of noise from the turbine to replacing the generator, electrical components, inverter, blades, or anemometer. Scheduled
264 maintenance site visit costs for a sample of small wind projects were collected for the Benchmarking U.S. Small Wind Costs
265 report (Orrell and Poehlman, 2017). Scheduled maintenance is typically performed annually. That data showed the average
266 scheduled maintenance cost per visit is about 32 €/kW (37 \$/kW); the same value was confirmed by some European companies
267 (Eunice Energy Group, pers. comm.). In general, upon combining different reference sources, it is reasonable to consider O&M
268 cost for small wind projects in the range of 1–3% of the initial investment (Tzen, 2020).

269 **3.3 Capacity factors**

270 The economic viability of SWTs depends in a complex way on several factors, including the life-cycle energy production and
271 the possible presence of incentives. To address the first issue, i.e., to correctly evaluate actual production, a key metric is the
272 capacity factor.

273 Bocard observed mean values below 21% in 2009 (Bocard, 2009), while more recent works observed values between 37%
274 and 40% (Anon, 2015). Figure 7 presents calculated capacity factors for SWTs installed in the United States, based on the
275 average of the first three years of reported generation for each project from the New York State Energy Research and
276 Development Authority and U.S. Department of Agriculture Rural Energy for America Program datasets and the turbine rated
277 capacity (Orrell et al., 2020).

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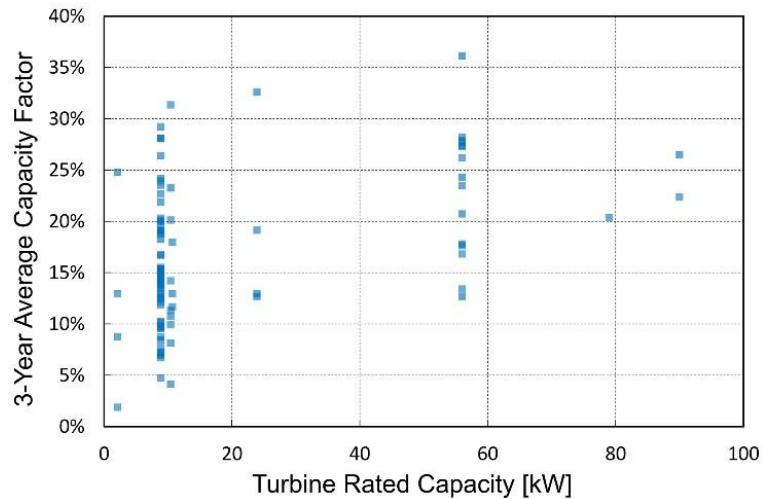


Figure 7 – Three-year average capacity factor for several U.S. wind projects. Data from (Orrell et al., 2020).

The three-year average capacity factor for small wind is 17%, but the dataset includes a range from as small as 2% to as high as 36%. This large variability reflects, more than other variables, the challenges to SWT siting and site suitability. For example, the capacity factors for the 8.9 kW rated capacity turbines range from 5% to 29%. This means that the same turbine model sited in different locations can achieve very different capacity factors. Overall, the wind resource quality has the largest impact on capacity factors, even though technology improvements have raised turbine power outputs significantly. Therefore, the wide variation of capacity factors across markets is predominantly due to differing wind resource qualities and, to a lesser extent, the different site configurations and technologies used.

3.4 Levelized cost of energy

Scattered data regarding the LCOE of SWTs can be found in literature and relevant reports. One of the most complete databases is provided by (Orrell et al., 2020), who collected the data reported in Figure 8 (prices are in cents of USD/EUR) for the U.S. market.

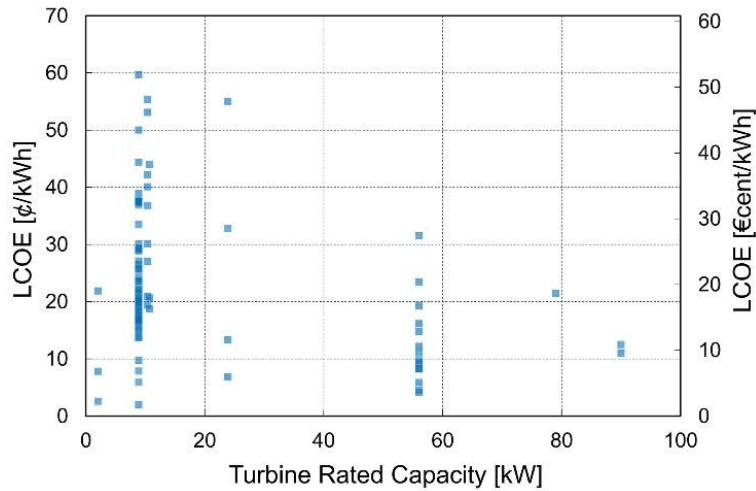


Figure 8 – Measured LCOE for SWT projects in the U.S. Data from (Orrell et al., 2020).

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297 The small-wind average LCOE after incentives was 0.2 €/kWh (23 ¢/kWh) (from 86 U.S. projects totalling 2 MW in rated
 298 capacity). To put these numbers in perspective, the LCOE of SWTs may be compared to the average residential retail electric
 299 rates ranging from approximately 7 to 17 ¢cent/kWh (8 to 20 ¢/kWh) in the continental United States (Orrell et al. 2019) and
 300 to the LCOE of residential PV, which is below 8.7 ¢cent/kWh (10 ¢/kWh) (Fu et al., 2018). Recent experiences in Europe for
 301 turbines in the range of 50 to 60 kW showed potential for a significantly lower LCOE on the order of 0.12 €/kWh (0.14 ¢/kWh)
 302 (Eunice Energy Group, pers. comm.). The relationship between calculated LCOEs after incentives and capacity factors is
 303 shown in Figure 9. As expected, the higher the capacity factor, the lower the LCOE in general. Higher capacity factors, which
 304 in turn can reduce LCOEs, can be achieved by better siting, which can help increase energy production and better turbine
 305 operations (i.e., higher turbine availability).

306

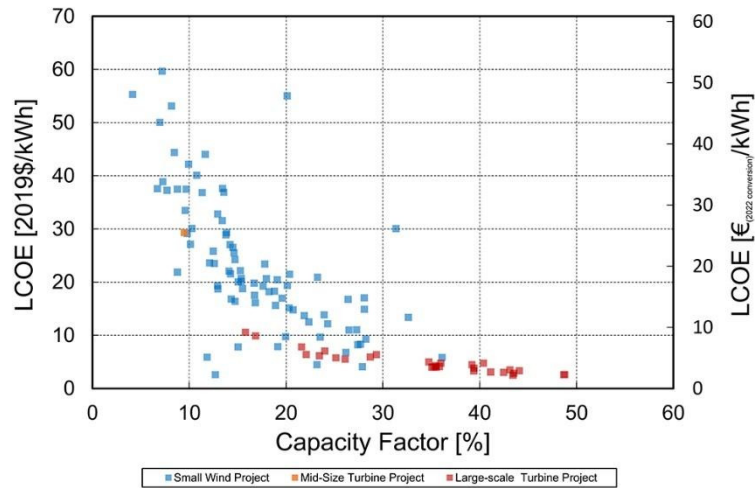


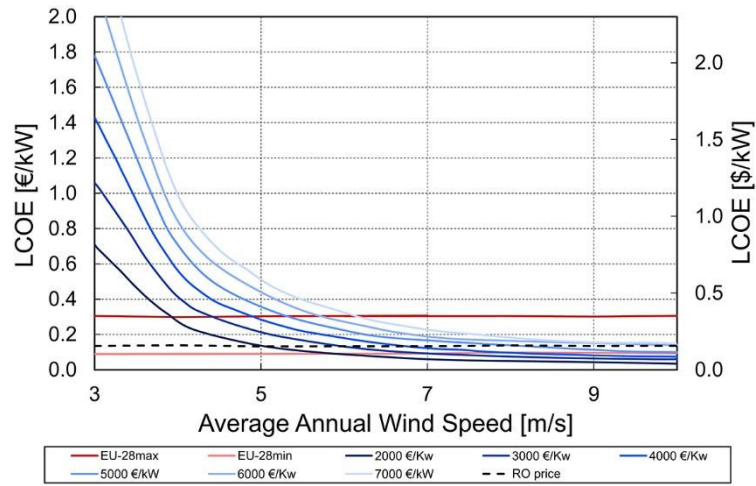
Figure 9 – Relationship between LCOE and capacity factor for SWT projects. Data from (Orrell et al., 2020).

Regarding the European Union, to the best of the authors' knowledge, there is no systematic study of the LCOE of SWTs, but there are a number of studies that point to higher LCOEs than those reported for the United States. For a site with a mean annual wind speed of 4.77 m/s, (Bukala et al., 2016) estimate a yearly energy production of 7,551 kWh for an SWT with a rated power of 5 kW, neglecting downtime. They estimate the investment cost of such a wind turbine at 36,500 € (42,000 \$), which is lower than that in the data reported for the United States. For a discount factor of 4% and assuming a yearly operation and maintenance cost of 2% of the investment cost, an LCOE of 45 €cent/kWh (52 ¢/kWh) is produced without incentives.

For an SWT with a rated power of 3.5 kW installed at an agricultural site in Belgium with a mean wind speed of 4.13 m/s, (Tordeur, 2018) reports an LCOE of 36 €cent/kWh (41.5 ¢/kWh) without incentives. This, coupled with all the incentives from which an agricultural small-medium enterprise may benefit in Belgium at the time of the measurement campaign (2016) and accounting for a discount rate of 4%, gives a discounted payback time of 19 years. It is worth noting that the true cost of this project was a very low 4,300 €/kW (4950 \$/kW). The low cost is partly explained by the fact that the farmer acquired the tower separately at reduced cost and performed most of the installation himself. Even with such major cost-cutting, the SWT is not economically viable, indicating that a mean wind speed of 4.13 m/s is too low for a viable SWT project.

(Bryne, 2017) reports the metered energy output for a number of sites in Ireland. For a site with a mean wind speed of 6.1 m/s, the AEP of a 5.2 kW rated wind turbine is 14,947 kWh, and for a site with a mean wind speed of 4.7 m/s, the AEP of a 2.1 kW rated wind turbine is 3,816 kWh. Assuming again a discount rate of 4%, a yearly operation and maintenance cost of 2% of the investment cost results in LCOEs of 33 €cent/kWh (38 ¢/kWh) and 51 €cent/kWh (59 ¢/kWh) for the 5.2 kW and 2.1 kW turbines, respectively, if the average installed cost per kW from (Orrell et al. 2019) is used. LCOEs of 14 €cent/kWh (16 ¢/kWh) and 22 €cent/kWh (25 ¢/kWh) are produced, respectively, if the average installed cost per kW from (Tordeur, 2018) is used.

330 Figure 10 presents the results of a study of the LCOE trend versus annual average wind speed at different specific investment
 331 values, with the household energy purchasing prices in EU also shown as references (Predescu, 2016).
 332



333
 334 **Figure 10 - LCOE trends versus annual average wind speed at different specific investment values in EU. Data from (Predescu,**
 335 **2016).**

336
 337 Financial viability for small-wind investment occurs in the region where the LCOE curve, computed for a specific investment
 338 value, is lower than the household energy price at the implementation location. The break-even point for a specific investment
 339 value is at the intersection of the respective LCOE curve with the line representing the household energy price. Beyond this
 340 point toward higher wind speeds, the savings obtained when using small wind technology brings long-term tax-free profit and
 341 savings to the investor. In countries where the household energy price is lower, financial viability can be reached at smaller
 342 specific investment costs and higher annual average wind speeds, which limits the geographical area where grid-connected
 343 small wind systems can be efficient. This analysis shows that in most situations, SWTs cannot compete with residential PV in
 344 terms of economic viability (European Court of Auditors, 2018). Even at sites with high wind speeds, the cost reduction
 345 required to achieve viability is still substantial. Taking the best case from (Bryne, 2017) as a close-to-optimal performance
 346 example with a capacity factor of 33%, the investment cost would need to be less than 6,000 €/kW (6,900 \$/kW) for the LCOE
 347 to fall below the 20 €cent/kWh (23 ¢/kWh), which is typical for residential retail electric rates in many European countries.
 348 This illustrates the main conclusion from the above analysis: SWTs may be viable, but only at very windy sites and with a
 349 serious additional effort to reduce the investment cost.

350 **4 Status of the technology**

351 While Sections 1–3 reported the status of the technology in terms of diffusion and costs, this section shifts the focus to the
352 specific features of SWTs, which are the core of small wind systems. The philosophy with which this study has been prepared
353 is highlighting those features that make SWTs different from utility-scale machines. This is important for introducing the
354 resulting challenges that must be tackled to further progress SWT technology.

355 **4.1 Typical features of small wind turbines compared to utility-scale turbines**

356 Utility-scale wind turbines are usually located in clusters and in areas with high wind resources, from a few turbines to large
357 wind plants located far (e.g., offshore) from the consumer. Although some utility-scale wind turbines may provide energy to
358 the owner, they are typically owned by or provide power to a utility company. In contrast, SWTs are typically owned by the
359 individual or organization that will use the power, such as a home or business, and are installed close to those loads. Because
360 the siting driver for SWTs is proximity to loads and not the optimal wind resource, the winds at these locations often have low
361 average speeds, are highly turbulent, and are more likely to have obstacles nearby, which can create flow structures of a scale
362 commensurable to that of the turbine. On the one hand, this usually leads to lower peak power coefficients, ranging
363 approximately from 0.25 to 0.40 (Wood, 2011), compared to values higher than 0.5 for utility-scale machines (Veers et al.,
364 2019). However, full transparency regarding the real efficiency of SWTs is often missing. For example, in a relatively recent
365 study, it was shown that 15 out of 43 manufacturers claim a power coefficient above the theoretical maximum or Betz–
366 Joukowsky limit (Simic et al., 2013). Notwithstanding this, it is undisputable that the peculiar environment these rotors work
367 in implies that SWTs must be specifically designed to work effectively in both low and turbulent wind resource conditions.
368 The implications of these peculiar working conditions are many and involve all aspects of turbine design and operation, as
369 summarized below.

371 **Aerodynamics**

372 The combination of dimensions much smaller than those of utility-scale machines with turbulent winds may present significant
373 problems for the aerodynamics of SWTs. First, the resulting low Reynolds numbers (Re) may cause a laminar separation
374 bubble, which is associated with a local maximum of the drag coefficient in the polar and a reduced lift-to-drag ratio (L/D)
375 (Selig, 2003). The presence of transition and the relative impact of inflow turbulence on it is key for airfoil performance
376 (Abbott and Von Doenhoff, 2010). This has many implications for design, including the fact that airfoils for SWTs must be
377 selected from those that provide good performance at low Re numbers, which favours airfoils with lower thicknesses that are,
378 however, more sensitive to stall. A compromise in this regard must be pursued. The presence of transition makes the L/D
379 dependent on Re and thus is particularly challenging for blade designers. Because the angle needed for maximum L/D is also
380 Re dependent, a constant pitch turbine would not operate at maximum efficiency at a constant tip-speed ratio, making the
381 control strategy in below-rated conditions more complicated (see the following subsection).

382 The aforementioned issues are particularly challenging in terms of proper simulation. Panel methods usually employed by
383 companies to define polars likely fail to correctly model these phenomena in many instances, especially in the near- and post-
384 stall regions. However, accurately modelling these phenomena is crucial for SWTs, particularly stall-controlled ones (Papi et
385 al., 2021). High-fidelity models used in academia are often not affordable for SWT companies, and airfoil selection is therefore
386 often based on published performance data. Examples of airfoils with good performance characteristics at low (around $5 \cdot 10^5$)
387 Reynolds numbers can be found in (Gigue`re and Selig, 1998; Timmer and van Rooij, 2003). Even high-fidelity turbulence
388 models, however, often do not predict lift and drag accurately in the presence of transition, let alone laminar separation, and
389 the designer should rely on lift and drag data measured in reliable wind tunnel tests (Van Treuren, 2015).

390 The problem of low Reynolds numbers is further exacerbated by the possible installation of SWTs at high altitude
391 (Pourrajabian et al., 2014), where the air density reduction can substantially reduce Re (up to more than 10%), bringing it to
392 those values where the effect of transition is more relevant. In this sense, it has been shown that the correction methods
393 proposed in the standards (wind or power correction) often fail in correctly representing reality.

394 The influence of blade roughness, due to insect accumulation in dry areas or leading edge erosion for example, also differs
395 between SWTs and large turbines. (Holst et al., 2016), for example, discuss the effects of roughness by comparing lift polars
396 of low-Re airfoils to high-Re utility-scale wind turbine airfoils. Experiments in that study revealed lift deficits of up to 50%
397 and confirmed the importance of a proper profile selection. In addition, simulations showed that roughness can reduce AEP
398 by up to 50%. Furthermore, roughness sensitivity could lead to premature separation, especially near the blade root that is
399 characterized by highly three-dimensional flow (Bangga et al., 2017). Thus, employing airfoils with good aerodynamic
400 characteristics for the specific blade span and expected operational regime is compelling.

401

402 **Control**

403 Large wind turbines have yaw-drive mechanisms to align the rotor to the mean wind direction. Such devices are much more
404 expensive for SWTs, especially for small rated-power values (10 kW or less): in these applications, some form of free or
405 passive yaw has been typically used. The most popular options are then a tail fin or the use of a downwind rotor, e.g., SD Wind
406 (SD Wind Energy, 2022), Skystream (XZERES Wind Turbines, 2022), Carter Wind (Carter Wind Energy, 2022), and others.
407 The downwind configuration solution is experiencing a revival for some specific applications in utility-scale machines,
408 especially for floating offshore applications (Bortolotti et al., 2021). For larger turbines, the same yaw-drive technology in use
409 for utility-scale machines is instead being increasingly applied.

410 Another control actuation commonly found in large wind turbines is the blade pitch system that can both regulate power and
411 slow down the rotor for overspeed protection by aerodynamically changing the blades' angle of attack. However, pitch control
412 is often not available at the scale of SWTs for economic reasons. Designing and manufacturing a fail-safe pitch system within
413 the physical constraint of a small hub and the capital cost constraints needed to keep an overall low LCOE are one of the
414 biggest challenges for the SWT industry. The need for a redundant brake mechanism, in fact, translates into either having
415 independent pitch actuation (as for the utility-scale machines) or an oversized mechanical brake that could bring the rotor to a

416 stop in the case of grid connection failure and associated runaway rotor. Both options have proven to be prohibitively expensive
417 in the DWT space thus far, and more economical solutions for avoiding overspeed that have been widely adopted include stall
418 regulation and/or rotating the rotor out of the wind direction via a furling mechanism. An attractive option for smaller SWTs
419 is “electromagnetic braking” by shorting the generator output (McMahon et al., 2015). This obviates the need for a mechanical
420 brake. Several current commercial SWTs such as the Bergey XL 15 (Bergey Wind Power, 2022) use this cost-reducing
421 strategy. Regarding active pitch, however, a recent study (Papi et al., 2021) highlights how the use of advanced pitch-to-feather
422 control strategies can significantly improve the performance of SWTs through more effective power regulation. It is speculated
423 that the aerodynamic power coefficient could be improved significantly to reach $C_p \approx 0.5$, which, together with simpler and
424 therefore more accurate aerodynamic modelling performance, could then justify the higher cost of pitch actuation in an
425 SWT. Also, another study (Papi et al., 2022) showed that a pitch control strategy can reduce peak loads in extreme conditions,
426 thus leading potentially to lighter and more cost-effective blade designs. Blade pitch can also help with start-up torque at low
427 wind speeds, whereas a fixed-pitch rotor must rely on its low wind speed and high angle-of-attack performance to overcome
428 the resistive torque of the drivetrain and generator. A quick starting characteristic is crucial for SWTs because they tend to
429 have more start and stop events compared to their larger counterparts due to higher turbulence levels and lower average wind
430 speeds.

431 Due to the aforementioned technical and economic issues, stall control is still largely used in SWTs. This latter strategy,
432 however, generates peak loads on the blades that are relatively much higher than those seen in utility-scale machines because
433 the pitch cannot be varied in parking conditions. In addition to the lower efficiency in terms of regulation across the functioning
434 range, the stall control strategy inherently introduces difficulties in predicting the aerodynamics of SWTs because three-
435 dimensional flow aspects and unsteady characteristics make the near- and post-stall regions of the polar curves difficult to
436 capture in aerodynamic models, especially in engineering methods (which can be economically used during the design phase).
437 These difficulties are further compounded in the case of passive-yaw configurations. Skewed inflow and dynamic wake physics
438 are still a topic of research in the wind energy community (Ning et al., 2015; Schepers et al., 2021) and in the case of SWTs,
439 given their more dynamic nature (e.g., higher yaw rates, rotational velocities, and passive yaw), introduce further nonlinearities
440 and unsteadiness in the rotor and tail induction fields, rotor aeroelasticity, and overall turbine response.

441 442 **Structural design and (scarce) aeroelasticity modelling**

443 In the field of large wind turbines, the use of aeroelastic simulation tools has been a consolidated practice for years (Bottasso
444 et al., 2006), as well as required for the certification of the machine itself. In the case of SWTs, the common approach up to a
445 few years ago was to build stiff blades characterized by high safety factors in the structural design in order to avoid significant
446 aeroelastic effects. As discussed, however, somewhat larger SWTs (from about 60 kW and up) are now practically equal in
447 complexity to large wind turbines (e.g., they usually have a variable-speed pitch-torque control system, an active yaw control
448 system and, because they often have a single actuation system for the blades, for safety they require mechanical brakes for the
449 emergency stop). In addition, they are often designed for medium-low wind speeds, so the blade is very large (for the 60 kW

450 blades, it is possible to reach 14–15 m). The experience of many authors of this paper, who had the opportunity in the last
451 decade to collaborate with the small or medium enterprises (SMEs) producing these rotors (IEA, 2014), shows that the use of
452 aeroelastic simulation tools is important to ensure a quality, safe, and economically sustainable project but is still very
453 uncommon. One of the few aeroelastic analyses of a 5 kW turbine is described by Evans et al. (2018b). The less frequent use
454 of aeroelastic models in industry is due mainly to a lack of experience of these companies, which very often come from other
455 industrial fields (e.g., producers of boats or heavy mechanical systems, etc.) where other design tools such as finite element
456 codes are primarily used. These companies are often not aware of the availability of good aeroelastic tools in the public domain
457 (e.g., OpenFAST from the National Renewable Energy Laboratory [NREL] (NREL, 2022)). Finally, another limitation to the
458 use of aeroelastic simulation tools for SWTs is connected to the lack of easy-to-handle post-processing tools. In fact, standards
459 require the designer to simulate the wind turbine in power production for different wind values and gusts, but also for a variety
460 of other operating conditions (starting phase, normal and emergency shutdown, transportation, faults, etc.). This results in a
461 few thousand simulations that must be analysed to extract maximum loading values for the various sub-components of the
462 wind turbine, including blades, tower, and drive train, but also pitch and yaw, air gap in the generator, supports, bearings,
463 brake discs, foundation, etc. In turn, these loads, together with fatigue loads and stress range cycles need to be delivered to the
464 different partner manufacturers. This process therefore requires automated tools and specific skills that are not always available
465 outside academia or large manufacturers.

466 **4.2 Innovative concepts and VAWTs**

467 Whereas conventional horizontal-axis wind turbines (HAWTs) have become the reference technology for all scales up to 15+
468 MW, alternative concepts are still being proposed for SWTs (Damota et al., 2015).

469 A popular modification to small HAWTs is to enclose the rotor with a diffuser to induce more air flow through the blades and
470 thereby increase the power output. This produces a diffuser-augmented wind turbine (DAWT), some examples of which are
471 shown in the first row of Figure 10. Adding a diffuser is indeed more attractive for small turbines than large ones, because the
472 additional structural and wind loads on the latter are likely to be excessive. A diffuser is a relatively simple modification to
473 basic turbine design, but it is still not clear how to optimize the diffuser and rotor to extract maximum power and whether the
474 extra power is worth the cost of the diffuser. An interesting review demonstrating the enduring fascination of the concept has
475 been recently reported by (Bontempo and Manna, 2020). There are other advantages of DAWTs: the diffuser may contain a
476 blade if it detaches from the rotor, and probably make the turbine quieter and less harmful to birds. These may well be
477 significant advantages for DAWTs in urban settings (Micallef and van Bussel, 2018). At least two companies have recently
478 commercialized small DAWTs, as showcased by (Evans et al., 2020) and (Visser, 2022). They have found a wide range of
479 applications from remote communication systems where the turbine partners a photovoltaic system, to more common stand-
480 alone systems.

481 Beyond other pioneering studies on novel energy-conversion systems such as DAWTs, most of the research on novel SWT
482 architectures has been directed to vertical-axis wind turbines (VAWTs) (Aslam Bhutta et al., 2012).

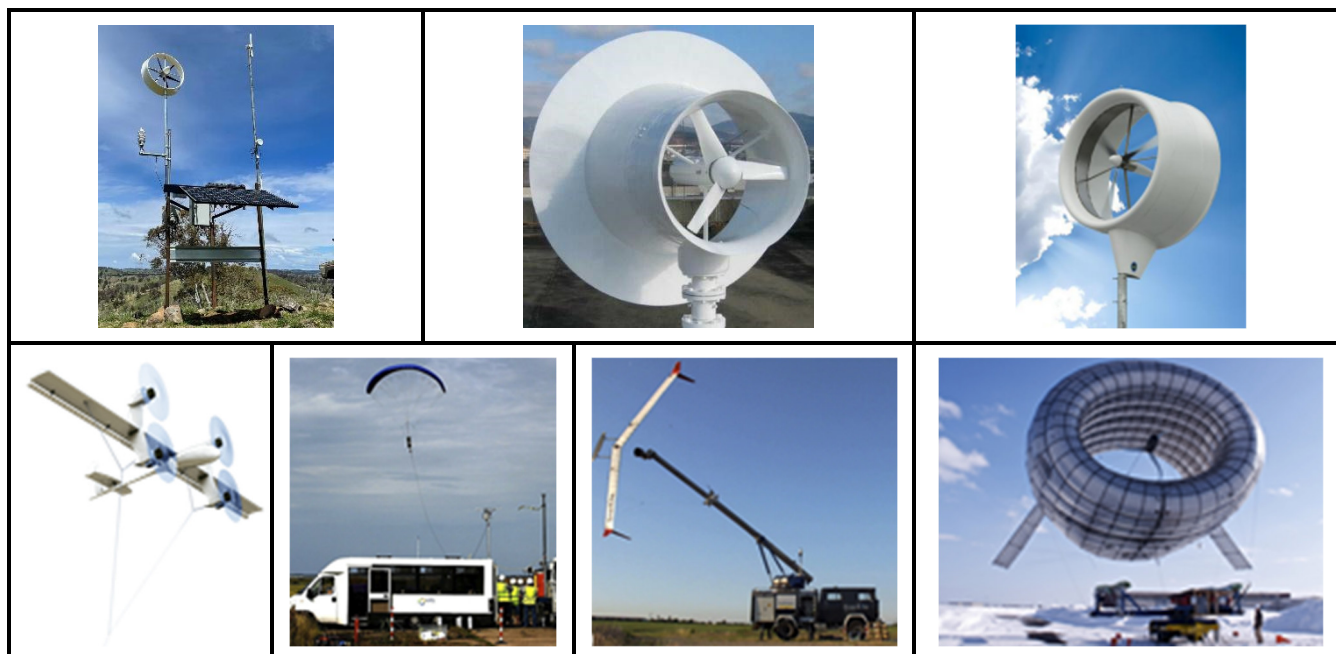
483 Among these, drag-type rotors like the Savonius turbine (Akwa et al., 2012) are relegated to very small applications due to
484 their low power coefficients and high mass-to-power ratio. Nevertheless, thanks to their simplicity, Savonius VAWTs are still
485 considered suitable in remote rural areas (e.g., the first electrification of developing countries) (Senthilvel et al., 2020).
486 On the other hand, despite a long absence from research agendas after the first generation of research culminated in the mid-
487 1990s, lift-driven VAWTs (or Darrieus concepts) are being increasingly studied (Bianchini et al., 2019). Despite popular
488 claims, the new understanding of the complex aerodynamics of Darrieus VAWTs achieved in the last decade has proven that
489 these machines can achieve power coefficients comparable to those of small HAWTs (Bianchini et al., 2015a). More
490 importantly, VAWTs present several advantages for small-scale applications, namely an intrinsic insensitivity to wind
491 direction, misaligned flows (Bianchini et al., 2012), or turbulence (Balduzzi et al., 2020), and lower acoustic noise generation
492 associated with generally lower tip speeds (Möllerström et al., 2016). The advantage of low blade speed, however, is offset by
493 the need to have a physically bigger, and therefore more expensive, generator and mechanical brake. In addition, VAWTs
494 allow for a variety of design solutions, which are considered aesthetically pleasant by the public and thus also suitable for
495 integration in buildings (Dayan, 2006) or with other infrastructure such as streets (Khan et al., 2017). Therefore, a variety of
496 small manufacturers entered the market either with downscaled VAWTs or with alternative concepts specifically intended for
497 use on rooftops (Mertens, 2003). Among others, one concept that is receiving increasing attention is the exploitation of the so-
498 called Magnus effect, which is a phenomenon associated with a solid object spinning in a fluid. This concept has been studied
499 for both HAWT, e.g., (Sedaghat, 2014), and VAWT designs (Shimizu, 2013). The potential advantage of these solutions lies
500 in the fact that they can operate in relatively low winds (Bychkov et al., 2007), thus covering a range of winds not typically
501 exploited by conventional wind turbines.

502 For very small VAWTs (< 3 kW), recent designs chose high-solidity rotors, i.e., rotors with larger chord-to-radius ratios,
503 mainly because of the need for sufficiently long chords to increase the aerodynamic forces and the Reynolds number. Based
504 on recent analyses, this aerodynamic solution seems to provide unprecedented specific power values for small rotors (Bianchini
505 et al., 2015a). On the other hand, these models showed the significant shortcomings of existing simulation models (Bianchini
506 et al., 2019), which were resolved largely by the new understanding of the role of flow curvature effects (Bianchini et al.,
507 2015b, 2016). Renewed research efforts are being undertaken to determine whether VAWTs can fit the scope of distributed
508 energy production in complex installation areas, as testified to by the recent EU project (Aeolus4Future, 2022). Parallel to
509 these research trends, VAWTs are being investigated for deep-water offshore applications with floating substructures (Paulsen
510 et al., 2013). The more favourable structural loads of the VAWT architecture and the possibility of placing the generator on
511 the floating platform—and thus lowering the system’s centre of mass—may lead to smaller floating supporting structures,
512 better control, reduced logistics and capital cost, and ultimately a lower LCOE (Arredondo-Galeana and Brennan, 2021). In
513 the realm of offshore SWTs, floating VAWTs could be deployed in some niche applications like integration with beacons at
514 the entrance of a port. A recent book, for example, explores the relationships between small wind and hydrokinetic turbines
515 (Clausen et al., 2021). Overall, despite the benefits that could be provided by VAWTs in some applications, they still lack both
516 theoretical understanding and technical maturity compared to HAWTs. Whereas the theoretical gap could be overcome by

517 modern investigation techniques, gaining the same level of industrial maturity as HAWTs seems out of reach at this time. The
518 potential impact of funded research projects at a national or a broader level could be relevant in proving the real prospects of
519 the technology and driving their development.

520 Other touted devices that, at least on paper, have demonstrated the potential for low LCOEs are airborne wind energy (AWE)
521 kites (Figure 11). They propose to extract wind power either through cross-wind by using lift and therefore flying faster than
522 the wind speed and carrying turbine generators onboard (fly-gen) or by pulling and unwinding a tether connected to a generator
523 on the ground (ground-gen). Other concepts expect to take advantage of very high-altitude winds via buoyant aerostat ducts.
524 None of these concepts has thus far demonstrated an economically viable power curve or has shown successful size scalability
525 in real-world settings. Yet, there is significant momentum in AWE research, with some pioneering industrial products already
526 in the market, and the applicability of these devices will likely be in the distributed wind space. While it is difficult to assess
527 the real costs and LCOE of AWE kites due to their nascent stage, the key advantage they provide is the absence of hefty and
528 expensive support structures while maintaining a generous rotor swept area. This would have favourable effects on the balance
529 of station costs that have plagued the DWT industry to date; this is the main reason why they are here mentioned as potential
530 actors of the small and, more likely, distributed wind market of the future. The challenges these devices face are numerous,
531 however, from flight safety and reliability to the efficiency of power generation and from the issuing of design and certification
532 standards to their acceptance by public and aviation authorities, and only future deployments will indicate whether they can
533 compete in the DWT market.

534



535 **Figure 11 - Currently proposed DAWT (upper row) and AWE kite archetypes (lower row). First row - from left to right: The Diffuse**
536 **Energy Hyland 920 diffuser-augmented turbine as part of a remote power system for a communication tower. The 200 W turbine**

537 has a maximum diameter of 0.92 m. Photo supplied by Dr Joss Kesby; HAWT with flanged diffuser (Ohya et al., 2008); DonQi
538 urban windmill (photo credit: DonQui Global) | Second row - from left to right cross-wind or fly-Gen (a.k.a. drag-power) devices
539 (image credit: Windlift); ground-gen (a.k.a. lift power) flexible kite (photo credit: KPS); ground-gen rigid kite (photo credit: Ampyx
540 Power); aerostat ducted wind turbine (photo credit: Altaeros).

541 4.3 Turbine archetypes and design standards

542 Unlike the typical utility-scale three-bladed, upwind machines, SWTs have not coalesced into a dominant archetype, with
543 many different layouts still being offered in the market. The variety of archetypes (upwind vs. downwind, HAWTs vs. VAWTs,
544 two vs. three or more blades, active pitch vs. stall controlled, etc.; see Figures 12 and 13) creates a challenge for the design
545 standardization and certification of SWTs (Damiani et al., 2022). This challenge is made stronger by the intention of standards
546 to facilitate the development of SWTs at relatively low cost; the “simplified loads methodology” (SLM) in IEC 61400-2 for
547 small horizontal-axis turbines is the main example.

548



549 **Figure 12 - Common HAWT archetypes found in the current DWT market. From left to right: Upwind, active pitch and yaw (photo**
550 **credit: Tozzi Nord); upwind, stall-controlled and active yaw (photo credit: Eunice); upwind, stall-controlled and tailed passive yaw**
551 **(photo credit: NREL pix 49511); downwind, stall-controlled, passive yaw (photo credit: Eocycle – formerly XANT); upwind, tailed**
552 **passive yaw, furling (photo credit: Bornay); downwind, pitch or pitch-coning controlled, passive yaw (photo credit: SD Wind**
553 **[formerly Proven]); downwind, stall-controlled, passive yaw and teeter (photo credit: Ryse Energy [formerly Gaia]).**

554

555



556 **Figure 13 - Common VAWT archetypes found in the current DWT market. From left to right: Darrieus Troposkien (photo credit:**
 557 **Chava Wind); H-Darrieus (photo credit: Xflow Energy); H-Darrieus with helix shape (photo credit: PRAMAC); Savonius (photo**
 558 **credit: BE Wind); combined Savonius-Darrieus (photo credit: HiVAWT).**

559

560 The lack of dominant archetypes complicates the development of standards and design tools for SWT's, resulting in a reduced
 561 refinement and robustness for all the archetypes as their counterparts for utility-scale machines.

562 Type certification for large wind turbines, which primarily follows IEC 61400-1 (IEC: International Standard, 2019a), are
 563 typically performed by large companies with extensive design teams who can afford multidisciplinary development
 564 departments, highly refined turbine specific aeroelastic models, high-performance computing, and testing facilities. The much
 565 smaller companies that manufacture SWTs do not have access to such resources. For example, even though estimating the
 566 loads according to the design standards would require only a few hours of computational time with state-of-the-art engineering
 567 codes, these codes require resources and staff with very specific skills to be utilized correctly and correlation to archetype
 568 specific loads measurements is needed to demonstrate confidence in the results.

569 The IEC standard for wind turbine design also includes the IEC 61400-2, dedicated to SWTs (IEC: International Standard,
 570 2019b). It covers all mechanical and electrical subsystems and includes support structure and foundations as well as the grid
 571 connection (including power electronics where applicable). The section applies to wind turbines with a rotor swept area smaller
 572 or equal to 200 m² generating at a voltage below 1000 V AC or 1500 V DC and covers both grid-connected turbines and off-
 573 grid applications. IEC 61400-2 allows for a number of simplifications to the design and analysis of turbines, including the use
 574 of the SLM and a reduced number of design load cases (DLCs). However, the SLM currently captured in the standards more
 575 than double the Safety Factor for Ultimate Loads, which may make the SLM process easier to use for the design phase and
 576 helps keep costs low but will create a heavier and more expensive product, which results in turbines that may not be competitive
 577 in the distributed generation market. By their nature, use of the SLM normally leads to a safe but over-designed product. For
 578 example, for very small SWTs, the critical DLC includes the gyroscopic loads on the blade roots and main shaft under yaw,
 579 however, in general terms our knowledge of the yaw behaviour of SWTs is poor across the range of turbine configurations.
 580 The magnitude of the gyroscopic moment is given by a simplified load equation involving the blade moment of inertia, the

581 blade angular velocity, and the yaw rate. Although the equation captures in principle the actual physics responsible for the
582 gyroscopic moment (Wilson et al., 2008), the safety factor for this load is 3. The SLM stipulates the maximum yaw rate as a
583 function of rotor area, and then requires this be multiplied by the maximum blade angular velocity. The limited information
584 available on SWT yaw behaviour, e.g., (Wright and Wood, 2007) and (Bradney et al., 2019), suggests however that high blade
585 speed correlates with low yaw rate, but this is not used in the SLM.

586 As an alternative or if the turbine configuration is not covered by the SLM equations, then alternative simulation modelling or
587 load measurements can be used, which may result in a more optimised final design. Additionally, many aspects of the turbine
588 aeroelastic response that are missed by the SLM approach could, in principle, be captured by higher-fidelity aero-servo-elastic
589 modelling. However, using aeroelastic modes for the design and certification of SWTs is challenged by the fact that while
590 models are well-tuned for active yaw and active pitch HAWTs, they are less validated for stall-controlled, passive-yaw HAWTs
591 and progressively less so for non-traditional archetypes (e.g., teetering hubs, VAWTs, AWE kites) (Damiani et al., 2022).

592 Regardless of the initial design approach, the reliability of SWTs is guaranteed through duration testing, where at least 6
593 months of operation is required during which minimum operation at high winds is stipulated. The standard requires
594 comprehensive documentation of the testing. In addition to the whole turbine testing, specific component tests are prescribed.
595 Some SWTs come with design variations. To limit the demands on the original equipment manufacturers, a full design
596 evaluation is only required on a selected representative configuration. Other variations need only be evaluated or tested in the
597 ways in which they are different from the representative configuration. Guidance on the conformity assessment, however, is
598 rather limited in the design standards, and this has been lamented by the industry as an obstacle to the commercialization of
599 new fleet products or in the case where changes to the product line, such as the use of a new manufacturing process for an
600 individual component, may open the product to extensive work to maintain certification.

601 For power performance testing, IEC 61400-12-1 includes a normative Annex H specifically for the power performance testing
602 of small turbines. This reflects the fact that testing according to the general standard using 10-minute averages, where the
603 complete wind speed range must be covered by sufficient data to minimize statistical uncertainty, can be a time-consuming
604 and expensive process. To get around this difficulty, testing SWTs involves using 1-minute averaged data, thus considerably
605 reducing the time needed for testing, but also because 1-minute averaging extends the frequency distribution of wind speed,
606 making high-wind-speed data points more common.

607 The SWT test standard also covers battery charging. Procedures are prescribed that minimize the influence of the specific
608 battery configuration and condition (state of charge). SWTs that use inverters for grid connection are tested together with the
609 inverters, and the power measured is the power available to the consumer. Most SWTs lack a clear definition of rated power
610 and wind speed; instead, a reference power is defined as the averaged power in the 11 m/s bin.

611 Comparisons of 10-minute averaged power curves with those based on 1-minute averaged data have been presented in (Elliott
612 and Infield, 2014). Fortunately, the systematic distortion of power curves due to so-called errors in bins was found to be small.
613 However, if the 1-minute power curve is used together with a 10-minute averaged wind speed distribution, then an error of
614 1.15% in the estimated annual energy yield is shown in the study. To avoid this, the energy yield calculation should ideally be

615 based on 1-minute averaged wind speed data. Because the calculation of turbulence intensity depends strongly on the averaging
616 period, it would be better for this aspect of site characterization to be based on 10-minute data, even if the power curve itself
617 is based on 1-minute data as prescribed in the SWT test standard.

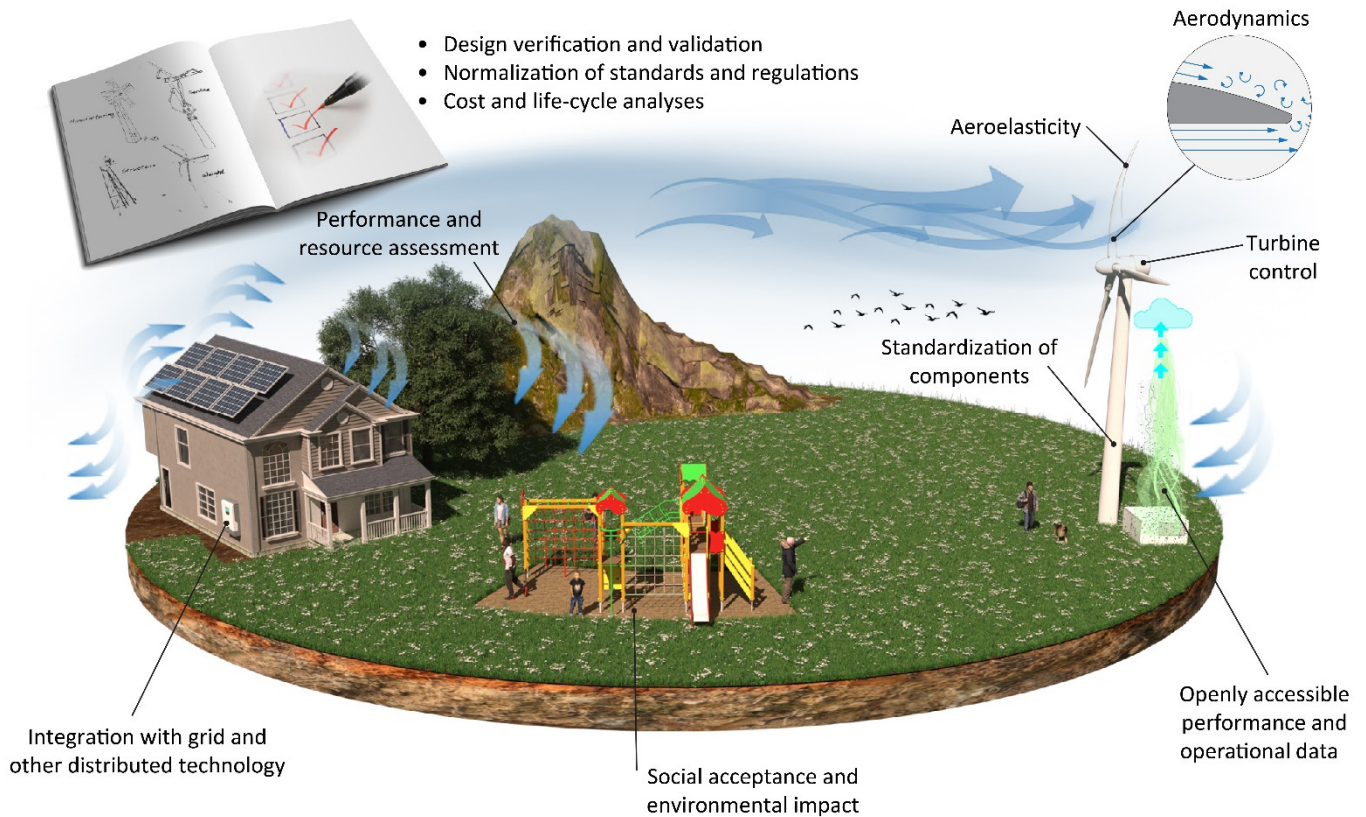
618 From this overview, it is clear that the SWT design standards can be substantially improved on multiple fronts, from the design
619 requirements to the testing, validation, and conformity assessment. The preparation of a new edition of IEC 61400-2 has just
620 started. It is anticipated that the SLM will be improved and there are likely to be further divisions of SWTs depending on size,
621 power rating, and archetype. Rotor swept area combined with rotor orientation, type of power-regulation, and type of yaw
622 control, for example, can lead to a matrix organization to determine requirements for design load calculations, structural
623 verification, and numerical model validation that would also depend on the experience of the numerical codes with the different
624 turbine archetypes (Damiani et al., 2022). A rigorous differentiation of certification requirements that depend on the turbine
625 configuration appears as the most urgent need in the design standards to arrive at a substantiated assessment of the load
626 categories for SWT. All these auspicious changes should make the standard significantly more useful to the manufacturers and
627 end-users of SWTs.

628 **5 Grand challenges for small wind turbine technology**

629 The transition to a more distributed production of energy, combined with the evolution of grids toward “smart” architectures
630 and control logics, which are more resilient, are leading to an evolution in the way electric services are being provided.
631 Distributed solar has already demonstrated wide-scale acceptance (IEA, 2019) in this more distributed energy system. While
632 SWTs have yet to reach general acceptance, they can play a similar and supporting role. To become more commercially
633 accepted, marked cost and performance improvements are needed. Although significant reductions can be achieved through
634 understood technology improvements, additional innovations are needed that lie beyond our current knowledge of critical
635 physics, with particular reference to turbulence, applicability of design assumptions, and the existing modelling and simulation
636 capabilities. Cost reductions that have been demonstrated within the distributed wind industry show that with adequate
637 investment, significant hardware cost reductions are possible (NREL, 2022). However, the generally low investment in small
638 wind technology research and a lack of consistent and substantial incentive programmes have relegated SWTs to niche
639 applications with minimal economies of scale. The success of solar PV, which has benefited from significantly more incentive
640 programmes than SWT in the distributed generation market, demonstrates the importance of stable incentive programmes of
641 this type in achieving market share.

642 Among other considerations, a recurring research gap noted in many studies is that SWTs often fail to achieve predicted or
643 published AEP. This is likely due to a host of considerations such as overly optimistic resource assessments, rotor
644 underperformance at low wind speeds and during high turbulence, or poor final turbine siting. The two flow features, rotor
645 underperformance in low winds and/or turbulent winds, are typical of installations on top of short towers and in proximity to
646 natural or artificial obstacles.

647 Based on the status of the technology described in the previous sections, the present study identifies five specific grand
 648 challenges (GCs) that must be overcome to spur SWT development and meet the globally expected demand for a wider variety
 649 of distributed energy resources. The grand challenges are visually presented in Figure 14, which represents the graphical
 650 abstract of this study. To address these challenges, a number of unknowns and gaps to be filled are identified (Section 5.1).
 651 Future enablers (Section 5.2) are also suggested as the keys to elevate SWTs to a more mature technology.
 652



653
 654 **Figure 14 – Visual synopsis on how the key enablers identified in this study may help tackling the five grand challenges for SWT**
 655 **technology.**
 656

657 **GRAND CHALLENGE 1 – Improve energy conversion of modern SWTs through better design and control, especially**
 658 **in the case of turbulent wind**

659 Because SWTs are typically installed in areas with lower (less energetic) and more turbulent wind resources, maximizing the
 660 amount of energy that can be harvested from the wind (i.e., maximizing the SWT’s capacity factor) while ensuring turbine
 661 longevity and survival through infrequent high-wind events is critical. Many wind turbines have been shown to underperform

662 in comparison to performance based on simulations. This is due to a combination of simulation tools that overpredict turbine
663 performance, driven largely by the simplification of flow features that these turbines are subject to and the actual complexity
664 of the oncoming flow. In particular, better insight into the impact of turbulence and gustiness on turbine performance is needed.
665 This can be achieved with a combination of more detailed testing data and more advanced design tools capable of modelling
666 the complex blade–flow interactions. Additionally, advancements focused to exploit oncoming winds more effectively,
667 including the use of taller towers or the design of lower specific power rotors to better exploit lower winds, must be continued.
668 To this end, it is now possible to undertake multidimensional blade design to minimize starting time, blade mass, and noise
669 while maintaining good power extraction and adequate blade strength, e.g., (Sessarego and Wood, 2015). Among other aspects,
670 blade mass is paramount because it correlates with manufacturing costs and blade inertia. In turn, the ability of a turbine to
671 start quickly to maximize power extraction at low wind speeds depends on the inertia, as do the gyroscopic loads discussed
672 above, giving this feature an importance that it does not have for large turbines. SWT blades are naturally stiff and benefit
673 from additional centrifugal stiffening at high angular speeds, so further optimization should be possible. Because the
674 gyroscopic loads are major fatigue (as well as ultimate) loads, an improved understanding of turbine yaw behaviour should
675 allow more optimized turbine design. This should be seen as the key challenge in the modelling of complex unsteady
676 aerodynamics in the presence of passively yawing rotors, either downwind of the tower or yawed by tail fins.

677 **GRAND CHALLENGE 2 – Improve prediction and reliability of long-term turbine performance despite limited**
678 **resource measurements**

679 Going beyond accurately optimizing and then predicting the power production of an SWT based on specific wind
680 characteristics, for SWT projects to receive financing, the industry must be able to accurately predict turbine power production
681 over the full life of the project. This accuracy of long-term performance prediction is needed to lower the risk associated with
682 SWTs as seen from the perspective of consumers, insurers, city planning professionals, project financiers, and regulators.

683 Long-term performance prediction is built on a number of factors, primarily the turbine performance characteristics combined
684 with accurate wind resource estimation and any changes due to local obstacles over the life of the project. Additionally, turbine
685 availability due to mechanical, electrical, and weather conditions at the specific site must be considered in addition to long-
686 term turbine reliability and performance degradation. Although not directly related to turbine design, the availability of spare
687 and replacement parts, approved turbine repair technicians, company warranty commitments, and specific turbine location
688 relative to all these factors will also drive long-term power generation.

689 Beyond corporate credibility of the installer and turbine manufacturer, long-term production reliability can be categorized in
690 two main areas, i.e., wind-driven resource performance and turbine reliability. Discussions with the SWT development
691 community have identified several key challenges to conducting low-cost but accurate resource assessments (Fields et al.,
692 2016). These include the availability of low-cost anemometer and remote sensing, the lack of high-quality mesoscale modelled
693 wind speed data at heights typical for SWT installation, and the availability of validated and easy-to-run obstacle modelling to

694 understand the potential impacts of local obstacles on the wind resource, especially in complex terrain (Duplyakin et al., 2021).
695 Once an accurate assessment of the resource at the site in question is available, typically for a model year, additional parameters
696 such as the conditional changes over time, growth of obstructions such as tree cover, and potential weather-driven availability
697 reduction will need to be added. Tools making resource recommendations must also be verified, providing confidence to
698 installers, consumers, and the financial community (Tinnesand and Sethuraman, 2019).
699 Many turbine manufacturers can point to turbines that have operated reliably for many years, but to be successful in today's
700 market, a long turbine life must be balanced with economic viability (see GC 3). The second element of this challenge is
701 developing methods that prove SWT technology will operate reliably over the turbine's design life. For example, the SLM of
702 IEC 61400-2 mandates a simple determination of the total number of fatigue cycles experienced by the blades of an SWT.
703 Because of the higher angular velocities of SWTs, the fatigue cycles for SWT blades are in the order of 100 times the number
704 for large turbine blades. Despite this, the standard does not mandate fatigue tests for small blades, and there is not strong
705 operational evidence that fatigue is a major issue for most SWT blades. On the other hand, the fatigue load case in the SLM
706 appears to be very conservative (Evans et al., 2021), which increases turbine costs and may not identify the likely locations
707 for fatigue driven failures in operating turbines. Addressing this challenge will centre on developing a better understanding of
708 the likely failure modes of SWTs, improved knowledge of the role of yaw behaviour in generating gyroscopic fatigue loads,
709 the development and use of validated design tools that address the likely failure modes, and standards and certification
710 processes to help ensure that turbines operate reliability over their design life. This improved understanding and improved
711 tools will also need to be validated for the wide array of SWT configurations, including free and damped yaw. For the future
712 SWT market to be successful, this effort will need to be accepted by large-scale financial organizations, which are driving
713 investment in distributed-scale power generations.

714 **GRAND CHALLENGE 3 – Improve the economic viability of small wind energy**

715 For an SWT to be economically successful, it must provide reliable power at a cost comparable to other similar technologies,
716 such as distributed solar PV, and be acceptable by the market. A reduction of the LCOE can be achieved by balancing better
717 capacity factors (see GC 1) and reducing unit installed cost. Reductions can come from design optimization, using new
718 materials and manufacturing techniques, developing standardized solutions for components that can be applied across multiple
719 turbine models, such as power inverters, and promoting or incentivizing production economies of scale. Moreover,
720 improvements in installation techniques, reducing the cost of foundations, and other related balance of station costs will be
721 needed.

722 Many strategies have been considered to lower the cost of turbine hardware, with some solid success in specific turbines. A
723 balance must however be made to optimize lower turbine costs, which is largely driven by reducing turbine materials and
724 ensuring successful operation over the turbine's designed life (see GC 2). This optimization must also be balanced with
725 international standards, which may drive up turbine system costs through the SLM. For example, tools used to predict the

726 impact of turbulence on component fatigue while load-reducing turbine control, such as adopting pitch regulation typical in
727 larger rotors, can also help ensure long-term turbine operation while optimizing turbine material needs. The expanded use of
728 validated aeroelastic design tools will also become more critical to help optimize this balance of reliability and low cost.
729 Recent increases in commodity prices as well as supply chain interruptions are causing increased costs for most SWT
730 manufacturers. Although some of these challenges could be overcome with expanded manufacturing, leading to larger
731 economies of scale and increased industry purchasing power, expanded research into material substitution for high-cost or
732 hard-to-access materials would help lower and stabilize turbine manufacturing costs. Expanded work in aligning component
733 supply across multiple SWT vendors may also help address some high costs and lower component availabilities, especially if
734 supply chain disruption becomes more common.
735 Overall, a lower LCOE will also help communities access SWT technology (see GC 5), allowing wind technology to play a
736 more active role in addressing issues of energy poverty and energy access while reducing the needs for financial incentives,
737 which typically favour wealthier consumers.

738 **GRAND CHALLENGE 4 – Facilitate the contribution of SWTs to energy demand and electrical system integration**

739 Having more distributed wind in the energy mix could contribute significantly to energy justice and power system
740 decarbonization. The ability of distributed wind to provide low-cost energy close to consumers with a higher energy density
741 and smaller footprint of other distributed technologies provides an important tool to achieving low carbon energy system goals.
742 Additionally, SWT lends itself to local development and deployment. Many developing countries, for example, are more likely
743 to have the capacity to build an indigenous SWT than the solar cells necessary for a PV system. If the fulfilment of GC 2 is
744 pivotal to make investment in SWTs attractive to many more customers, the introduction of many SWTs to the grid is non-
745 trivial. Although the expanded use of distributed energy resources will generally require improved energy control and likely
746 distribution system enhancements. The highly discontinuous power production of SWTs, which can be hampered by some
747 energy grids with restrictive ramp rates requirements or that are particularly susceptible to faults, requires additional thinking.
748 SWT technology must not only advance to meet the rapidly evolving grid code requirements for distributed generation (Preus
749 et al., 2021), but the value they may add to grid reliability and resilience should be highlighted and monetized. Standardization
750 through improved future revisions of IEC 61400-2 will bring the industry to a similar technical level for remote control and
751 safety in the smart grids of tomorrow. Due to their distributed nature, the ability of SWTs to assist load reduction or load
752 shifting in behind-the-meter applications, especially in markets that are expanding electrification in an effort to reduce carbon
753 production, must be fully assessed and articulated. The ability for SWTs to complement distributed solar PV technologies will
754 allow improved cost and operability to high renewable contribution systems for both behind- and in-front-of-the-meter
755 applications (Reiman et al., 2020), especially with expanded consumer electrification for heating and transportation. The role
756 of energy storage, and particularly of batteries, will be important not only for wind, but in general for enabling the transition
757 to a smart-user-based grid paradigm.

758 The increasing interconnection requirements of all distributed generation, including in many cases two-way communication
759 with grid control systems, require new SWTs to be more responsive, such as providing low-voltage ride through, more
760 advanced grid services, and potentially direct grid support. Additionally, with these expanded communication needs, additional
761 cybersecurity considerations will be required of future SWT technology.

762 The role of SWTs, however, should not be limited to grid-connected installations. Large global markets for isolated energy
763 systems, the provision of energy access, and off-grid energy services such as ice making, water pumping, irrigation, or direct
764 heat could further increase the market potential of the technology and again aid in global decarbonization by offsetting typically
765 fossil-based means of providing these services.

766 **GRAND CHALLENGE 5 – Foster engagement, social acceptance, and deployment for global distributed wind markets**

767 Engaging communities, societies, and regulatory authorities is key for SWT development. Actions need to be taken to enhance
768 the social understanding of SWTs and to provide evidence that modern turbines are expected to be significantly more efficient
769 than their predecessors. Turbines must also be designed and deployed while taking into account their installation in proximity
770 to people and within communities, with a clear understanding of their social and environmental impacts. Expanded research
771 on community-based impact, such as ice throw and safety setbacks, needs to be carried out, leading to improved standards and
772 guidelines for turbine installation. While some virtuous examples have been presented recently (e.g., the RELY COST Action
773 (Roth et al., 2018) (US DOE WindExchange, 2022) additional programs are seen as key enablers to increase awareness and
774 acceptance about the technology.

775 Political and regulatory actions, especially if coordinated among countries on a larger scale, must be enhanced to allow
776 deployment of the technology in a more effective way. Common regulatory and permitting requirements, based on science and
777 modern understandings of potential impacts, are needed to streamline development timelines and reduce costs. Incentives,
778 standards, and promotional policies should also be aligned. This is not only needed in the context of governments, but also
779 within multi-lateral nongovernmental organizations, development banks, and foundations. For example, the creation of equal
780 incentives across nations, including a clearly defined timeline for them to stay in place, is needed to encourage investment and
781 the creation of economies of scale that will be important to sustain each of the other grand challenges.

782 **5.1 Unknowns and knowledge gaps**

783 Associated with the grand challenges identified above, the following sections 5.1.1-5.1.6 identify specific areas that will need
784 ongoing global focus if SWT technology is going to be successfully developed to support long-term global needs for power
785 generation to meet local loads. In particular, these sections identify the main unknowns and knowledge gaps that need to be
786 addressed to allow the five grand challenges to be resolved.

787 **5.1.1 Higher LCOE due to a lack of an economy of scales, resulting in high balance of station cost**

788 As discussed, the total global installed cumulative small wind² capacity was estimated to be about 1.8 GW as of 2020 (Orrell
789 et al., 2021). In contrast, an estimated 19 GW of residential solar PV was installed worldwide in 2020 alone (IEA, 2020). The
790 difference in installed capacities is driven by a number of factors, including intrinsic siting requirements, availability of
791 incentives, market acceptance, and differences in costs. High deployment costs are driven by a number of factors. In particular,
792 a lack of economies of scale and high balance of station costs.

793 Currently, most manufacturing of SWTs is conducted in small plants using batch processes because of the relatively small
794 manufacturing volume and limited corporate cash flow. Small commercial volumes increase component costs, reduce
795 purchasing power, and in times of restricted supply chains, necessitate the ability to substitute components if traditional ones
796 are unavailable. Each of these items increase cost and complexity and reduce the reliability of SWT products. As has been
797 clearly demonstrated within the solar industry, large efficiencies and cost reductions can be gained across the SWT industry
798 by significantly increasing production (Pillai, 2015). A transition to serial production, large-volume component purchasing,
799 and advanced manufacturing techniques will significantly reduce the equipment costs for small turbines while also improving
800 product quality control. An effort to greatly expand manufacturing capacity should be placed against an industry desire to
801 continue using small plants that are located in the communities they are serving to meet energy justice, diversity, local
802 development, product reliability while also reducing climate impacts associated with global shipping.

803 Balance of station costs include all costs of a turbine system outside of the wind turbine and tower equipment and can represent
804 up to 60% of a small wind project's total installed cost (Orrell and Poehlman, 2017). These costs typically include customer
805 acquisition; zoning, permitting, inspection, and incentive application; engineering and design; transportation and logistics;
806 foundation design and installation; electrical infrastructure; turbine and tower installation and erection; taxes; and overhead
807 and profit. Zoning and permitting costs in particular can be burdensome for small wind. For example, at one point it was
808 reported that potential customers in the Republic of Korea needed written approval from neighbours within a given radius to
809 install an SWT (Kim, 2018).

810 Although not typically a direct one-to-one substitution, the generally lower cost, in great part due to governmental incentives,
811 and easier siting of solar PV gives it a competitive advantage over small wind. From 2008 to 2012, the drop in the overall
812 installed cost of PV systems was mainly due to the drop in cost of crystalline silicon. Since 2012, installed costs have continued
813 to drop due to decreases in other costs, focusing on greatly reducing balance of station costs (Barbose and Darghouth, 2015).
814 In addition, as demand for solar PV increases, production of PV modules can enjoy the benefit of economies of scale, helping
815 further decrease installed costs.

² This small wind capacity value mostly represents wind turbines up through 100 kW in size, with some capacity from wind turbines up through 250 kW in size.

816 **5.1.2 Uncertainty in power curves and local wind conditions, resulting in poor estimations of AEP**

817 The estimation of the AEP of a wind turbine has two main components: the power curve of the wind turbine and the knowledge
818 of the wind conditions on the site. Nordic Folkecenter's Catalogue of Small Wind Turbines (8th edition) lists 302 types of wind
819 turbines with a rated power below 50 kW, only a fraction of which have independently measured power curves (Nordic
820 Folkecenter for Renewable Energy, 2016). This is in stark contrast to large wind turbines, where the vast majority of turbines
821 have independently measured power curves.

822 Over the past decades, there have been multiple facilities developed for SWT testing, some of which are still in operation,
823 some of which are still in operation, providing the performance testing needed to increase the number of SWTs with
824 independently measured power curves. However, the IEC 61400-2 is still the most credited reference to standardize
825 performance measurements, some discrepancies still exist with other references and some aspects are still not completely
826 covered. Further improving this standard could contribute significantly to closing the gap between small-scale and large-scale
827 wind turbines. Only when a standard is applied to all these aspects will wind turbines be reliable. Generally, PV modules,
828 inverters and ancillary systems are more standardized than SWTs, and this one of their keys to lower costs and market success.
829 Because tower heights are commensurate with rotor diameter, SWTs are placed on relatively short towers. Furthermore, tower
830 heights are often restricted below their optimal values by local planning regulations. Due to wind shear, low towers result in
831 lower mean wind speeds and therefore lower production. As discussed, SWTs are also strongly affected by installation at high
832 altitude, where the reduction in air density leads to low Reynolds numbers and in turn to a lower aerodynamic efficiency.
833 Furthermore, the wind flow for SWTs is more likely to be perturbed by nearby obstacles. This has two important effects: (1)
834 the wind pattern can change over very short distances, making the micrositing of SWTs complex; and (2) the wind is likely
835 more turbulent. As a result, even when power curves have been independently measured at a certified test site, those power
836 curves may not be representative of real-life performance on the installation site.

837 The uncertainty in power curves and local wind conditions leads to considerable uncertainty in the estimate of the AEP.

838 In absence of new remote sensing or model-based assessment technologies, the way to reduce uncertainty in the
839 characterization of local wind conditions is to take on-site wind measurements. However, site assessment through on-site
840 measurement is often expensive in relation to the installed cost of SWTs and their generation potential. Deploying instruments
841 for measurement is also far more expensive and more time consuming than using model-based approaches to estimate a wind
842 resource, which has led to limited uptake in the use of on-site measurements for small wind (Tinneland and Sethuraman, 2019).
843 Although expanded consideration of remote sensing and high-fidelity, model-based resource assessment techniques are being
844 developed which may prove reliable for energy production estimation, these are likely to be insufficient in areas with complex
845 terrain, especially because the SWTs are close to the ground. In these cases, a site assessment is necessary for the project to be
846 successful.

847 **5.1.3 Intermittent incentives and regulations between countries**

848 Incentives applicable to small wind can include net-metering, FITs, other types of production-based payments, grants, rebates,
849 and tax credits. Regulations that affect small wind can include government renewable energy goals and mandates,
850 interconnection standards and rules, and utility programmes and interconnection rules. Both incentive programmes and
851 regulations vary widely across countries and utilities. Incentive programmes can vary with respect to the amount and type of
852 funding they provide, what types of projects are eligible to apply, the cap on the number of projects they support, and the
853 length of time they are available. Regulations are highly country and utility specific. For example, in countries with complex
854 terrain good spots are mostly remote (on hills and mountains rather than in large land fields); to exploit these remote areas,
855 network expansion from low-voltage to medium-voltage connection is therefore needed. This increases costs for the investment
856 but simultaneously—and indirectly—helps the distribution companies expand their network with new equipment.

857 As discussed in Section 2, Japan, Italy, the United Kingdom, and the Republic of Korea are examples of countries where
858 intermittent incentive availability and funding levels have changed greatly due to the changes to their FIT programmes over
859 the past approximately 10 years. Changing availability of incentives is one reason why many SWT manufacturers have not
860 been able to remain in the market or do not participate in certain markets. The fluctuating sales presence of small wind
861 manufacturers both in and exporting from the United States and China provide examples of how small wind manufacturers
862 must adapt to different market conditions across countries. In the past, Japan, Italy, and the United Kingdom had been key
863 export markets for SWT manufacturers. With the programmes discontinued or drastically reduced, the markets are much less
864 attractive, and this contributes to manufacturers leaving the market. Long term consistency across incentive programs would
865 greatly improve the development of the SWT sector. The lack of consistency also holds for national certification requirements
866 and is another possible reason for manufacturers leaving the SWT market. If there was a unification (IEC certification, for
867 example), then all the manufacturers could sell globally. For example, six U.S. small wind manufacturers reported international
868 exports in 2015 with just three in 2020 (Orrell et al., 2021). Similarly, sales in China and exports from China have fluctuated
869 with the number of Chinese small wind manufacturers in that market. In 2017, only 15 Chinese SWT manufacturers reported
870 sales, a decrease from 28 in 2014 (Duo, 2017), corresponding to a 60% drop in sales from 2014 to 2017 (Orrell et al., 2021).

871 **5.1.4 Lack of openly available data for detailed validation and development of design tools**

872 Aeroelastic modelling should be the primary methodology for structural and performance assessment of any wind turbine.
873 Such modelling allows the turbine designer to understand and predict the load and power behaviour of the turbine before
874 witnessing it in the field and to demonstrate and optimise the control parameters that have the highest impact on the design
875 and optimize the configuration most efficiently.

876 For the results of an aeroelastic model to be used for design and certification, the aeroelastic code (the software), the turbine-
877 specific inputs, the aeroelastic model setup and usage with those inputs, and the post-processing of the results must achieve a
878 certain level of verification and validation. Most distributed wind modelers utilize the open-source aeroelastic code

879 OpenFAST, or the proprietary code HAWC2. While these tools have received adequate validation in past research work, there
880 remains a need for experimental field data to validate turbine-specific models, especially in the case of SWTs. Publicly
881 available aeroelastic models are well-tuned for traditional three-bladed HAWTs, although less so for downwind HAWTs, and
882 are progressively less and less validated for passive yaw, pitch-to-stall, furling, and VAWT machines (Forsyth et al., 2019).
883 Scarcity of these data is seen in many aspects related to SWTs.

884 In the validation process, the model results are compared to experimental datasets to ascertain the degree to which the model
885 represents the actual physics. Therefore, the validation datasets must be properly collected and quality assured. Validation,
886 however, is not a binary statement about whether a model is valid or invalid, but rather a critical part in the overall assessment
887 of the suitability of the computational model for the intended application (Hills et al., 2015).

888 A successful validation exercise requires close collaboration between the experimentalists, the modelers, certification bodies,
889 and the relevant stakeholders throughout the conceptualization, design, execution, and post-processing phases of the
890 experiments. Additionally, the computational model should be used to help design the details of the experimental campaign,
891 which is effectively another (physical) simulation of the true behaviour of the systems.

892 **5.1.5 Social acceptance and environmental issues (noise, visual impact, vibrations)**

893 In 2016, some studies suggested that around 70 to 80% of people in Europe support wind farms (Allen, 2016), although there
894 were still concerns around noise and aesthetics. However, little was known about public attitudes toward locally developed
895 SWTs. According to (Ellis and Ferraro, 2016), the social acceptance of wind energy is influenced by a much wider and complex
896 set of mutual effects between individuals, communities, place, wind energy operators, regulatory regimes, and technology
897 operating at a variety of geographical scales. Social acceptance should therefore be viewed within this wider set of relationships
898 and as part of the transition to a low-carbon economy. In particular, small wind is commonly located closer to the customers
899 that benefit, but may also have been more expanded impacts to the other local members of the community. For this reason,
900 SWT may stimulate social acceptance of wind energy if the installation and the technology used is really adequate and if local
901 benefits are shown.

902 In 2016, a research survey was completed looking at the drivers of public attitudes toward SWTs in the UK (Tatchley et al.,
903 2016). The results showed that half of respondents felt that SWTs were acceptable across a range of settings, with those on
904 road signs being most accepted and those in hedgerows and gardens being least accepted.

905 Similar to the results obtained in a survey developed in Europe for the SWIP Project (SWIP Project, 2014) about the awareness
906 level and public opinion of SWTs, more than 75% of people interviewed showed a positive reaction to the installation of SWTs
907 in their environment and only 5% showed a negative reaction. Even for all demographic groups involved, the response was
908 more positive to SWTs than large, utility-scale wind turbines. "Energy Communities" schemes increased this acceptance rate
909 because more people are able to invest and benefit from a wind turbine investment. Generally, people feel detached from large,
910 utility-scale wind facilities because they do not see the same direct benefits as in the case of SWT investments. Another
911 conclusion was that industrial sites were regarded as the most acceptable places for installing SWTs, far ahead of the second

912 place response of roofs in residential areas. Even so, a bad attitude toward SWTs is still noticeable in politics and local
913 administration in many regions, especially in those countries where historical or aesthetic restrictions are present (e.g., Italy).
914 In relation to noise emissions, SWT manufacturers have identified noise as a concern (also because some countries do require
915 noise emission evaluations) and new SWT designs are typically less noisy. However, the general opinion is still that SWTs
916 are noisy, especially if they are compared with solar PV.

917 For visual impact (including visual flicker), noise, or safety issues, considerably less concern was shown than toward
918 performance issues or high investment costs. This is supported by the fact that when an adequate support programme for small
919 wind is established, social concerns decline. Nevertheless, their visual impact in an urban area can still be a source of concern.
920 According to (Emblin, 2017), developers must find smart ideas and designs to integrate turbines into communities and to
921 educate local populations about the long-term benefits and impacts that SWT can bring. The visual impact can also be
922 minimized if the turbines are placed carefully and sensitively, although turbine design also plays a significant role. These are
923 all issues that may be addressed through expanded social science research, science based community engagement and
924 innovations in design and software.

925 Vibration is another relevant issue, especially in roof-mounted wind turbines with no adequate damping solution and/or SWTs
926 operating under high-wind conditions regulated by passive power regulation techniques. In those cases, vibration is transmitted
927 through the pole to the roof or to the ground. When the turbine is sited near dwellings, residents have been known to express
928 annoyance.

929 **5.1.6 Real and perceived concerns with SWT reliability and the high cost of certification.**

930 As discussed, financial incentives in the form of FITs, direct-pay grants, and tax credits help strengthen the global distributed
931 wind market. Incentive agencies and other industry stakeholders have worked to formulate and implement programme
932 eligibility requirements to ensure the public funds used in these programmes are directed to successful projects and
933 embarrassing failures are avoided. One common strategy is to require third-party certification of the wind turbine system
934 according to national and international standards. The goal of the standards is to provide meaningful criteria upon which to
935 assess the quality of the engineering that has gone into an SWT and to provide consumers with performance data that will help
936 them make informed purchasing decisions, e.g., (IEC: International Standard, 2019b). While certification attests that a wind
937 turbine has been tested and designed according to requirements in the relevant standards, a third party cannot guarantee that a
938 turbine model will exhibit perfect reliability in the field. Therefore, a level of surveillance must be put in place by the
939 certification body to monitor and respond to field failures, in collaboration with the turbine manufacturer.

940 While certification helps improve the reliability of deployed wind turbines, it comes at a significant cost, although efforts have
941 been made to reduce the complexity and cost of meeting standards for SWTs. To achieve certification, the turbine must be
942 field tested for power performance, acoustic noise, safety and function, and durability. The turbine designer must also generate
943 a significant engineering report documenting the calculation of turbine loads, both extreme and fatigue, and the structural
944 analysis of the major components in the load path. These test and design reports are then evaluated by a third party, usually an

945 internationally accredited certification body. If the work is found to conform with the applicable standards, certification is
946 granted, making the turbine model eligible for financial incentives. The validity of the certificate must then be maintained
947 because of design changes or other factors.

948 Other certifications or dedicated studies are typically required as part of the installation process, including structural
949 engineering of the tower, the foundation (mostly within the permitting phase), and electrical safety (part of the IEC
950 certification) related to protection from electrical shock and fire.

951 While it is very difficult to find publicly available data for field testing and reporting, industrial contacts of the authors in
952 Europe determined that it costs about 200,000 € (230,000 \$) for the complete design assessment of an SWT, while field testing
953 and reporting alone can cost upwards of 85,000 € (100,000 \$) and third-party certification can cost up to about 43,000 €
954 (50,000 \$). Small and medium wind turbine manufacturers in the United States have reported that certification costs, including
955 fees, direct expenses, and labour time, range from \$150,000 (134,000 €) to \$500,000 (435,000 €) (Orrell et al., 2020).

956 **5.2 Improvement areas**

957 By addressing the five identified grand challenges, SWT technology is expected to decrease significantly in cost, become more
958 accepted within the distributed energy investment community, and demonstrate acceptable community impact to allow direct
959 community-based acceptance. To this scope, the following section reviews some main improvement areas where major
960 research and development is suggested to allow the global SWT market to flourish.

961 **5.2.1 Changes in turbine design and control**

962 The task of designing, manufacturing, and installing SWTs has always been challenging. Suppliers of small wind technology
963 must produce a product that will be deployed in a wide variety of sites around the globe, maintain reliable operation with
964 minimal maintenance, and be an economically viable choice. For small wind to maintain a competitive stance in the
965 international distributed clean energy market, future designs must be further optimized, lowering the LCOE. Unlike the process
966 used largely for current SWT products on the market, future optimized SWT designs will need to utilize validated aero-servo-
967 elastic modelling as a design tool starting at the concept phase, utilize low-cost, reliable overspeed protection methods, and
968 incorporate strategies including design for manufacturing, design for certification, and design for installation, and design for
969 recycling, all before initial prototype testing and ideally in the framework of improved and more detailed, internationally
970 accepted design standards.

971 While addressing all these is beyond the scope of this study, some key enabling actions are proposed in the following, clustered
972 together based on the main technical areas.

973

974 **Aerodynamics**

975 Basic wind turbine aerodynamics lead to the statement that a good blade is composed of good airfoils: “good” in the sense of
976 having a high lift-to-drag ratio. At the low Reynolds numbers of SWTs, this is a major design challenge that has languished

977 for over two decades. Given the developments in Reynolds-Averaged Navier–Stokes (RANS) turbulence and transition
978 models, a design methodology is becoming available to overcome the limitations of conventional panel methods in use up to
979 now. In particular, better modelling of the near- and post-stall region of airfoil polars is key not only to improve stall-controlled
980 machines, but also to get more reliable estimations of loads in a variety of DLCs prescribed by the standards, thus leading to
981 better prediction of turbine lifetime and possibly enabling lower safety factors. Innovations at the airfoil level should not only
982 focus on pure aerodynamic performance (in terms of high glide ratio, resistance to stall, and low sensitivity to Re variations),
983 but also on further lowering noise levels to make turbines more suitable for installations in proximity to populated areas
984 (improved certification labelling could also be useful in this regard).

985 The introduction of *smart blade* technologies for flow control in SWTs may provide a significant boost toward better designs
986 in the near future. For example, the potential of retrofitting SWTs with passive flow control elements such as vortex generators
987 and Gurney flaps to improve their starting behaviour and to reduce the risk of stall caused by roughness has recently shown
988 very promising prospects (Holst et al., 2017).

989 **Aeroelastic modelling**

990 Up to now, SWT blades have been much stiffer and protected by large safety factors in their structural design than blades for
991 large turbines. To enable wider use of this simulation tool for design and optimization, gaps and barriers to its use must be
992 identified and solutions implemented (Damiani et al., 2022). Growth in the theoretical knowledge owned by SWT-producing
993 companies and a wider availability of easy-to-set, open-source tools will also be required. To evaluate the impact of the above,
994 (Evans et al., 2018, 2021) investigated blade fatigue by undertaking aeroelastic simulations of six SWTs up to 50 kW in rated
995 power using OpenFAST (OpenFAST, 2019). Their research shows that the fatigue DLC in IEC 61400-2 is unduly pessimistic
996 and that more detailed aeroelastic modelling to allow the design of fatigue-resistant blades at lower cost will be needed. To
997 support more efficient designs while reducing blade cost and weight allow for a blade weight/cost reduction and more efficient
998 designs, aeroelastic modelling should be increasingly used in SWTs design, as it has been used for utility-scale turbines. To
999 enable wider use of this simulation tool for design and optimization, several gaps and barriers for to its use across the SWT
1000 industry must be identified and addressed (Damiani et al., 2022). Growth in the theoretical knowledge of typically small,
1001 owned by SWT-producing companies and a wider availability of easy-to-set-up, open-source tools will also be required.
1002 Additionally, the challenge of expanding the use of aeroelastic models must be supported through dedicated verification and
1003 validation campaigns on a number of different turbine archetypes, sizes, and computational codes. One particular area of
1004 importance for very small turbines is the need for better understanding of yaw behaviour of turbines with a tail fin. Yaw
1005 response gives rise to gyroscopic ultimate and fatigue loads, which can be the largest loads on a turbine of around 1 kW (Wood,
1006 2011). None of the currently available aeroelastic codes contain a tail fin model.

1007 **Control**

1010 Control strategies for SWTs must also evolve to become more robust and cost-effective. We see an example of this evolution
1011 in the contemporary trend of turbine designers moving from tail furling to stall regulation and in some cases pitch regulation.
1012 An example of this transition is the evolution of the Bergey Excel 10 turbine toward the Excel 15 (Bergey Wind Power, 2022).
1013 The change was in both the increase of power capture via a larger, more efficient rotor and the moving away from the furling
1014 strategy toward a more controlled-stall strategy. Other manufacturers (e.g., (Tozzi Nord, 2022)) are proposing models with
1015 both active yaw and pitch. The difficulty here is to package these controls in relatively tight spaces while still guaranteeing
1016 reliability and redundancy. A recent research article (Damiani and Davis, 2022) explores the technical and economic viability
1017 of retrofitting a stall-controlled turbine with pitch control together with an extended rotor for increased power capture. Both
1018 pitch-to-stall and pitch-to-feather approaches are investigated, and the advantages of each solution are discussed. The authors
1019 devise a compact, redundant independent pitch-control system, but conclude that, for power regulation, the economics do not
1020 warrant the extra complexity of the pitch control, which is then relegated to overspeed protection alone. More research and
1021 technical support in this direction is needed because the experience of utility-scale machines is not directly applicable in SWTs
1022 due to cost and physical constraints. However, as discussed in Section 4, recent studies suggest that the use of pitch control
1023 could significantly improve the efficiency of SWTs (Papi et al., 2021) and new grid integration requirements being driven by
1024 the expanded use of distributed generation may require more active power control than what can be achieved through traditional
1025 controlled stall designs.

1026

1027 **Generator and drivetrain**

1028 The unsteady behaviour of SWTs, especially during start-up, depends on drivetrain and generator resistance (Vaz et al., 2018).
1029 Typically, the wind speed at which an SWT begins power production as the wind increases in strength is significantly higher
1030 than the speed at which it ceases production as the wind dies away (Wood, 2011). The cut-in wind speed is usually an average
1031 of these two speeds and therefore can give a misleading indication of what wind speed is needed for an SWT to start producing
1032 power. In particular, the cogging torque of permanent magnet generators (PMGs) can be a major impediment to very low wind
1033 speed start-up of small turbines. This problem is exacerbated because, due their relatively small size, SWT manufacturers are
1034 typically forced to purchase third-party generators that may not match their blade design, resulting in the need for higher wind
1035 speeds to overcome the cogging torque of the generator. Additionally, because there appears to be few uses for PMGs in the
1036 sub-10 kW capacity, there is little market pressure on generator manufacturers to optimize their designs for SWT applications.
1037 Eventually, SWT manufacturers may design and build their own generators, but turbine sales must expand greatly to warrant
1038 this large investment. The design of turbine-specific generators, optimized with specific blade and rotor design, would require
1039 improved understanding of generators, control systems, permanent magnet design, and the use of modern additive
1040 manufacturing.

1041

1042

1043

1044 **Design strategies**

1045 Knowing that an SWT must be manufactured, tested, certified, installed, maintained and then recycled at the end of its life
1046 puts pressure on the designer to incorporate this thinking into the design from the initial concept. Understanding key market
1047 drivers, such as subsidies that may incentive capital costs compared to operational costs must be considered carefully to balance
1048 up front and operating costs, in turn making the LCOE of SWTs more competitive. Several, sometimes competing, additional
1049 design strategies that may be implemented that will impact turbine performance and cost include *Design for manufacturing*
1050 (incorporating the manufacturing in the design process to avoid future issues in fabrication and assembly), *Design for*
1051 *certification* (incorporating conformity with the relevant design standards early in the design process to avoid future issues in
1052 the design evaluation and turbine certification), lastly, since the SWT must be shipped, installed, and commissioned; *design*
1053 *for installation* strategies must be considered, especially if the turbine is to be deployed in remote or isolated locations. With
1054 this in mind, the complete small wind system, including the foundation, tower, inverter, wiring, disconnects, monitoring,
1055 nacelle, access platforms, and rotor, will need to be designed in a way that makes the installation process efficient, well thought-
1056 out, innovative, and safe.

1057
1058 **Novel concepts**

1059 While continuously improving existing concepts and archetypes, the recent novel designs discussed in Section 4 like DAWT,
1060 Darrieus VAWTs, and mostly recently AWE still deserve attention and research efforts, since they could represent an important
1061 future contribution to distributed power production. Novel turbine concepts, however, are not limited only to the individual
1062 turbine performance, but should also include holistic considerations of different elements, from economics to social
1063 perspectives, which will be further discussed in subsequent sections.

1064 **5.2.2 Open data from field experiments**

1065 Many, but not all, SWT manufacturers remotely monitor the operation of their turbine fleets. For many smaller turbines,
1066 monitoring focuses on electrical parameters that are measured as part of the inverter system, but ongoing measurements of
1067 many turbine-specific parameters simply increases the cost and maintenance requirements of turbine systems. Sharing any
1068 available remote monitoring data is an opportunity for researchers and manufacturers to collaborate on a variety of potential
1069 research areas that could expand small wind markets while also helping reduce costs. These areas include isolating and
1070 identifying the factors that affect why actual performance differs from predicted performance in real-world conditions and
1071 then improving performance prediction tools accordingly, improving wind resource assessment data and models for small
1072 wind, calculating actual LCOEs, using the performance data to understand wind's complementarity to solar PV, and enabling
1073 wind to complement and communicate with other distributed energy resources in the grid of the future. The inability to predict
1074 performance consistently and accurately can negatively affect customer confidence in small wind and access to financing.
1075 Increasing investor confidence, reducing perceived risk, and decreasing assessment costs with improved tools and datasets will
1076 help small wind achieve large-scale deployment. In this regard, however, it must be clarified that the real "performance" of a

1077 wind turbine system is the amount of achievable AEP. As discussed in Section 5.1.2, this actually is driven by variables beyond
1078 just turbine technology, including, but not limited to, the project’s available wind resource, siting (i.e., tower height, local
1079 obstructions, and other micrositing issues), and turbine availability (i.e., downtime for expected or unexpected maintenance or
1080 grid outages). These variables contribute to why accurately estimating small wind project performance can be challenging. A
1081 better prediction of performance can then be synthesized into the proper combination of good resource estimation coupled with
1082 accurate power performance and then with the guarantee that the turbine will provide that same level of power over its design
1083 life. While the current performance prediction tools generally focus on the first of these questions, which is driven by good
1084 resource assessment and accurate representation of the turbine power curve as discussed above, they largely do not address the
1085 second part, which is failure analysis. Open data on turbine failure mechanisms for the verification and tuning of performance
1086 prediction tools will then need not only to cover turbine performance vs. actual wind resource, but also real production vs.
1087 time, fatigue, and failure analyses.

1088 Regarding prediction tools, in particular, special attention is also needed to make available open data to *calibrate and further*
1089 *develop design aero-servo-elastic tools* (see Section 5.2.1) in operating conditions outside of turbine-specific validation that
1090 may be needed as part of turbine certification processes. Having detailed field data that may only be available from heavily
1091 instrumented research-grade turbines in the wind tunnel (e.g., those shared in internationally coordinated programmes like
1092 those from the International Energy Agency (IEA) Wind Technical Collaboration Programme) will foster the development of
1093 more robust design tools for SWTs, enabling the modelers to improve the accuracy of the turbine design tools. Data must also
1094 be collected over a wide range of operating conditions, from the standard steady-state operation to predicting the turbine loads,
1095 performance, and lifetime in actual operating conditions. In this sense, the tools can be validated for scenarios that can be
1096 significantly different from one particular site to another site, e.g., different turbulence levels, anisotropy, wind speed, wind
1097 direction, ground stability, etc. An overview of measurement data collected within IEA projects is given in (Schepers and
1098 Schreck, 2019). These projects also provide examples of how international consensus on sharing data will help the users
1099 validate models while maintaining any needed confidentiality.

1100 **5.2.3 Improvements in installation, maintenance, and life-cycle analysis**

1101 Over the 10 years from 2010 to 2020, the cost for installing residential-scale solar PV systems in the United States has seen an
1102 approximately 64% reduction in benchmark costs. 42% of these costs have been attributed to installation labour and additional
1103 soft costs, such as siting, permitting, sales tax, and overhead (IEA, 2020). Although a smaller percentage of overall total costs,
1104 significant reductions are seen in structural and electrical hardware costs outside of the inverter and solar module. These
1105 installation costs (the total cost outside of the module and inverter) now make up almost 70% of the total installed cost of a
1106 modern residential-scale solar PV system (Feldman et al., 2021). Limited published data exists for similar balance of station
1107 installation specific costs for small wind ((Orrell et al., 2021) as an example), but a 2017 study of the U.S. distributed wind
1108 market shows that similar costs represent 63% of the cost of residential wind systems (Orrell and Poehlman, 2017), which

1109 indicates that if a cost reduction of a similar magnitude as that demonstrated in the solar industry can be achieved for small
1110 wind, this would represent a 25% reduction in the installed costs of small wind systems.

1111 To date, limited systematic analysis has been undertaken to identify methods to reduce the installation costs of small wind
1112 technology. Having more of these studies for different countries and environments is considered a key research area for the
1113 evolution of small wind systems.

1114 The SMART Wind Roadmap (DWEA, 2016) identifies a set of potential cost-reduction opportunities based on a consensus-
1115 based collaboration of small wind industry members. Most of the focus of this work was in the area of turbine hardware cost
1116 reductions, but the report does identify tower, foundation, and turbine erection costs as significant cost drivers for small wind,
1117 on par with the costs of the turbine hardware itself. Recent work by industry has focused primarily on reducing the costs of
1118 towers, primarily developing self-erecting mono-pole towers that provide lower installation and turbine maintenance costs.
1119 Recent efforts to reduce installation costs through the DOE-funded Competitiveness Improvement Project (NREL, 2021) have
1120 focused on tower and foundation design, including the use of low or no concrete foundations for SWTs, which can greatly
1121 reduce turbine installation timelines and costs. Expanded cost reductions could also be expected in site assessment with the
1122 expanded use of modelling tools, simplified installation procedures, and reductions in project acquisition and project
1123 permitting, each of which needs to be explored in more detail.

1124 Similarly, a full understanding of O&M costs of DWTs is limited. As introduced in Section 3.2, the most recent U.S.
1125 Distributed Wind Market Report (Orrell et al., 2021) provides an estimate of cost of 37 \$/kW (32 €/kW) per scheduled
1126 maintenance site visit, which is typically required annually. This cost has not seemed to decrease over time. In comparison,
1127 O&M expenses on a \$(€)/kWh-yr basis for residential-scale solar PV systems has dropped by almost 50% over the last 10
1128 years, again demonstrating strong potential for cost savings (Feldman et al., 2021). Maintenance needs of small turbines cover
1129 a range of requirements. Most residential and small commercial turbines are designed to require minimal ongoing maintenance,
1130 such as bi-annual inspections and potentially blade reconditioning, depending on the environment. Turbines greater than 50
1131 kW in capacity are assumed to undergo more ongoing maintenance, similar to large wind turbines. Ideas that have been
1132 identified to support lower long-term maintenance costs include the expanded use of remote monitoring to understand service
1133 needs before maintenance is required and expanded turbine structural modelling to eliminate unplanned maintenance.
1134 Systematic approaches to reduce maintenance for the distributed wind fleet should also be pursued. Although individual
1135 manufacturers have a good sense of long-term turbine-specific component failure rates, no system-wide assessment has been
1136 undertaken to focus research efforts into components that have higher service requirements, such as power electronics. This
1137 would also represent a key enabler. Focusing on local and national standards will isolate the SWT manufacturers in the borders
1138 of their countries. Unification under a common standard (such as IEC) should be proposed as for PVs. History also shows how
1139 the SWT market has failed to follow the large wind turbine and PV pace for growth.

1140 Although stories abound of particular SWTs operating for decades, factual data on the full life-cycle cost and performance of
1141 many SWTs is limited, reducing the ability to assess the long-term cost of energy for small wind systems. Additionally, the
1142 wide variety of turbines, their almost constant change in design, and limited number of operational small turbines that have

1143 undergone a full certification to national and international standards also make it challenging to develop meaningful,
1144 information-based estimates of life-cycle cost as has been done with other technologies. To support the better full assessment
1145 of life-cycle costs, NREL developed a cost taxonomy for distributed wind (Forsyth et al., 2017) that has been applied in a
1146 small number of cases such as (Orrell and Pohlman, 2017). Most work today focuses on articulating costs based on the
1147 installed cost of wind technology, making assumptions on maintenance costs and long-term turbine performance. Estimates of
1148 life-cycle costs for SWTs at and below 10 ¢/kWh (8.7 ¢cent/kWh) are being reported but have not been independently
1149 demonstrated or verified. A better estimation of life-cycle costs of SWTs is considered a key enabler. In doing so, of critical
1150 concern is an accurate accounting of long-term turbine production. Work has been undertaken in relation to an improved
1151 estimation of the site-specific wind resource, a topic that is more complicated due to the higher likelihood of local obstructions
1152 (Drew et al., 2015). Long-term performance production, which could include consideration of long-term wind turbine
1153 availability, turbine performance degradation, and increased impact of obstacles such as vegetation growth, have not been
1154 systematically considered to date and would definitely improve these estimations (see also Section 5.2.2).

1155 **5.2.4 Regional appreciation of distributed generation and integration with storage systems**

1156 Although historically used in remote and edge-of-grid applications (Hemeida et al., 2022; Duchaud et al., 2019), the continued
1157 decrease in the costs of renewable energy generation and storage technologies, combined with incentive programmes and
1158 policies to support local generation, have resulted in a wider acceptance of grid-connected distributed generation. With the
1159 advent of lower-cost controls, advanced power electronics, and improved communication systems, the use of more distributed
1160 power generation is becoming common. Additionally, new efforts to expand clean energy development, paired with the high
1161 costs and typically long project development timelines for transmission development, make the use of distributed generation
1162 even more cost-effective as a way to support local power development. Lastly, although it typically requires additional
1163 expenses and planning, distributed generation can also be used to support grid resilience when combined with storage and
1164 other grid-forming technologies. The bold plans of the European Union as well as many other countries around the world in
1165 the direction of e-mobility requires significant infrastructure investments to facilitate the millions of electric vehicle chargers
1166 that will be installed. This expansion will, however, put an additional large load on existing low-voltage grid infrastructure
1167 that, in most countries, is old and extremely expensive to upgrade. The strain on the low-voltage grid cascades toward the
1168 medium-voltage infrastructure, which is also coming much closer to its capacity limits.

1169 Enhancing this development while maintaining a reasonable cost involves simultaneously unloading the low- and medium-
1170 voltage grid from some capacity through local energy generation and storage. This is possible when buildings and households
1171 in local communities are able to become "net prosumers", meaning that they are simultaneously energy producers and
1172 consumers. In the future, these prosumers can serve as active members of the energy system network with the ability to
1173 exchange energy and offer stabilizing services to the grid. This is achieved through the integration of renewables with storage
1174 in combination with decentralized control. Solar has been the first technology to be successfully combined with storage on a
1175 residential or local community level, contributing effectively to the "net prosumer" concept. SWTs have been traditionally

1176 very simplistic with respect to their design and control, making their combination with storage more difficult. However,
1177 numerous current designs include variable-speed full converter AC/DC/AC turbine concepts and have been successfully
1178 integrated with modern storage technologies. The combination of SWTs with fast-response storage systems allows for the
1179 generation of significant quantities of energy at the low-voltage grid level with a simultaneous grid stabilization capability that
1180 is able to unload capacity in an effective manner from the grid. Similarly, combining wind, solar, and storage in many parts of
1181 the world where wind and solar are not typically coincident, either daily or seasonally, could provide expanded benefits to the
1182 low- and medium-voltage energy distribution network. Actions can also be carried out directly on wind turbine design and
1183 control, e.g., integrating fault ride through technologies.

1184 The biggest challenges for this integration involve the volatile nature of wind turbine operation, which requires a very fast
1185 response from the power electronics and storage technology to maintain constant production levels and allow for fast-response
1186 voltage and frequency regulation. However, building on the distributed generation concept into regional development, the
1187 wider use of distributed wind combined with solar and storage at small scales across a region will reduce the variability
1188 experienced with just single units, providing more reliable and less transient power, likely at a reduced cost and certainly faster
1189 than large-scale transmission system development.

1190 To address the expanded need for energy to remote areas not served by current energy infrastructure across the globe, SWTs
1191 in combination with solar, storage, and advanced load control technology is likely to play an expanding role. Although most
1192 investments within the energy access space currently focus on solar and storage, growing energy needs will make it difficult
1193 and expensive to rely on oversized solar and storage facilities to provide full-time power. The use of SWTs and other renewable
1194 energy devices such as pico-hydro and biomass can provide energy at different times than solar, reducing the cost and space
1195 requirements of large storage systems. The limited civil infrastructure and difficulties in providing the on-site service expertise
1196 that is required for larger wind turbines will make SWT technologies more applicable for these more remote applications.

1197 **5.2.5 Shared programmes of incentives and social actions to improve acceptance**

1198 The majority of renewable energy incentives are targeted at large-scale wind projects and wind farms, where scale is a critical
1199 component in a country's wind energy development success rate (Wolsink, 2013). Social acceptability can also be construed
1200 as commercial acceptance in the case of small wind. Wind energy is naturally more complex to diffuse than other energy
1201 alternatives such as solar panels because it frequently involves infrastructure (foundation, tower, and grid interconnection).

1202 If the economic competitiveness of SWTs can progress significantly as a result of improvements in efficiency, manufacturing,
1203 and siting, then the technology could be sustained in the transitory phase by more coordinated political and regulatory actions
1204 at large scale. For example, a federation like Europe could promote the harmonization of incentives between the countries,
1205 although energy policies are still managed individually by the members. This could create in turn a common, broader market
1206 for SWTs, promoting the development of an economy of scales. Moreover, different from previous practices, the time
1207 framework for these incentives to stay in place should be clearly assessed to reassure investors and companies and prompt

1208 them to bid on the technology. In this context, networks of research institutions like EAWE in Europe, NAWEA in the United
1209 States, or of wind energy industries like WindEurope can play an important role advising regulatory bodies and politicians.
1210 Social acceptance of SWTs could potentially be improved if the drawback on local ecology such as the habitats of birds,
1211 insects, and other small animals, as well as noise and vibrations, can be minimized. While these concerns are largely debated
1212 in utility-scale machines and a vast literature does exist, the environmental impacts of SWTs are not so well defined as a result
1213 of less scientific research on the topic. Additional studies and projects on the topic would also represent an important enabler
1214 to improve acceptance of small wind.

1215 Finally, it is worth mentioning that the diffusion of small wind technology could also be supported by actions that are somehow
1216 a combination of technical and social aspects. A good example of this is a *virtual net-metering approach* (Hellenic Electricity
1217 Distribution Network Operator S.A., 2021). Under this scheme, consumers could install SWTs away from the consumption
1218 meter and liquidate the energy as a classic net-metering. There is a trend where companies try to get "green electricity" from
1219 their providers or through their own investments to compensate for their footprint (Wang, 2013). This will and should get
1220 amplified in the next few years as companies of all sizes try to become greener. These efforts will boost the sector but also in
1221 a more secure and professional way because this "green point system" will push the wind turbine makers toward real power
1222 curves and better products (Simic et al., 2013). Additionally, a link between this type of investment with ESG [environmental,
1223 social, and governance] policies will boost the market even more due to the comparative advantages of SWTs. For example,
1224 many industrial consumers who have already installed PVs may be eager to increase their green electricity, but they may not
1225 have space available for additional PV.

1226

1227 **5.3 Key enablers**

1228 As a final product of the work, the aforementioned areas of focus are synthesized below in 10 key enablers that, in the authors'
1229 opinion, more than others would represent the catalysts for a significant development of SWT worldwide.

- 1230 • Aeroelasticity for SWTs – If aeroelasticity has represented the main driver of the size and capacity factor of utility-
1231 scale machines, its diffusion to SWTs could also be extremely beneficial. For example, an improved aeroelastic design
1232 could contribute to reducing the structural safety factors, in turn enabling a blade weight and cost reduction and more
1233 efficient designs. To enable wider use of aero-servo-elastic simulation tools for design and optimization, gaps and
1234 barriers still need to be identified and solutions implemented, including growth in the theoretical knowledge owned
1235 by SWT-producing companies and wider availability of easy-to-set, open-source tools.
- 1236 • Improvement in control strategies – To achieve more effective and robust control, thus maximizing the energy
1237 conversion, a transition away from furling toward more controlled-stall strategies is also seen in very small machines.
1238 Moreover, some manufacturers are proposing models with both active yaw and pitch. While the implementation of
1239 these controls in SWTs is not straightforward due to the difficulty of packaging them in relatively tight spaces while
1240 still guaranteeing reliability and redundancy, recent studies suggest that the use of active pitch and yaw controls could
1241 significantly improve the efficiency of future SWTs.

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- Improvement in design, with a focus on the characterization of airfoil aerodynamics at low Re – Improvements in the design of SWTs will be needed at any level, from the rotor-nacelle assembly (e.g., minimization of drivetrain and generator resistance, with particular reference to the cogging torque) to blades’ material and cost, or use of cheaper materials for some of the most expensive components such as the towers. Among others, a key area for improvement is defining (possibly validated with experiments) accurate and reliable airfoil polars with the low Reynolds number range that SWT blades usually work with, remembering their strong sensitivity to air density variations due to installations in altitude for example. Having those data available will produce benefits at different levels, including more effective aerodynamic designs, better prediction of loads, and a more reliable definition of turbine control (especially in stall-controlled machines). Special attention should also be given to aerodynamic noise in view of turbine installation in proximity to populated areas.
 - Open data from both wind tunnel and field experiments – Open data for verification, validation, and optimization of SWTs are seen as a key enabler for the future evolution of the technology. In particular, thanks to the smaller size of SWTs compared to utility-scale machines, they can be placed at full scale or at low scale in a wind tunnel, meaning that reliable testing can take place in the controlled and known wind tunnel environment. Data collected in these conditions would be of particular use for the evolution and calibration of simulation tools. On the other hand, there is also an urgent need for different open datasets, i.e., related to field measurements of real turbine performance. These will need to not only cover turbine performance vs. actual wind resource, but also real production vs. time, fatigue, and failure analyses.
 - More accurate performance and resource assessments – More accurate assessments of both the real performance of SWTs and the wind resource are key to improving design, siting, and operation. Regarding performance assessment, a better quantification of several factors could be beneficial, including the impact of turbulence or the effect of obstacles. For example, a DOE-funded project plans to include obstacle modelling research results as an add-on feature to wind resource data for the United States available via an application programming interface. Regarding resource assessment, high-fidelity Computational Fluid Dynamics (CFD) simulations could provide a significant contribution, even though the economic convenience of their computational cost must still be proven.
 - Variable validation and verification of SWTs, especially for non-traditional archetypes – Balancing certification requirements from a regulatory point of view, which prioritizes design thoroughness, model validation, and public safety, against requests from the original equipment manufacturers for more streamlined and economical approaches to certification is difficult. Therefore, there is an immediate need for breaking SWTs into categories for load assessment and validation requirements that account for both size and archetype. Smaller turbines and more established archetypes would benefit from less onerous requirements in terms of load assessment and validation, whereas more complicated machines would require a more in-depth review of the prediction capabilities of the code used for design and load analysis. Verification and validation guidance in the current design standards is limited, and this is one area that requires more research and data to increase the diffusion of DWT and SWTs.

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- Standardization – Standardization at different levels is key for further development of SWT technology. First, standardization is needed for components to promote an economy of scale. In particular, it is suggested that generic products are designed and produced to achieve economies of scale, in turn enabling reduction of the purchase cost of SWTs. Examples of this could be the design and production of a generic rotor blade family or lighter and easier-to-install towers. Similarly, research must be focused on the utilization of lower-cost generators, possibly available on the market with a standardized design. Standardization would come with non-negligible technical challenges but could represent the key catalyst for reducing the LCOE in the near future. Moreover, more effective standardization is needed for regulations and standards. Regulations for SWT installation among different countries are also largely variable and making those regulations more uniform through international coordination would represent another pillar toward the creation of a stable market for the technology. Standards should instead evolve along with the changes in the design and operation of new machines, with a special focus on aeroelastic design and certification. In particular, we suggest that a major enabler could be the differentiation of standards as a function of turbine archetype.
 - Detailed studies on cost and life-cycle analysis – To date, limited systematic analysis has been undertaken to identify methods to reduce the installation costs of small wind technology. Having more of these studies for different countries and environments is proposed as a key enabler for the evolution of small wind systems, in connection with the impulse toward standardization. The same applies to life-cycle costs, in which a critical concern is accurate accounting for long-term turbine production; this should include consideration of long-term wind turbine availability, turbine performance degradation, and increased impact of obstacles, such as vegetation growth, which have not been systematically considered to date and would definitely improve the estimations.
 - Grid compliance and integration, including storage systems – To comply with most of the current grid codes as well as the upcoming grid code modifications, SWTs of larger rated power should probably mostly become variable speed and make full use of AC/DC/AC converters. Also, new SWT developments will likely make larger use of fault ride through technologies because they are becoming compulsory for small-scale generating systems. Beyond this, the combination of SWTs with fast-response storage systems is thought to be key for allowing generation of significant quantities of energy at the low-voltage-grid level with a simultaneous grid stabilization capability that is able to unload capacity in an effective manner from the grid. Similarly, combining wind, solar, and storage in many parts of the world where wind and solar are not typically coincident, either daily or seasonally, could provide expanded benefits to the low- and medium-voltage energy distribution network and support the establishment of a significant market for small wind technology.
 - Shared programmes of incentives and new paradigms to support SWT diffusion, with special focus on social acceptance – Both incentive programmes and regulations have been widely variable across different countries, making it difficult for producers to stay in the market. More coordinated political and regulatory actions at a large scale should be fostered in view of the creation of a broader market for SWTs, thus promoting the development of an economy of scale. Different from previous practices, the time framework for these incentives to stay in place should

1310 be clearly assessed to assure investors and companies and prompt them to bid on the technology. In this context,
1311 networks of research institutions or wind energy industrials could play an important role in advising regulatory bodies
1312 and politicians. All these actions must be coordinated with a better understanding of the environmental impacts of
1313 SWTs so that greater social acceptance can be achieved

1314 **6 Conclusions**

1315 For SWTs to be widely successful, tomorrow's technology will require a new generation of turbines optimized for complex,
1316 low wind speed locations with high turbulence that can also successfully and reliably operate throughout their design life,
1317 producing the power expected when they were installed. Such turbine designs will require higher-fidelity modelling and
1318 simulation to support lower-order tools for design and optimization of turbine systems in complex installation contexts. These
1319 models will need additional open data for validation and calibration, which are currently very scarce. Also, advancements in
1320 control and materials will be needed to improve the energy capture in gusty flows and to reduce the overall cost. Additionally,
1321 these higher-efficiency and reliable turbines must be paired with accurate performance assessment tools to ensure life-cycle
1322 power production, providing confidence to consumers and financiers alike. Finally, these turbines will be more effectively
1323 integrated with storage systems to achieve higher appreciation of small wind for distributed generation.

1324 To make this scenario possible in the near future, the present study suggests five grand challenges for the small wind
1325 community, on which common and synergic efforts should be devoted. These grand challenges translate into:

- 1326 (1) improve energy conversion of modern SWTs through better design and control, especially in the case of turbulent wind
- 1327 (2) better predict long-term turbine performance with limited resource measurements and prove reliability
- 1328 (3) improve the economic viability of small wind energy
- 1329 (4) facilitate the contribution of SWTs to the energy demand and electrical system integration
- 1330 (5) foster engagement, social acceptance, and deployment for global distributed wind markets.

1331 To overcome these challenges, the main unknowns and gaps that must be filled have been presented, as well as the main
1332 improvement areas in which major research and development actions should be devoted. As a final product of the work, 10
1333 key enablers are proposed by the authors as the proper catalysts for a significant development of SWT worldwide, i.e.:

- 1334 I. More effective use of aeroelasticity for SWTs
- 1335 II. Improvement in control strategies
- 1336 III. Improvement in design, with a focus on the characterization of airfoil aerodynamics at low Re
- 1337 IV. Open data from both wind tunnel and field experiments
- 1338 V. More accurate performance and resource assessments
- 1339 VI. Variable validation and verification of SWTs, especially for non-traditional archetypes
- 1340 VII. Standardization
- 1341 VIII. Detailed studies on cost and life-cycle analysis

- 1342 IX. Grid compliance and integration, including storage systems
1343 X. Shared programmes of incentives and new paradigms to support SWT diffusion, with special focus on social
1344 acceptance

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1361 Some authors are members of the editorial board of *Wind Energy Science*. The peer-review process was guided by an
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1363 **Author contribution**

1364 All authors were involved in the original draft preparation, review and editing. AB directed the work and was responsible for
1365 much of the introductory, recommendations and summary material. AO was the main author responsible for Section 2 and 3,
1366 with IBG, GE and RD. GB, AC, JIC, RD, CSF, DI, CNN, GP, MR, GS, BS, DW contributed with all their expertise to Section
1367 4. All the authors contributed to Sections 5 and 6. Much material was shared or moved between sections and editing
1368 responsibilities were comprehensive, so Sect. authorship is never exclusive.

1370 **References**

- 1371 Abbott, I. H. and Von Doenhoff, A. E.: Theory of wing sections: including a summary of airfoil data, Dover Publ, New York,
1372 NY, 691 pp., 2010.
- 1373 Aeolus4Future: Efficient Harvesting of the Wind Energy, Marie Skłodowska-Curie grant agreement No. 643167,
1374 <https://cordis.europa.eu/article/id/386860-a-breath-of-fresh-air-for-wind-energy>, last access 17/08/2022
- 1375 Akwa, J. V., Vielmo, H. A., and Petry, A. P.: A review on the performance of Savonius wind turbines, Renewable and
1376 Sustainable Energy Reviews, 16, 3054–3064, <https://doi.org/10.1016/j.rser.2012.02.056>, 2012.
- 1377 Allen, M.: Gauging public opinion on small wind turbines, 2016. [https://www.youris.com/energy/renewables/gauging-public-](https://www.youris.com/energy/renewables/gauging-public-opinion-on-small-wind-turbines.kl)
1378 [opinion-on-small-wind-turbines.kl](https://www.youris.com/energy/renewables/gauging-public-opinion-on-small-wind-turbines.kl), last access 17/08/2022
- 1379 Anon: A Siting Specialist. Capacity Factors - Performance over time, 2015.
- 1380 Arredondo-Galeana, A. and Brennan, F.: Floating Offshore Vertical Axis Wind Turbines: Opportunities, Challenges and Way
1381 Forward, Energies, 14, 8000, <https://doi.org/10.3390/en14238000>, 2021.
- 1382 Aslam Bhutta, M. M., Hayat, N., Farooq, A. U., Ali, Z., Jamil, Sh. R., and Hussain, Z.: Vertical axis wind turbine - A review
1383 of various configurations and design techniques, 16, 1926–1939, <https://doi.org/10.1016/j.rser.2011.12.004>, 2012.
- 1384 Baker, T. L.: A field guide to American windmills, 1st ed., University of Oklahoma Press, Norman, 516 pp., 1985.
- 1385 Balduzzi, F., Bianchini, A., and Ferrari, L.: Microeolic turbines in the built environment: Influence of the installation site on
1386 the potential energy yield, 45, 163–174, <https://doi.org/10.1016/j.renene.2012.02.022>, 2012.
- 1387 Balduzzi, F., Zini, M., Molina, A. C., Bartoli, G., De Troyer, T., Runacres, M. C., Ferrara, G., and Bianchini, A.: Understanding
1388 the aerodynamic behavior and energy conversion capability of small darrieus vertical axis wind turbines in turbulent flows,
1389 13, <https://doi.org/10.3390/en13112936>, 2020.
- 1390 Bangga, G., Lutz, T., and Krämer, E.: Root flow characteristics and 3D effects of an isolated wind turbine rotor, J Mech Sci
1391 Technol, 31, 3839–3844, <https://doi.org/10.1007/s12206-017-0728-6>, 2017.
- 1392 Barbose, G. and Darghouth, N.: Tracking the Sun VIII, The Installed Price of Residential and Non-Residential Photovoltaic
1393 Systems in the United States, 2015. https://emp.lbl.gov/sites/all/files/lbnl-188238_2.pdf, last access 17/08/2022
- 1394 Battisti, L.: Wind Energy Exploitation in Urban Environment, 2018th ed., Springer International Publishing, 2018.
- 1395 Bergey Wind Power, 2022, <http://www.bergey.com/>, last access 17/08/2022
- 1396 Bianchini, A.: Trends, Prospects, and R&D Directions in Wind Turbine Technology☆, in: Reference Module in Earth Systems
1397 and Environmental Sciences, Elsevier, <https://doi.org/10.1016/B978-0-12-409548-9.11864-0>, 2019.
- 1398 Bianchini, A., Ferrara, G., Ferrari, L., and Magnani, S.: An improved model for the performance estimation of an H-Darrieus
1399 wind turbine in skewed flow, 36, 667–686, <https://doi.org/10.1260/0309-524X.36.6.667>, 2012.

- 1400 Bianchini, A., Ferrara, G., and Ferrari, L.: Design guidelines for H-Darrieus wind turbines: Optimization of the annual energy
1401 yield, 89, 690–707, <https://doi.org/10.1016/j.enconman.2014.10.038>, 2015a.
- 1402 Bianchini, A., Balduzzi, F., Rainbird, J. M., Peiró, J., Graham, J. M. R., Ferrara, G., and Ferrari, L.: On the influence of virtual
1403 camber effect on airfoil polars for use in simulations of Darrieus wind turbines, 106, 373–384,
1404 <https://doi.org/10.1016/j.enconman.2015.09.053>, 2015b.
- 1405 Bianchini, A., Balduzzi, F., Ferrara, G., and Ferrari, L.: Virtual incidence effect on rotating airfoils in Darrieus wind turbines,
1406 111, 329–338, <https://doi.org/10.1016/j.enconman.2015.12.056>, 2016.
- 1407 Bianchini, A., Balduzzi, F., Ferrara, G., Persico, G., Dossena, V., and Ferrari, L.: A critical analysis on low-order simulation
1408 models for darrieus vawts: How much do they pertain to the real flow?, 141, <https://doi.org/10.1115/1.4040851>, 2019.
- 1409 Boccard, N.: Capacity factor of wind power realized values vs. estimates, *Energy Policy*, 37, 2679–2688,
1410 <https://doi.org/10.1016/j.enpol.2009.02.046>, 2009.
- 1411 Bontempo, R. and Manna, M.: Diffuser augmented wind turbines: Review and assessment of theoretical models, *Applied*
1412 *Energy*, 280, 115867, <https://doi.org/10.1016/j.apenergy.2020.115867>, 2020.
- 1413 Bortolini, M., Gamberi, M., Graziani, A., Manzini, R., and Pilati, F.: Performance and viability analysis of small wind turbines
1414 in the European Union, *Renewable Energy*, 62, 629–639, <https://doi.org/10.1016/j.renene.2013.08.004>, 2014.
- 1415 Bortolotti, P., Ivanov, H., Johnson, N., Barter, G. E., Veers, P., and Namura, N.: Challenges, opportunities, and a research
1416 roadmap for downwind wind turbines, *Wind Energy*, we.2676, <https://doi.org/10.1002/we.2676>, 2021.
- 1417 Bottasso, C. L., Croce, A., Savini, B., Sirchi, W., and Trainelli, L.: Aero-servo-elastic modeling and control of wind turbines
1418 using finite-element multibody procedures, *Multibody Syst Dyn*, 16, 291–308, <https://doi.org/10.1007/s11044-006-9027-1>,
1419 2006.
- 1420 Bradney, D., Evans, S., and Clausen, P.: The Effect of Tail Fin Size on the Yaw Performance of Small Wind Turbines
1421 Operating in Unsteady Flow, in: *Wind Energy Exploitation in Urban Environment*, Cham, 55–70, https://doi.org/10.1007/978-3-030-13531-7_4, 2019.
- 1423 Bryne, R.: SWT energy performance at consumer sites: Post installation experiences from a field trial in Ireland, *Austrian*
1424 *Small Wind Conference*, Wien, 2017.
- 1425 Bukala, J., Damaziak, K., Kroszczynski, K., Malachowski, J., Szafranski, T., Tomaszewski, M., Karimi, H. R., Jozwik, K.,
1426 Karczewski, M., and Sobczak, K.: Small Wind Turbines: Specification, Design, and Economic Evaluation, in: *Wind Turbines*
1427 *- Design, Control and Applications*, edited by: Aissaoui, A. G. and Tahour, A., InTech, <https://doi.org/10.5772/62821>, 2016.
- 1428 Bychkov, N. M., Dovgal, A. V., and Kozlov, V. V.: Magnus wind turbines as an alternative to the blade ones, *J. Phys.: Conf.*
1429 *Ser.*, 75, 012004, <https://doi.org/10.1088/1742-6596/75/1/012004>, 2007.
- 1430 Carter Wind Energy, 2022, <https://carterwind.com/>, last access 17/08/2022
- 1431 Chagas, C. C. M., Pereira, M. G., Rosa, L. P., da Silva, N. F., Freitas, M. A. V., and Hunt, J. D.: From Megawatts to Kilowatts:
1432 A Review of Small Wind Turbine Applications, *Lessons From The US to Brazil*, 12, 2760,
1433 <https://doi.org/10.3390/su12072760>, 2020.
- 1434 Clausen, P., Whale, J., and Wood, D.: *Small wind and hydrokinetic turbines*, ISBN 978-1-83953-072-2, 2021.

- 1435 Damiani, R., Davis, D.: Engineering a Reduction of the Levelized Cost of Energy of Distributed Wind Turbines via Rotor and
1436 Control Enhancements, *J. Phys.: Conf. Ser.* 2265 042080.
- 1437 Damiani, R., Davis, D., and Summerville, B.: Challenges and Possible Solutions in Aeroelastic Modeling for the Distributed
1438 Wind Turbine Industry, *J. Phys.: Conf. Ser.* 2265 042075.
- 1439 Damota, J., Lamas, I., Couce, A., and Rodríguez, J.: Vertical Axis Wind Turbines: Current Technologies and Future Trends,
1440 *REPQJ*, 530–535, <https://doi.org/10.24084/repqj13.389>, 2015.
- 1441 Dayan, E.: Wind energy in buildings. Power generation from wind in the urban environment - where it is needed most, 7, 33-
1442 34,36,38, [https://doi.org/10.1016/S1471-0846\(06\)70545-5](https://doi.org/10.1016/S1471-0846(06)70545-5), 2006.
- 1443 Dentons: Italy: The 2019-2020 incentives regime for renewable energy plants, 2020. [https://www.dentons.com/en/pdf-pages/-](https://www.dentons.com/en/pdf-pages/-/media/fcaeaba3d7424b2da0b0110ec08f6b06.ashx)
1444 [/media/fcaeaba3d7424b2da0b0110ec08f6b06.ashx](https://www.dentons.com/en/pdf-pages/-/media/fcaeaba3d7424b2da0b0110ec08f6b06.ashx), last access 17/08/2022
- 1445 Drew, D. R., Barlow, J. F., Cockerill, T. T., and Vahdati, M. M.: The importance of accurate wind resource assessment for
1446 evaluating the economic viability of small wind turbines, *Renewable Energy*, 77, 493–500,
1447 <https://doi.org/10.1016/j.renene.2014.12.032>, 2015
- 1448 Duchaud, J.-L., Notton, G., Fouilloy, A., and Voyant, C.: Hybrid renewable power plant sizing – Graphical decision tool,
1449 sensitivity analysis and applications in Ajaccio and Tilos, *Applied Energy*, 254, 113601,
1450 <https://doi.org/10.1016/j.apenergy.2019.113601>, 2019.
- 1451 Duo, C.: China Medium/Small Wind Industry, Austrian Small Wind Conference, Wien, 2017.
- 1452 Duplyakin, D., Zisman, S., Phillips, C., and Tinnesand, H.: Bias Characterization, Vertical Interpolation, and Horizontal
1453 Interpolation for Distributed Wind Siting Using Mesoscale Wind Resource Estimates, 2021.
- 1454 DWEA: Smart Wind Roadmap: A Consensus-Based, Shared Vision for the Sustainable Manufacturing, Advanced Research
1455 & Technology Action Plan for Distributed Wind, 2016.
- 1456 EAWC: Small Wind Turbine Technical Committee, 2020. <https://www.eawc.eu/organisation/committees/>, last access
1457 17/08/2022
- 1458 Elliott, D. and Infield, D.: An assessment of the impact of reduced averaging time on small wind turbine power curves, energy
1459 capture predictions and turbulence intensity measurements: Impact of reduced averaging time on small wind turbine
1460 performance, *Wind Energ.*, 17, 337–342, <https://doi.org/10.1002/we.1579>, 2014.
- 1461 Ellis, G. and Ferraro, G.: The social acceptance of wind energy, JRC Science for Policy Report, 2016.
- 1462 Emblin, D.: Small wind turbines: the art of disguise, 2017. [https://www.youris.com/Energy/Renewables/Small-Wind-](https://www.youris.com/Energy/Renewables/Small-Wind-Turbines-The-Art-Of-Disguise.kl)
1463 [Turbines-The-Art-Of-Disguise.kl](https://www.youris.com/Energy/Renewables/Small-Wind-Turbines-The-Art-Of-Disguise.kl), last access 17/08/2022
- 1464 Eunice Energy Group: EW16 Thetis, 2021. <https://eunice-group.com/projects/ew16-thetis/>, last access 17/08/2022
- 1465 European Court of Auditors: Electricity production from wind and solar photovoltaic power in the EU, 2018.
- 1466 Evans, S., Dana, S., Clausen, P., and Wood, D.: A simple method for modelling fatigue spectra of small wind turbine blades,
1467 *Wind Energy*, 24, 549–557, <https://doi.org/10.1002/we.2588>, 2021.

- 1468 Evans, S. P., Bradney, D. R., and Clausen, P. D.: Assessing the IEC simplified fatigue load equations for small wind turbine
1469 blades: How simple is too simple?, *Renewable Energy*, 127, 24–31, <https://doi.org/10.1016/j.renene.2018.04.041>, 2018.
- 1470 Evans, S. P., Kesby, J. E., Bradley, J., and Clausen, P. D.: Commercialization of a Diffuser Augmented Wind Turbine for
1471 Distributed Generation, *J. Phys.: Conf. Ser.*, 1452, 012014, <https://doi.org/10.1088/1742-6596/1452/1/012014>, 2020.
- 1472 Feldman, D., Ramasamy, V., Fu, R., Ramdas, A., Desai, J., and Margolis, R.: U.S. Solar Photovoltaic System Cost Benchmark:
1473 Q1 2020, 2021.
- 1474 Fields, M. J., Tinnesand, H., and Baring-Gould, E. A.: *Distributed Wind Resource Assessment: State of the Industry*, 2016.
- 1475 Forsyth, T., Jimenez, T., Preus, R., Tegen, S., and Baring-Gould, I.: *The Distributed Wind Cost Taxonomy*, 2017.
- 1476 Forsyth, T., Van Dam, J., and Preus, R.: *Summary of the International Standards Assessment Forum (ISAF) 2019*, 2019.
- 1477 Gabra, S., Miles, J., and Scott, S. A.: Techno-economic analysis of stand-alone wind micro-grids, compared with PV and diesel
1478 in Africa, *Renewable Energy*, 143, 1928–1938, <https://doi.org/10.1016/j.renene.2019.05.119>, 2019.
- 1479 Gigue`re, P. and Selig, M. S.: New Airfoils for Small Horizontal Axis Wind Turbines, 120, 108–114,
1480 <https://doi.org/10.1115/1.2888052>, 1998.
- 1481 Global Info Research: *Global Small wind Market 2020 by Manufacturers, Regions, Type and Application, Forecast top 2025*,
1482 2021.
- 1483 Greek Government Gazette: FEK 3150/B/30-7-2020, 2021.
- 1484 GWEC: *Global Wind Report 2020*, GWEC, 2020.
- 1485 Hellenic Electricity Distribution Network Operator S.A., 2021. [https://deddie.gr/en/themata-stathmon-ape-sithia/fv-apo-
1486 autoparagwous-me-eikoniko-energeiako-sumps/](https://deddie.gr/en/themata-stathmon-ape-sithia/fv-apo-autoparagwous-me-eikoniko-energeiako-sumps/), last access 17/08/2022
- 1487 Hemeida, A. M., Omer, A. S., Bahaa-Eldin, A. M., Alkhalaf, S., Ahmed, M., Senjyu, T., and El-Saady, G.: Multi-objective
1488 multi-verse optimization of renewable energy sources-based micro-grid system: Real case, *Ain Shams Engineering Journal*,
1489 13, 101543, <https://doi.org/10.1016/j.asej.2021.06.028>, 2022.
- 1490 Hills, R. G., Maniaci, D. C., and Naughton, J. W.: V&v framework, SAND2015-7455, 2015.
1491 <https://www.osti.gov/biblio/1214246-framework>, last access 17/08/2022
- 1492 Holst, D., Pechlivanoglou, G., Kohlrausch, C. T., Nayeri, C. N., and Paschereit, C. O.: sHAWT Design: Airfoil Aerodynamics
1493 Under the Influence of Roughness, *ASME Turbo Expo 2016: Turbomachinery Technical Conference and Exposition*,
1494 <https://doi.org/10.1115/GT2016-56377>, 2016.
- 1495 Holst, D., Pechlivanoglou, G., Wegner, F., Nayeri, C. N., and Paschereit, C. O.: Potential of Retrofit Passive Flow Control for
1496 Small Horizontal Axis Wind Turbines, 139, 032604, <https://doi.org/10.1115/1.4034543>, 2017.
- 1497 IEA: IEA WIND 2013 Annual Report, 2014.
1498 https://nachhaltigwirtschaften.at/resources/iea_pdf/reports/iea_wind_annual_report_2013.pdf, last access 17/08/2022
- 1499 IEA: *Renewables 2019*, 2019. <https://www.iea.org/reports/renewables-2019>, last access 17/08/2022

- 1500 IEA: Solar PV net capacity additions by application segment, 2017-2022, 2020. [https://www.iea.org/data-and-](https://www.iea.org/data-and-statistics/charts/solar-pv-net-capacity-additions-by-application-segment-2017-2022)
1501 [statistics/charts/solar-pv-net-capacity-additions-by-application-segment-2017-2022](https://www.iea.org/data-and-statistics/charts/solar-pv-net-capacity-additions-by-application-segment-2017-2022), last access 17/08/2022
- 1502 IEC: International Standard: 61400-1 Wind turbines – Part 1: Design Requirements, 2019a.
- 1503 IEC: International Standard: 61400-2 Wind turbines – Part 2: Design requirements for small wind turbines, 2019b.
- 1504 Kaldellis, J. K. and Zafirakis, D. P.: Trends, Prospects, and R&D Directions in Wind Turbine Technology, in: Comprehensive
1505 Renewable Energy, Elsevier, 671–724, <https://doi.org/10.1016/B978-0-08-087872-0.00224-9>, 2012.
- 1506 Karekezi, S.: Renewables in Africa—meeting the energy needs of the poor, Energy Policy, 30, 1059–1069,
1507 [https://doi.org/10.1016/S0301-4215\(02\)00058-7](https://doi.org/10.1016/S0301-4215(02)00058-7), 2002.
- 1508 Khan, M., Alavi, M., Mohan, N., Azeez, A., Shanif, A., and Javed, B.: Wind Turbine design and fabrication to power street
1509 lights, MATEC Web Conf., 108, 08010, <https://doi.org/10.1051/mateconf/201710808010>, 2017.
- 1510 Kim, S.: Country Report: Small Wind in Korea, 2018.
- 1511 Lo, K.: Renewable Energy: Are feed-in tariffs going out of style?, Power Technology, April, 2018. [https://www.power-](https://www.power-technology.com/features/featurerenewable-energy-are-feed-in-tariffs-going-out-ofstyle-5718419/)
1512 [technology.com/features/featurerenewable-energy-are-feed-in-tariffs-going-out-ofstyle-5718419/](https://www.power-technology.com/features/featurerenewable-energy-are-feed-in-tariffs-going-out-ofstyle-5718419/), last access 17/08/2022
- 1513 McMahon, N. M., Burton, P. R., and Sharman, D. M.: On Electrodynamic Braking for Small Wind Turbines, Wind
1514 Engineering, 39, 549–555, <https://doi.org/10.1260/0309-524X.39.5.549>, 2015.
- 1515 Meghana, A., Smitha, B., and Jagwani, S.: Technological Advances in Airborne Wind Power: A Review, in: Emerging
1516 Research in Computing, Information, Communication and Applications, vol. 790, edited by: Shetty, N. R., Patnaik, L. M.,
1517 Nagaraj, H. C., Hamsavath, P. N., and Nalini, N., Springer Singapore, Singapore, 349–359, [https://doi.org/10.1007/978-981-](https://doi.org/10.1007/978-981-16-1342-5_28)
1518 [16-1342-5_28](https://doi.org/10.1007/978-981-16-1342-5_28), 2022.
- 1519 Mertens, S.: The energy yield of roof mounted wind turbines, 27, 507–518, <https://doi.org/10.1260/030952403773617472>,
1520 2003.
- 1521 Micallef, D. and van Bussel, G.: A Review of Urban Wind Energy Research: Aerodynamics and Other Challenges, Energies,
1522 11, 2204, <https://doi.org/10.3390/en11092204>, 2018.
- 1523 Möllerström, E., Ottermo, F., Hylander, J., and Bernhoff, H.: Noise Emission of a 200 kW Vertical Axis Wind Turbine, 9, 19,
1524 <https://doi.org/10.3390/en9010019>, 2016.
- 1525 NREL: Competitiveness Improvement Project, 2022. <https://www.nrel.gov/wind/competitiveness-improvement-project.html>,
1526 last access 17/08/2022
- 1527 NREL, OpenFAST: <https://github.com/OpenFAST>, last access: 31 October 2019.
- 1528 Ning, A., Hayman, G., Damiani, R., and Jonkman, J. M.: Development and Validation of a New Blade Element Momentum
1529 Skewed-Wake Model within AeroDyn, in: 33rd Wind Energy Symposium, American Institute of Aeronautics and
1530 Astronautics, <https://doi.org/10.2514/6.2015-0215>, 2015.
- 1531 Nordic Folkecenter for Renewable Energy: Folkecenter’s Catalogue of small wind turbines - 8th Edition, 2016.
- 1532 Ofgem: Environmental programmes, 2021. <https://www.ofgem.gov.uk/environmental-programmes>, last access 17/08/2022

- 1533 Ohya, Y., Karasudani, T., Sakurai, A., Abe, K., and Inoue, M.: Development of a shrouded wind turbine with a flanged diffuser,
1534 *Journal of Wind Engineering and Industrial Aerodynamics*, 96, 524–539, <https://doi.org/10.1016/j.jweia.2008.01.006>, 2008.
- 1535 Orrell, A. C. and Poehlman, E. A.: Benchmarking U.S. Small Wind Costs with the Distributed Wind Taxonomy, Pacific
1536 Northwest National Lab. (PNNL), Richland, WA (United States), <https://doi.org/10.2172/1400355>, 2017.
- 1537 Orrell, A. C., Preziuso, D., Morris, D., and Homer, J.: 2019 Distributed Wind Data Summary, PNNL-30168, 2020.
1538 <https://www.pnnl.gov/sites/default/files/media/file/2019%20Distributed%20Wind%20Data%20Summary-10Aug20.pdf>, last
1539 access 17/08/2022
- 1540 Orrell, A. C., Kazimierczuk, K., and Sheridan, L.: Distributed Wind Market Report: 2021 Edition, DOE/GO-102021-5620,
1541 2021. <https://www.energy.gov/eere/wind/articles/distributed-wind-market-report-2021-edition-released>, last
1542 access 17/08/2022
- 1543 Papi, F., Pagamonci, L. and Bianchini, A.: Design Loads in Small Wind Turbines: a Detailed Comparison Between Pitch and
1544 Stall Regulation, IOP Conference Proceedings, ATI2022 Conference, paper in publishing, 2022.
- 1545 Papi, F., Nocentini, A., Ferrara, G., and Bianchini, A.: On the Use of Modern Engineering Codes for Designing a Small Wind
1546 Turbine: An Annotated Case Study, 14, 1013, <https://doi.org/10.3390/en14041013>, 2021.
- 1547 Paulsen, U. S., Madsen, H. A., Hattel, J. H., Baran, I., and Nielsen, P. H.: Design Optimization of a 5 MW Floating Offshore
1548 Vertical-axis Wind Turbine, *Energy Procedia*, 35, 22–32, <https://doi.org/10.1016/j.egypro.2013.07.155>, 2013.
- 1549 Pillai, U.: Drivers of cost reduction in solar photovoltaics, *Energy Economics*, 50, 286–293,
1550 <https://doi.org/10.1016/j.eneco.2015.05.015>, 2015.
- 1551 Pourrajabian, A., Mirzaei, M., Ebrahimi, R., and Wood, D.: Effect of air density on the performance of a small wind turbine
1552 blade: A case study in Iran, *Journal of Wind Engineering and Industrial Aerodynamics*, 126, 1–10,
1553 <https://doi.org/10.1016/j.jweia.2014.01.001>, 2014.
- 1554 Predescu, M.: Economic evaluation of small wind turbines and hybrid systems for residential use, *Renew. Energy Environ.*
1555 *Sustain.*, 1, 33, <https://doi.org/10.1051/rees/2016023>, 2016.
- 1556 Preus, R., Reilly, J., Johnson, J., Baring-Gould, I., and Coddington, M.: Distributed Wind Considerations from the IEEE 1547-
1557 2018 Revision, 2021. <https://www.nrel.gov/docs/fy21osti/78948.pdf>, last access 17/08/2022
- 1558 Reiman, A. P., Homer, J. S., Bhattarai, B., and Orrell, A. C.: Quantifying Technical Diversity Benefits of Wind as a Distributed
1559 Energy Resource, in: 2020 IEEE Power & Energy Society Innovative Smart Grid Technologies Conference (ISGT), 2020
1560 IEEE Power & Energy Society Innovative Smart Grid Technologies Conference (ISGT), Washington, DC, USA, 1–5,
1561 <https://doi.org/10.1109/ISGT45199.2020.9087665>, 2020.
- 1562 Roth, M., Eiter, S., Röhner, S., Kruse, A., Schmitz, S., Frantál, B., Centeri, C., Frolova, M., Buchecker, M., Stober, D., Karan,
1563 I., and Van der Horst, D. (Eds.): Renewable energy and landscape quality, Jovis, Berlin, 295 pp., 2018.
- 1564 Schepers, J. G. and Schreck, S. J.: Aerodynamic measurements on wind turbines, *WIREs Energy Environ.*, 8,
1565 <https://doi.org/10.1002/wene.320>, 2019.
- 1566 Schepers, J. G., Boorsma, K., Madsen, H. A., Pirrung, G. R., Bangga, G., Guma, G., Lutz, T., Potentier, T., Braud, C.,
1567 Guilmineau, E., Croce, A., Cacciola, S., Schaffarczyk, A. P., Lobo, B. A., Ivanell, S., Asmuth, H., Bertagnolio, F., Sørensen,
1568 N. N., Shen, W. Z., Grinderslev, C., Forsting, A. M., Blondel, F., Bozonnet, P., Boisard, R., Yassin, K., Hoening, L.,

- 1569 Stoevesandt, B., Imiela, M., Greco, L., Testa, C., Magionesi, F., Vijayakumar, G., Ananthan, S., Sprague, M. A., Branlard, E.,
 1570 Jonkman, J., Carrion, M., Parkinson, S., and Cicirello, E.: IEA Wind TCP Task 29, Phase IV: Detailed Aerodynamics of Wind
 1571 Turbines, Zenodo, <https://doi.org/10.5281/zenodo.4813068>, 2021.
- 1572 SD Wind Energy, 2022, <https://sd-windenergy.com/>, last access 17/08/2022
- 1573 Sedaghat, A.: Magnus type wind turbines: Prospectus and challenges in design and modelling, *Renewable Energy*, 62, 619–
 1574 628, <https://doi.org/10.1016/j.renene.2013.08.029>, 2014.
- 1575 Selig, M. S.: Low Reynolds Number Airfoil Design - Lecture Notes, 2003. [https://m-selig.ae.illinois.edu/pubs/Selig-2003-](https://m-selig.ae.illinois.edu/pubs/Selig-2003-VKI-LRN-Airfoil-Design-Lecture-Series.pdf)
 1576 [VKI-LRN-Airfoil-Design-Lecture-Series.pdf](https://m-selig.ae.illinois.edu/pubs/Selig-2003-VKI-LRN-Airfoil-Design-Lecture-Series.pdf), last access 17/08/2022
- 1577 Senthilvel, G., Vivekanandan, M., Nawas Shareef, H., and Sivabalamurugan, V.: Renewable Energy in Rural Areas using
 1578 Savonius Wind Turbine, 3, 1–6, <https://doi.org/10.5281/zenodo.3903587>, 2020.
- 1579 Sessarego, M. and Wood, D.: Multi-dimensional optimization of small wind turbine blades, *Renewables*, 2, 9,
 1580 <https://doi.org/10.1186/s40807-015-0009-x>, 2015.
- 1581 Sheridan, L. M., Phillips, C., Orrell, A. C., Berg, L. K., Tinnesand, H., Rai, R. K., Zisman, S., Duplyakin, D., and Flaherty, J.
 1582 E.: Validation of wind resource and energy production simulations for small wind turbines in the United States, *Wind Energ.*
 1583 *Sci.*, 7, 659–676, <https://doi.org/10.5194/wes-7-659-2022>, 2022.
- 1584 Shimizu, A, 敦史: Vertical axis type magnus wind turbine generator, 2013.
- 1585 Simic, Z., Havelka, J. G., and Bozicevic Vrhovcak, M.: Small wind turbines – A unique segment of the wind power market,
 1586 *Renewable Energy*, 50, 1027–1036, <https://doi.org/10.1016/j.renene.2012.08.038>, 2013.
- 1587 Sheridan, L. M., Phillips, C., Orrell, A. C., Berg, L. K., Tinnesand, H., Rai, R. K., Zisman, S., Duplyakin, D., and Flaherty, J.
 1588 E.: Validation of wind resource and energy production simulations for small wind turbines in the United States, *Wind Energ.*
 1589 *Sci.*, 7, 659–676, <https://doi.org/10.5194/wes-7-659-2022>, 2022.
- 1590 Stathopoulos, T., Alrawashdeh, H., Al-Quraan, A., Blocken, B., Dilimulati, A., Paraschivoiu, M., and Pilay, P.: Urban wind
 1591 energy: Some views on potential and challenges, *Journal of Wind Engineering and Industrial Aerodynamics*, 179, 146–157,
 1592 <https://doi.org/10.1016/j.jweia.2018.05.018>, 2018.
- 1593 Summerville, B., Van Dam, J., Preus, R., Baring-Gould, I., Forsyth, T., and Bergey, M.: Justification for Updates to ANSI/ACP
 1594 Small Wind Turbine Standard, NREL/TP-5000-79775, 2021. <https://www.nrel.gov/docs/fy21osti/79775.pdf>, last access
 1595 17/08/2022
- 1596 SWIP Project: European SWIP Project: small wind energy in cities, *FuturEnergy*, 2014. [http://swipproject.eu/wp-](http://swipproject.eu/wp-content/uploads/2015/04/FuturEnergy-Magazine_SWIP.pdf)
 1597 [content/uploads/2015/04/FuturEnergy-Magazine_SWIP.pdf](http://swipproject.eu/wp-content/uploads/2015/04/FuturEnergy-Magazine_SWIP.pdf), last access 17/08/2022
- 1598 Tatchley, C., Paton, H., Robertson, E., Minderman, J., Hanley, N., and Park, K.: Drivers of Public Attitudes towards Small
 1599 Wind Turbines in the UK, *PLoS ONE*, 11, e0152033, <https://doi.org/10.1371/journal.pone.0152033>, 2016.
- 1600 Timmer, W. A. and van Rooij, R. P. J. O. M.: Summary of the Delft University Wind Turbine Dedicated Airfoils, 125, 488–
 1601 496, <https://doi.org/10.1115/1.1626129>, 2003.

- 1602 Tinnesand, H. and Sethuraman, L.: Distributed Wind Resource Assessment Framework: Functional Requirements and Metrics
 1603 for Performance and Reliability Modeling, NREL/TP-5000-72523, 2019. <https://www.nrel.gov/docs/fy19osti/72523.pdf>, last
 1604 access 17/08/2022
- 1605 Toja-Silva, F., Colmenar-Santos, A., and Castro-Gil, M.: Urban wind energy exploitation systems: Behaviour under
 1606 multidirectional flow conditions - Opportunities and challenges, 24, 364–378, <https://doi.org/10.1016/j.rser.2013.03.052>,
 1607 2013.
- 1608 Tordeur, P.: Monitoring and control of a small wind turbine, MSc Thesis, Vrije Universiteit Brussel, 2018.
- 1609 Tozzi Nord, 2022. <https://www.tozzinord.com/en/categoria-prodotto/wind-turbines>, last access 17/08/2022
- 1610 US DOE WindExchange: Community Wind Energy, 2022. <https://windexchange.energy.gov/markets/community>, last access
 1611 17/08/2022
- 1612 Visser, K. D.: Real-world development challenges of the Clarkson University 3 meter ducted wind turbine, J. Phys.: Conf.
 1613 Ser., 2265, 042072, <https://doi.org/10.1088/1742-6596/2265/4/042072>, 2022. Tzen, E.: Small wind turbines for on grid and off
 1614 grid applications, IOP Conf. Ser.: Earth Environ. Sci., 410, 012047, <https://doi.org/10.1088/1755-1315/410/1/012047>, 2020.
- 1615 Van Treuren, K. W.: Small-Scale Wind Turbine Testing in Wind Tunnels Under Low Reynolds Number Conditions, 137,
 1616 051208, <https://doi.org/10.1115/1.4030617>, 2015.
- 1617 Vaz, J. R. P., Wood, D. H., Bhattacharjee, D., and Lins, E. F.: Drivetrain resistance and starting performance of a small wind
 1618 turbine, Renewable Energy, 117, 509–519, <https://doi.org/10.1016/j.renene.2017.10.071>, 2018.
- 1619 Veers, P., Dykes, K., Lantz, E., Barth, S., Bottasso, C. L., Carlson, O., Clifton, A., Green, J., Green, P., Holttinen, H., Laird,
 1620 D., Lehtomäki, V., Lundquist, J. K., Manwell, J., Marquis, M., Meneveau, C., Moriarty, P., Munduate, X., Muskulus, M.,
 1621 Naughton, J., Pao, L., Paquette, J., Peinke, J., Robertson, A., Rodrigo, J. S., Sempreviva, A. M., Smith, J. C., Tuohy, A., and
 1622 Wisser, R.: Grand challenges in the science of wind energy, <https://doi.org/10.1126/science.aau2027>, 2019.
- 1623 Wang, U.: Why corporations like Microsoft are investing in renewable energy, 2013.
 1624 <https://www.theguardian.com/sustainable-business/microsoft-walmart-google-renewable-energy-wind-farm-solar>, last access
 1625 17/08/2022
- 1626 Wen, T. W., Palanichamy, C., and Ramasamy, G.: Small Wind Turbines as Partial Solution for Energy Sustainability of
 1627 Malaysia, 9, 257–266, 2019.
- 1628 Wilson, S. V. R., Clausen, P. D., and Wood, D. H.: Gyroscopic moments on small wind turbine blades at high yaw rates,
 1629 Australian Journal of Mechanical Engineering, 5, 1–8, <https://doi.org/10.1080/14484846.2008.11464529>, 2008.
- 1630 WINEUR project: Publishable Result-Oriented Report – WINEUR Wind Energy Integration in the Urban Environment Grant
 1631 agreement no. EIE/04/130/S07.38591, 2005.
- 1632 Wolsink, M.: Wind Power wind power : Basic Challenge Concerning Social Acceptance wind power social acceptance, in:
 1633 Renewable Energy Systems, edited by: Kaltschmitt, M., Themelis, N. J., Bronicki, L. Y., Söder, L., and Vega, L. A., Springer
 1634 New York, New York, NY, 1785–1821, https://doi.org/10.1007/978-1-4614-5820-3_88, 2013.
- 1635 Wood, D.: Small wind turbines, Springer, ISBN: 978-1-84996-175-2, 2011.

- 1636 Wright, A. K. and Wood, D. H.: Yaw Rate, Rotor Speed and Gyroscopic Loads on a Small Horizontal Axis Wind Turbine,
1637 Wind Engineering, 31, 197–209, <https://doi.org/10.1260/030952407781998837>, 2007.
- 1638 XZERES Wind Turbines, 2022, <https://it.wind-turbine-models.com/manufacturers/533-xzeres-wind>, last access 17/08/2022