Tropical cyclone low-level wind speed, shear, and veer: sensitivity to the boundary layer parameterization in WRF

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Abstract. Mesoscale modeling can be used to analyze key parameters for wind turbine load assessment in a large variety of tropical cyclones. However, the modeled wind structure of tropical cyclones is known to be sensitive to the boundary layer scheme. We analyze modeled wind speed, shear, and wind veer across a wind turbine rotor plane in the eyewall and ~~rainband region~~outer cyclone. We further assess the sensitivity of wind speed, shear, and veer to the boundary layer parameterization. Three model realizations of typhoon Megi over the open ocean using three frequently used boundary layer schemes in the Weather Research and Forecasting model are analyzed. All three typhoon simulations reasonably reproduce the cyclone track and structure. The boundary layer parametrization causes up to ~~21~~15 % differences in median ~~hub height~~ wind speed at hub height between the simulations. The simulated wind speed variability ~~is further dependent~~also depends on the boundary layer scheme. The modeled median wind shear is smaller or equal to 0.11 used in the current IEC standard regardless of the boundary layer scheme for the eyewall and ~~rainband region.~~outer cyclone region. However, up to 43.6 % of the simulated wind profiles in the eyewall region exceed 0.11. While the surface inflow angle is sensitive to the boundary layer ~~simulation~~scheme, wind veer in the lowest $400\,\mathrm{m}$ of the atmospheric boundary layer is less affected by the boundary layer ~~parametrization. Simulated~~ scheme. Simulated median wind veer reaches values up to ~~(~~$1.7 \times 10^{-2\,\circ}\mathrm{m}^{-1}$ ($1.2 \times 10^{-2\,\circ}\mathrm{m}^{-1}$) in the eyewall region (~~rainband~~outer cyclone region) and is relatively small compared to moderate wind speed regimes. On average, simulated wind speed shear and wind veer are highest in the eyewall region. Yet strong spatial organization of wind shear and veer along the rainbands may increase wind turbine loads, due to rapid ~~coherent wind profile changes~~changes in the wind profile at the turbine location.

1 Introduction

~~Research~~ Offshore wind power has over the past decades ~~made offshore wind power~~ become accessible for a wide region around the tropical and subtropical West Pacific. This region includes areas with large wind resources but it is frequently hit by tropical cyclones. For wind turbines in this region, tropical cyclones form the most extreme wind conditions~~. Therefore~~, and therefore, the tropical cyclone wind field is a challenge for wind turbine design standards. Over the past decade turbine failures have been caused during different typhoons, such as Usagi, Rammasun, and Maria (Li et al., 2022). Tropical cyclones can cause fatigue failure of ~~a wind turbine (Chen et al., 2022)~~wind turbines (Chen et al., 2015; Chen and Xu, 2016; Chen, 2022).

25 Further research incorporating mesoscale and microscale numerical models into aeroelastic wind turbine models is necessary to achieve reliable structural analysis of wind turbines in tropical cyclone conditions (Li et al., 2022).

~~The wind input for aeroelastic wind turbine models consists of a~~ To ensure the structural integrity of wind turbines, turbine design standards are defined in the International Electrotechnical Commission's standard (IEC) for onshore and offshore turbines (IEC, 2019a, b). The standards are based on site-specific wind speed classes and turbulence classes. The ability of

30 wind turbines to withstand wind conditions within the turbine class is tested in design load cases (DLC). Different DLCs assess the loads acting on wind turbines during power production, and at stand-still. In and close to the eyewall wind speeds typically exceed the turbine-specific cutoff wind speed. In this case, turbines are parked to minimize loads. However, further away from the cyclone center, turbines may still be operating. Either way, the wind conditions tested in the DLCs consist of a mean wind profile combined with either a deterministic gust profile or turbulence. A power-law model is used for the wind

35 profile with an associated hub height wind speed and wind shear over the rotor plane. ~~In the International Electrotechnical Commission's standard (IEC), a universal~~ A constant wind shear is suggested for load simulations ~~(?)~~of operating and parked turbines. Such a simplified wind shear model has an influence on turbine loading (Dimitrov et al., 2015). Wind veer, the change in wind direction with height is not accounted for in the IEC standards. However, measurements from He et al. (2016) suggest that wind veer in tropical cyclones can be substantial. Similarly, Worsnop et al. (2017) ~~found~~ find high gust factors,

40 rapid directional changes, and substantial veer in tropical cyclones related to non-stationary small-scale structures in ~~large eddy~~ large-eddy simulations. Kapoor et al. (2020) show, that these features lead to substantially increased loads with respect to the ~~cyclone scale~~ cyclone-scale mean state. Both studies highlight that wind veer should be considered in wind turbine load assessment. Both studies from Worsnop et al. (2017) and Kapoor et al. (2020) are based on idealized Category 5 hurricane simulation. Gomez et al. (2023) analyze wind shear and veer in idealized simulations of Category 1-3 Hurricanes. They find

45 that both wind shear and wind veer exceed current design standards. Because of the high computational costs of ~~large eddy~~ large-eddy simulations, mesoscale simulations remain an attractive and important tool for assessing a large number of tropical cyclones with different intensities and storm sizes embedded in the large-scale circulation.

However, mesoscale models are bound to parameterize sub-grid-scale (SGS) turbulent transport of heat~~momentum~~, momentum, and moisture at the sea surface and in the boundary layer. The relative size of these fluxes is crucial for the intensification

50 of tropical cyclones (Emanuel, 1986). The impact of SGS turbulent fluxes on tropical cyclone simulations has been widely investigated. Ye et al. (2023a) show how the spatial distribution of SGS turbulent fluxes depends on the boundary layer closure and how the SGS fluxes affect the tropical cyclone wind field. It has been shown, that the choice of the boundary layer scheme affects the tropical cyclone intensity ~~(Gopalakrishnan et al., 2013; Rai and Pattnaik, 2018; Rajeswari et al., 2020; Zhang et al., 2020)~~ (Gopalakrishnan et al., 2013; Rai and Pattnaik, 2018; Rajeswari et al., 2020; Zhang et al., 2020; Ye et al., 2023b), the storm ra-

55 dius ~~(Gopalakrishnan et al., 2013)~~(Gopalakrishnan et al., 2013; Ye et al., 2023b), the boundary layer inflow strength (Gopalakrishnan et al., 2013; Rajeswari et al., 2020; Zhang et al., 2020) and the inflow layer depth (Rai and Pattnaik, 2018; Gopalakrishnan et al., 2013; Chen, 2022). This suggests, that ~~the tropical cyclone~~ for tropical cyclones, the three parameters, namely, mean wind speed, wind shear, and veer ~~are~~ can be sensitive to the surface and boundary layer parametrization. For moderate wind conditions in mid-latitudes, simulated wind shear ~~is~~ was found to be sensitive to the boundary layer parametrization and the

model performance depends on atmospheric stability (Draxl et al., 2014; Krogsæter and Reuder, 2014). For tropical cyclone conditions, the sensitivity of wind shear and veer on the boundary layer parametrization might differ from these moderate wind regimes. It is important to know how large the associated uncertainty in these three parameters is. Because civil structures are within the lowest hundred meters it is especially important to focus on the lower part of the boundary layer.

Mesoscale atmospheric simulations use larger grid spacing than ~~large eddy simulationsand cannot resolve sub-kilometer scale variability (Skamarock, 2004).~~ large-eddy simulations. Typically they can only resolve wind speed variability on scales in the order of seven times the horizontal grid spacing (Skamarock, 2004). Smaller scale structures resolved in LES simulations, such as roll vortices, cannot be adequately resolved in mesoscale simulations (Li et al., 2021). With that, the modeled spatial and temporal maximal values of a variable, such as wind speed, depend on the resolved model variability (Larsén et al., 2012). Yet, extreme values are important for structural design and load assessments, and maximal modeled wind speed is one of the most used for model verification (Rajeswari et al., 2020; Shenoy et al., 2021). ~~In Nolan et al. (2009b) the boundary layer parametrization parameters are affected if eyewall vorticity maxima are developed in mesoscale simulations . This suggests~~Nolan et al. (2009b, a) show that the amount of high-frequency perturbations along the eyewall varies between mesoscale simulations with different boundary layer parameterizations. Zhu et al. (2014) analyze the mechanism leading to eyewall perturbations with different frequencies. They show, that the ~~boundary layer parametrization affects wind speed variability in tropical cyclones~~eyewall perturbations depend on vertical SGS fluxes. Similarly, Xu et al. (2021) show that SGS fluxes influence the fine-scale structure of the tropical cyclone wind field in the turbulent gray-zone. Given the effect of the boundary layer simulation on wind field perturbations, the wind speed variability is likely affected by the boundary layer parametrization.

Tropical cyclones have a characteristic wind field structure consisting of three regions. The tropical cyclone eye forms the storm center. There, wind speeds are low and wind turbine loads are expected to be small. The wind speeds are largest and often above wind turbine cut-out in the eyewall region. In the ~~rainband~~ outer cyclone region winds are less extreme and wind turbines might still be operating. Wang et al. (2022) proposes a multi-stage framework to account for the difference in wind speed and turbulence profiles between the eyewall and rainband region.

Accordingly, we investigate the following aspects of the tropical cyclone wind field:

1. How much is the median wind speed, shear, and veer affected by the boundary layer scheme, and how do they compare to the IEC standard?

2. What is the distribution and variability of modeled wind shear, veer, and horizontal wind speed, and how does the distribution depend on the boundary layer parametrization?

3. How is wind speed, shear, and veer, spatially distributed and how does it differ between the eyewall and the ~~rainband~~ outer cyclone region?

2 Methods

2.1 Model set up

The open-source ~~weather research and forecasting~~ Weather Research and Forecasting model (WRF) version 4.4 is used to simulate typhoon Megi, which hit Taiwan in September 2016. This case is chosen for a couple of reasons. First of all, Megi is one of the most severe storms that affected the region over Taiwan. As such it serves as a good example of severe wind conditions. Second, ~~synthetic aperture radar~~ Synthetic Aperture Radar (SAR) data are available, in addition to the best track data sets (described in Sect. 2.3).

We ~~run 36-hour simulations starting at 12 UTC on 25 September after a 12 h spin-up time. We~~ compare three simulations using three different boundary-layer parametrization schemes, summarized in Table 1. The ~~goal of the study~~ purpose is to evaluate the spread between the best physics suits for the different boundary layer schemes. Therefore, each boundary layer scheme is combined with the surface layer scheme that it has been developed with.

1. The Mellor-Yamada-Janjic boundary layer scheme (MYJ) (Janić, 2001) with the revised Eta similarity surface layer scheme (Janić, 2001).

2. The Mellor-Yamada-Nakanishi-Niino order 2.5 boundary layer scheme (MYNN) (Nakanishi and Niino, 2009) with the MYNN surface layer scheme (Nakanishi and Niino, 2009)

3. The Yonsei University boundary layer scheme (YSU) (Hong et al., 2006) with the revised MM5 surface layer scheme (Jiménez et al., 2012).

The ~~YSU scheme is a~~ three schemes use different ways to calculate SGS turbulent fluxes. The YSU scheme uses a non-local first-order K-closure. The MYJ and MYNN schemes use a 1.5 order local Turbulent kinetic energy (TKE) closure. MYNN is formulated based on variables conserved for moist reversible adiabatic processes and is therefore often called a "moist" scheme (Zhu et al., 2014). Differently, YSU and MYJ are "dry" schemes. The three schemes are widely used in WRF. Due to its non-local ~~scheme. Its eddy viscosity is described by a parabolic profile, which is itself a function of boundary layer height. As a non-local scheme , YSU considers that turbulence can be regarded as surface-driven (Kepert, 2012). More precisely, in the YSU scheme, the turbulent tendencies at each vertical level are related to the heat and temperature profile throughout the boundary layer (Nolan et al., 2009b). This scheme is however sensitive to the definition of the boundary layer height (Kepert, 2012), while dynamic and thermodynamic definitions of the boundary layer height lead to different results (Zhang et al., 2011). Most studies find, that YSU performs well for tropical cyclones (Rajeswari et al., 2020). In contrast to the YSU scheme, MYJ and MYNN are local schemes. Their eddy viscosity is defined as a function of the turbulent kinetic energy, which is calculated independently at all model height levels~~closure, YSU is a popular choice to simulate tropical cyclones. Many studies analyze tropical cyclones simulated with the MYJ scheme (Nolan et al., 2009b; Sparks et al., 2019; Rajeswari et al., 2020; Shenoy et al., 2021), partly because it was one of only two boundary layer options in the earlier version of WRF (V2.2). The MYNN scheme is an important option for wind resource assessment in the presence of wind farm effects, because wind turbine parametriza-

tions are available for the scheme (Fitch et al., 2012; Volker et al., 2015).

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The high wind speeds in tropical cyclones affect the surface fluxes. Under moderate wind conditions, the surface momentum flux over water is typically modeled using the Charnock relation (Charnock, 1955). In the Charnock relation, the drag coefficient (C_d) increases monotonically with the wind speed. As a default, the MYJ and the MYNN scheme are based on the Charnock relation and feature monotonically increasing C_d with wind speed. However, observations in Powell et al. (2003) and Donelan et al. (2004) suggest that C_d levels off for wind speeds larger than 33 $\mathrm{m\,s^{-1}}$. Correcting the drag coefficient towards these findings was shown to improve modeling results (Nolan et al., 2009b). In WRF version 4.4, ETA similarity surface layer scheme is the only surface layer scheme with the option to account for such a dependence of C_d on wind speed. In WRF version 4.4, it can be selected over the *isftcflx* option. We use the *isftcflx* option 2 for the YSU simulation. This option has a constant drag coefficient for wind speeds faster than 33 $\mathrm{m\,s^{-1}}$ (Green and Zhang, 2013). In the default, the exchange coefficients for sensible and latent heat are a function of C_d. Using the *isftcflx* option 2, these coefficients are modified based on Garratt (1994). At 40 $\mathrm{m\,s^{-1}}$ surface wind speeds, the exchange coefficients of sensible and latent heat are 40 % to 50 % smaller than in the default (Green and Zhang, 2013).

In all simulations, the Thompson scheme is used to parameterize the micro-physical processes (Thompson et al., 2008). On the outermost domain, convective clouds are parametrized by the Kain-Fritch (Kain, 2004) cumulus scheme. The longwave and shortwave radiation is parametrized by the RRTMG (Iacono et al., 2008) scheme. ~~To reduce the complexity related to friction over land~~Even though offshore wind projects are mostly limited to coastal regions, we chose to focus on the cyclone intensification stage over open water ~~,~~before the typhoon makes landfall. This stage is chosen for two reasons: 1.) Temporal and spatial averaging of the wind field is only reasonably applicable in the absence of abrupt surface changes. 2.) The comparison to literature is simplified, as the majority of model studies addressing the tropical cyclone wind structure focus on tropical cyclones over the open ocean. How the wind field over land and in close proximity to land differs from the open ocean should be addressed in further studies, where our study can serve as a baseline. The domain setup is displayed in Fig. 1. WRF is run on three one-way nested domains, where the two innermost domains use the vortex following grid configuration. All three domains are initialized at 00 UTC on 25 September. The first 12 h are used as spin-up time. The following 36-hour simulations starting at 12 UTC on 25 September are used for the analysis. The outer domain has 350 × 361 grid points with a horizontal grid spacing of 18 km. The two inner domains have 361 × 361 grid points and a horizontal spacing of 6 km and 2 km. The three domains are run with a 45, 15, and 5 s timestep~~on 60~~. All domains use 70 vertical layers. The lowest model levels have a mean height of 8, 26, 47, 72, 102, 139, 183, 234, 297, and 372 m. The model top is at 200 hPa. For the initial and boundary conditions, ERA5 reanalysis data (Hersbach et al., 2018) is used. The sea surface temperature is used from OSTIA (Donlon et al., 2012).

Table 1. Summary of parametrization schemes used in the three simulations with YSU, MYJ, and MYNN 2.5.

Name	YSU	MYJ	MYNN
Boundary layer scheme	YSU	MYJ	MYNN 2.5
Surface layer scheme	MM5	Eta similarity	MYNN surface layer
Ocean surface drag	isftcflx=2	unchanged	unchanged
Micro physics scheme		Thomson et al.	
Cumulus scheme in d01		Kain-Fritsch	
Radiation physics scheme		RRTMG	
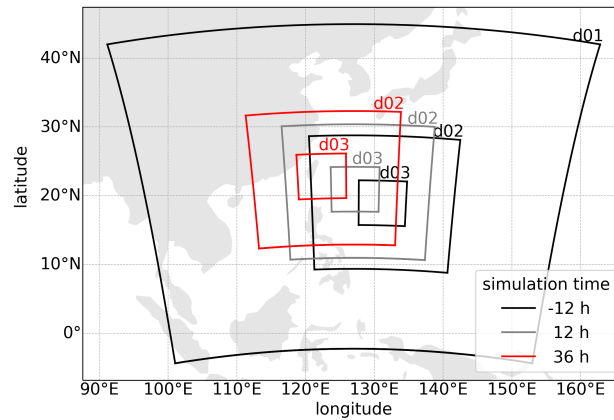
Figure 1. Domain set up: domain borders at the start of the 12 h spin-up time (black), after 12 simulation hours (~~grey~~gray), and after 36 simulation hours (red). Note that domain d01 is fixed in time.

2.2 Analysis method

Wind speed, wind shear, and veer are calculated from the three simulations. The analysis is based on the instantaneous model output of the innermost domain, saved every ten minutes. ~~In the IEC , wind shear is mostly expressed as~~ The analysis of wind shear is performed, such that a comparison to the IEC standard is straightforward. For the assessment of extreme wind conditions, the IEC assumes a wind profile according to the extreme wind speed model:

$$V_{50} = V_{ref} * (\frac{z}{z_{hub}})^\alpha \tag{1}$$

Here V_{50} is the extreme wind speed with a return period of 50 years, averaged over a ten minute interval. For areas affected by tropical cyclones, the reference wind speed V_{ref} is $57 \mathrm{\ m\,s^{-1}}$. The height is given by z, and the hub height by z_{hub}. The wind shear exponent α ~~, which describes a power-law wind profile (?):~~ is a measure of vertical wind shear. Strong wind shear

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is associated with larger α values. For extreme wind conditions, the IEC uses a constant α of 0.11 (IEC, 2019a). Under normal wind conditions offshore, α is set to 0.14 (IEC, 2019b). In this study α is calculated using Eq. 2.

$$\frac{u_2}{u_1} \alpha = \frac{z_2}{z_1} \alpha - \frac{\ln(u_2/u_1)}{\ln(z_2/z_1)} \tag{2}$$

Here, u_1 and u_2 are the wind speeds at heights z_1 and z_2 respectively. ~~Wind veer is defined based on the inflow angle θ, which is the angle between the tangential and the radial wind vector (Ming et al., 2022). Wind veer is then calculated from the difference of θ between two model levels and normalized over the vertical distance between the model layers:~~

$$Veer = -\frac{\theta_2 - \theta_1}{z_2 - z_1},$$

~~Here, θ is defined at the model heights z_1 and z_2. The minus sign in Eq. 3 is introduced such that positive (negative) veer values are obtained for clockwise (counterclockwise) rotating wind vectors with height. We define z_1 and z_2 such that they represent a wind turbine~~ While α depends on height, the IEC assumes a constant α over the rotor plane. We analyze both α between consecutive model levels at different heights and the total α over the rotor plane. For the latter, we use a least square fit between $\ln(u)$ and $\ln(z)$. All model levels between the rotor bottom and ~~top. For z_1~~ the rotor top are used for the fit.

For the rotor bottom, we use the height of the second model level, which has a median height of 26 m. The ~~seventh~~ eighth model level with a median height of 234 m is used as ~~z_2~~ the height of the rotor top. The heights are chosen as a compromise between using model-level heights and representing a wide range of future wind turbine types planned in the Taiwan Strait based on 4Coffshore (2023). The described fictional turbine has a rotor diameter of 208 m and a hub height of 130 m. While most operating turbines in the Taiwan ~~strait~~ Strait have smaller rotor diameters, 14 MW wind turbines with 222 m rotor diameter are now planned in the Hailong Offshore wind farm to be operational in 2026. We further analyze the wind speed, at the fifth model level. This model level has a medium height of 139 m and is closest to the hub height of the fictional wind turbine. ~~To understand the sensitivity of our analysis to the selection of these three heights, the profiles of wind speed and inflow angle are further analyzed. As we define shear and veer based on only two heights, only a monotonic change of wind speed and direction~~

Wind veer is defined as the shortest rotational path between the wind direction (WD) at different heights, which is maximal 180 °. It is defined such that positive (negative) veer values describe clockwise (counterclockwise) rotation with increasing height. With that, a decreasing (increasing) inflow angle with height is ~~considered. In reality, maxima might occur between the two points as found in Kapoor et al. (2020). However, this is~~ associated with positive (negative) veer values. In this study we normalize wind veer by the vertical distance between two used heights. Veer is calculated as follows:

$$Veer = \frac{\min(WD_2 - WD_1)}{z_2 - z_1} \tag{3}$$

Here, WD is defined at the model heights z_1 and z_2. Similar to the analysis of α, wind veer is analyzed between consecutive model levels at different heights, as well as over the rotor plane. For the latter, we use a least square fit between WD and z. All

195 model levels between the rotor bottom and the rotor top are used for the ~~case for only 0.3% (3.3%) of the analyzed wind speed (wind direction) profiles in our study~~fit.

The eyewall and ~~the rainband~~ outer cyclone regions are analyzed separately. ~~These two regions are defined based on the distance~~ With that, we can account for and characterize differences between the two storm regions. To avoid, that the position of the simulation domain relative to the cyclone center ~~. The eyewall region is defined as the area with~~ influences the analysis,
200 we use only grid points within a distance to the cyclone center ~~between 60 and 120 km. The decision of this radius range~~ (R) smaller than 350 km. The definitions of the eyewall and outer region are illustrated in Fig. 2 and summarized in Eq. 4 and 5. We define the eyewall as a high wind speed regime. Our definition is based on the ~~analysis of the median wind speed as a function of radius (shown in Sect.~~ simulated wind speed at 10 ~~3). It is chosen such that it includes the highest wind speeds in the simulation. The rainband region is defined as the region with a distance to the cyclone center between 200 and 400 km~~
205 ~~and contains the spiraling rainbands~~ m (WS_{10}) at each simulation time step. Grid points are assigned to the eyewall region if two criteria are fulfilled: 1.) WS_{10} is greater than or equal to the 80th percentile of WS_{10} ($P_{80}(WS_{10})$), and 2.) R is less than 250 km. The selected eyewall area is 76000 km^2. The thickness of the eyewall is not symmetrical over the azimuth and can be zero. Note also, that the area includes gaps, where the wind speed is lower than $P_{80}(WS_{10})$. The outer region includes all grid points that are not part of the eyewall and the eye. To distinguish between the outer region and the eye, we define a critical
210 radius R_{Eye} in Eq. 5. Here, R_{Eye} is taken as the 10th percentile of R of the eyewall grid points ($P_{10}(R_{Eyewall})$). Thus

$$\text{Region} = \begin{cases} \text{Eyewall:} & \text{if } WS_{10} \geq P_{80}(WS_{10}) \text{ and } R < 250\,\text{km,} \\ \text{Outer cyclone:} & \text{if not Eyewall and } R > R_{Eye} \end{cases} \tag{4}$$

where

$$R_{Eye} = P_{10}(R_{Eyewall}) \tag{5}$$

The outer region is not homogeneous. It includes both the rainbands and the non-convective moat areas. These areas have
215 different properties. However, we do not separate them, to prevent the analysis from becoming sensitive to the selection criteria. Radial averages, profiles, and probability density distributions are calculated using all 144 output timesteps from ~~the~~ 12 UTC on 25 September to 12 UTC on 26 September. Later timesteps are not included, because of enhanced wind field asymmetries near and over Taiwan. We note ~~, that ,~~ that typhoon-land interactions are clearly important for wind turbines, and they ~~should be addressed in future studies~~are addressed in Müller et al. (2023). All grid points within the defined radius range are used,
220 resulting in over ~~120,000~~ 2.7 million points for the eyewall region and ~~10 times more in the rainband~~ 10.4 million in the outer cyclone region. The median and the interquartile range (IQR) are compared between the simulations.

In this study, the cyclone track, inflow angle, and differentiation between the ~~rainband~~ outer cyclone and eyewall region are based on the definition of the cyclone center. We obtain the cyclone center with an algorithm based on the minimal variance of the sea level pressure (SLP) over bands with equal distance to the cyclone center. This center detecting method is recommended
225 by Yang et al. (2020), because it leads to a smooth track variation over time and enhanced symmetry in the wind field.
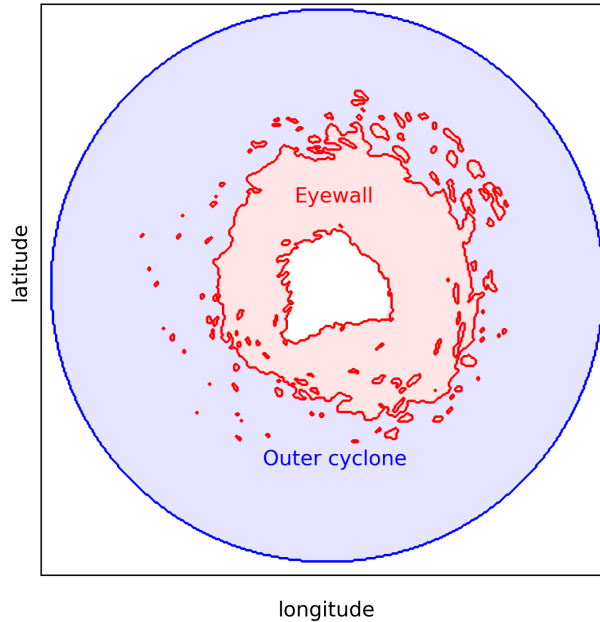
Figure 2. Eyewall and outer cyclone region at an example timestep.

The one-dimensional power spectrum in the wave number domain is used as a measure of variability in the horizontal 10 m wind speed as in Skamarock (2004). For each time step one-dimensional spectra are calculated over the model domain for each model row (oriented approximately in the west-east direction) and column (oriented approximately in the north-south direction). Before calculating the spectra, linear trends in the rows and columns are removed by individually subtracting the result of a linear least-squares fit. The spectrum is obtained by Fourier transform. Ten ~~grid points at the grid edges are removed~~ lines of grid points are removed from the model domain edges to avoid the sponge-layer effects related to the domain nesting. This results in 2×341 spectra per time step. These spectra are averaged over all 144-time steps between 12 UTC on 25 September and 12 UTC on 26 September. The purpose of the spectral analysis of the wind field is to examine the resolved wind variability in comparison with theory as well as with SAR wind data.

2.3 Validation method

The model data is compared to and qualitatively validated against the best track data. Best track data is publicly available from different meteorological centers. In this study best track data sets from two centers are used: the US Joint Typhoon Warning Center (JTWC) and the Regional Specialized Meteorological Center (RSMC) Tokyo-Typhoon Center operated by the Japan Meteorological Agency (JMA). Both data sets include the cyclone's central position in three to six-hour intervals. The best track data sets further include the central pressure and the maximal sustained wind speed. These are mainly based on the method described by Dvorak (1984) (RSMC, 2021; Chu et al., 2002). The maximal sustained wind speed is defined

differently in the two data sets. JTWC reports the maximal one-minute sustained wind speed (Chu et al., 2002), defined as the maximal 10 m wind speed averaged over 1 minute encountered over the entire cyclone structure. JMA in contrast reports the maximal ten-minute sustained wind speed, giving the maximal 10 minute average wind speed (RSMC, 2021). The conversion

245 between the two metrics is not straightforward. Harper et al. (2010) recommends a conversion factor of 0.93 between the larger one-minute sustained wind speed and the ten-minute sustained wind speed over the ocean. Chu et al. (2002) states that the one-minute sustained wind speed is in general around 14 % larger than the ten-minute sustained wind speed. This results in a conversion factor of 0.88, and a larger difference between the two data sets. The difference between the sustained wind speed in the two data sets is even larger than 14 % (Ott, 2006). We decided to use both best track data sets to see the model spread

250 in relation to the spread in the best track data. For easier comparison, we additionally provide the JTWC one-minute sustained wind speeds converted to ten-minute sustained wind speeds. We use, the factor 0.93 recommended by Harper et al. (2010) for the conversion.

We further use Synthetic Aperture Radar (SAR) wind scenes for the validation of the modeled horizontal wind speed structure and variability. Wind scenes are post-processed by Badger et al. (2022) and taken from the European ~~space agency~~ Space

255 Agency (ESA). This study uses eight wind scenes, that cover different areas of typhoon Megi between 9 and 22 UTC on 26 September 2016. The scenes are shown in Fig. 3. The scenes provide the 10 m wind speed in a regular 500 m grid. One-dimensional power spectra are calculated from the eight wind scenes in the same way as for the model data (see Sect. 2.2). The spectra are calculated over the axis with the larger number of grid points and averaged over the shorter axis for each of the eight SAR wind scenes.

260 Lastly, the wind profile structure is compared to global positioning system dropsonde measurements documented in Powell et al. (2003) and Vickery et al. (2009). The measurements include 331 profiles from 15 tropical cyclones over the Atlantic Eastern and Central Pacific. Based on these measurements Vickery et al. (2009) suggests an empirical formulation for the tropical cyclone boundary layer which accounts for a low-level jet:

$$U(z) = u_*/\kappa[ln(z/z_0) - a(z/H^*)^n], \tag{6}$$

265 Here, u_* is the friction velocity, κ the von Kármán coefficient, z the height, z_0 the surface roughness length, and H^* a boundary layer height parameter. The parameters a and n are free parameters fitted to the dropsonde measurements. Vickery et al. (2009) analyze the dropsonde measurements in a composites sense. They group the measurements according to the radius of maximal winds (RMW) and the mean boundary layer (MBL) wind speed. The latter is defined as the mean wind speed over a height range of 10 to $500\,\mathrm{m}$. Based on the JTWC best track ~~dataset~~data set, typhoon Megi's RMW is mostly in the range of 30-

270 60 km during the analyzed period. The MBL wind speed is calculated from the simulated eyewall profiles. Depending on the boundary layer scheme used in the simulation, the MBL wind speed is in the range of 30-39 $\mathrm{m\,s^{-1}}$ or 40-49 $\mathrm{m\,s^{-1}}$. With that, we can compare the simulated wind profiles with ~~two~~ wind profiles defined by parameter-sets given by Vickery et al. (2009), describing wind profiles with the corresponding RMW and the two MBL wind speed ranges. Vickery et al. (2009) further assess two methods to obtain the parameter-sets for each group. Both parameter-sets are used in our study. To compare the

275 vertical wind shear from the dropsonde measurements to the analyzed simulations, α is calculated from Eq. 2.
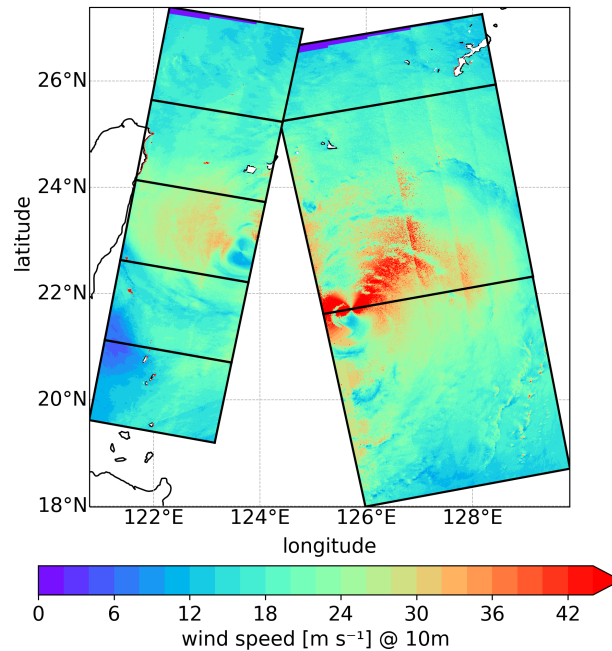
Figure 3. Synthetic aperture radar wind scenes used for model validation. The five wind scenes on the western side are taken between 9.35 and 9.38 UTC and the three on the eastern side between 21.31 and 21.46 UTC on 26 September 2016. The wind scenes are retrieved from Badger et al. (2022).

3 Results

3.1 Model verification against best track data

Cyclone Megi develops from a tropical disturbance in the western Pacific Ocean and reaches tropical cyclone intensity on 24 September. Megi's track and intensity in terms of minimal SLP and maximal wind speed from 25 September onward are shown in Fig. 4 and 5. On 24 September cyclone Megi continues its trajectory north-westwards toward Taiwan. During this trajectory over the open ocean, Megi intensifies. Its minimal SLP decreases and the maximal wind speed increases and reaches a maximum at 00 UTC on 27 September (see Fig. 5). On 27 September Megi hits Taiwan and weakens. This can be seen in the consequent increase of the minimal SLP and the decrease in wind speed. After entering the Taiwan ~~strait~~ Strait, Megi makes landfall over mainland China between 18 UTC on 27 September and 00 UTC on 28 September.

The simulations cover the period between 12 UTC on 25 to 00 UTC on 27 September when Megi intensifies over the open ocean. During this time, the two best track data sets are in close agreement in terms of central position (Fig. 4). All three simulations can reproduce the general cyclone track, with only a slight southward deflection. The error at the end of the simulations is within 130 km. The error in the simulated track is larger than in the ERA5 ~~dataset~~data set, which is used as boundary conditions. The simulations can further reproduce cyclone intensification (Fig. 5). However, the degree of intensi-
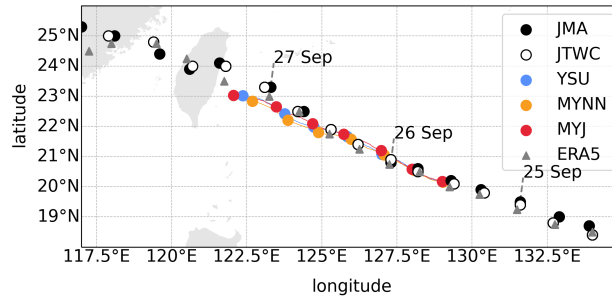
Figure 4. Typhoon track: Cyclone center position of the YSU (blue), MYNN (red), MYNN-eta (purple), and MYJ (yellow) simulation and of the best track data sets from JMA (black filled points) and JTWC (white filled points). Points show the position at 00, 06, 12, and 18 UTC. Lines show the position every 10 minutes for the simulations.

fication varies between the simulations. From Fig. 5 it can be seen that the minimal SLP drops initially at the highest rate in the MYJ simulation. However, at 6 UTC on 26 September, the MYJ simulation stops intensifying. At the simulation end, the minimal SLP of the MYJ and the YSU schemes are similar. The comparison between the maximal wind speed and minimal SLP in the simulations and the best track data has shortcomings, especially since the two sizes depend on the spatial and temporal resolution of the simulation. Nevertheless, the comparison is widely used and helpful to qualitatively evaluate the simulated intensity (Rajeswari et al., 2020; Shenoy et al., 2021; Zhu et al., 2014). The minimal SLP of both MYJ and YSU is mostly between the minimal SLP from the JTWC and the JMA best track data set. The difference in the simulated minimal SLP between these two simulations is smaller than between the best track ~~datasets~~data sets. Similarly, the maximal wind speed of the YSU and the MYJ simulation is between the maximal ten-minute sustained wind speed reported by JMA and the maximal one-minute sustained wind speed reported by JTWC. Differently, the typhoon in the MYNN simulation intensifies less than in the JMA and JTWC best track data sets. Its minimal SLP follows the higher minimal SLP of the coarser ERA5 data. The MYNN maximal wind speed follows the maximal ten-minute sustained wind speed reported by JMA and is lower than in the YSU and MYJ simulations.

3.2 Mean wind field

We analyze the characteristic structure of a tropical cyclone through an example simulation timestep at 00 UTC on 26 September. This timestep is the center of the analyzed period from 12 UTC on 25 September to 12 UTC on 26 September. The horizontal wind field at $10\,\mathrm{m}$ at that time is given in Fig. 6 ~~a-c~~ for the three different boundary layer schemes. In the eye, the center of the storm, wind speeds are near zero. Outside of the eye, the wind rotates in a circular pattern counterclockwise. Larger wind speeds are evident in the ~~top~~ back right quadrant, ~~northwestward~~ northeastward of the eye. Here, wind speeds are around $4\,\mathrm{m\,s^{-1}}$ larger than in the back left quadrant, southwestward of the eye. Nevertheless, the ~~symmetric wind speed component dominates over asymmetric features~~wind speed changes similarly with increasing distance to the cyclone center in all quadrants. This allows averaging the wind field over the azimuth, as shown in Fig. 7. Based on the averaged wind over
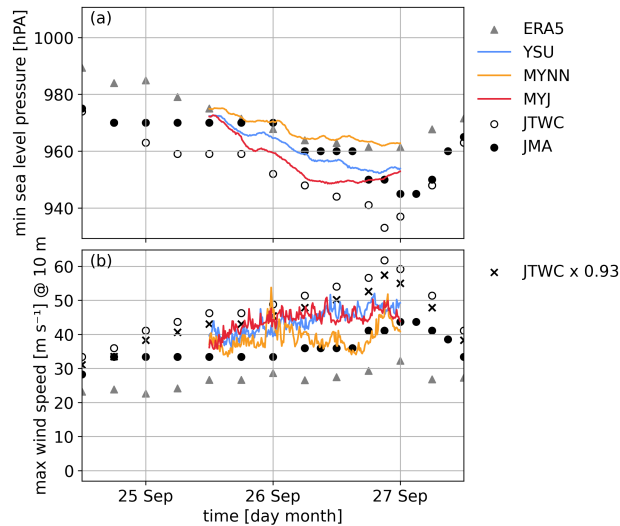
Figure 5. Cyclone intensity in terms of a) minimal SLP of the simulations (lines) and the ERA5 reanalysis data (triangles) compared to the best track data (circles) and b) maximal instantaneous wind speed ~~at 10 m~~ in the simulations (lines), the ERA5 reanalysis (triangles), the maximal ten-minutes sustained wind field from JMA (black points), and the maximal one-minute sustained wind field from JTWC (white points). Black crosses show the JTWC values multiplied by 0.93, as recommended by ~~(Harper et al., 2010)~~ Harper et al. (2010) to convert ~~ten-minute~~ one-minute sustained wind speeds to ~~one-minute~~ ten-minute sustained wind speeds in tropical cyclones over the sea.

time and azimuth, we can systematically compare the wind speed in the three simulations. Wind speeds are maximal in the eyewall. ~~There, the~~ In the YSU and MYJ simulations, the wind speed at 10 m ~~wind speeds are in the median in the YSU and the MYJ simulations~~ is $32\,\mathrm{m\,s^{-1}}$ in the eyewall. The MYNN simulation shows a $12\,\mathrm{m\,s^{-1}}$ lower 10 m eyewall wind speed than

315 the MYJ and the YSU simulation. This qualitatively agrees with the lower maximal wind speed in the MYNN simulation over the entire simulation period as described in Sect. 3.1. Additionally, the distance between the eye and the maximal wind speed in the eyewall is larger in the MYNN (104 km) simulation than in the YSU ~~and the MYJ simulations. In terms of the radius of maximal averaged wind, the difference is 12 km (10~~ (92 km) ~~with respect to the YSU (MYJ) simulation~~ and the MYJ (94 km) simulations. With increasing distance from the eyewall outwards, the wind speed gradually decreases. The radial gradient in

320 wind speed is most pronounced in the MYJ simulation. In the ~~eyewall~~ outer cyclone region, the surface wind speeds are highest in the YSU simulation, followed by the MYJ simulation and the MYNN simulation.

The simulated vertical wind field structure is analyzed based on ~~profiles of wind speed and inflow angle~~ median profiles. The wind speed increases with height as shown in Fig. 8. The structure of the simulated profiles qualitatively agrees with the structure of dropsonde measurements reported by Vickery et al. (2009). The simulated profiles are characterized by a jet

325 at around 800 m in the eyewall region and at 1200 m in the outer cyclone region. Below the jet, the simulations have an approximately logarithmic wind speed increase with height. The simulated wind profiles differ in two aspects: Firstly, the wind shear below the jet nose is more pronounced in the YSU simulation with respect to the profiles from Vickery et al. (2009)
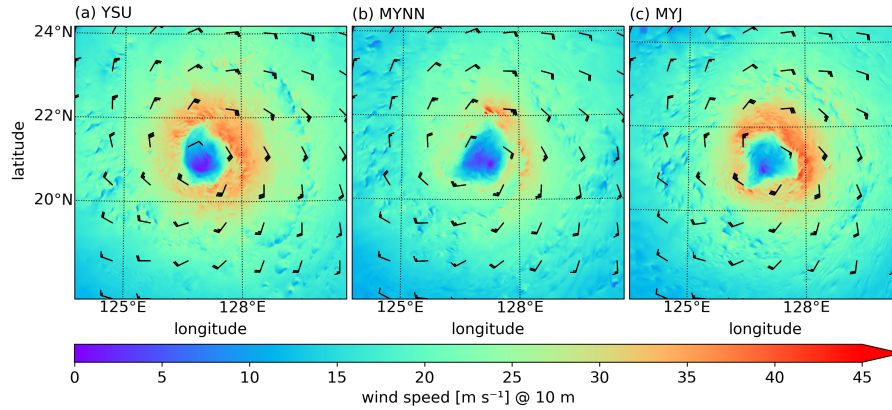
Figure 6. ~~Horizontal fields~~ Wind speed at 10 m taken from the model output at ~~12~~00 UTC on 26 September ~~. a-c) show the instantaneous horizontal wind field at 10 m in~~ for the ~~YSU, MYNN, and MYJ simulation. d-f~~a) ~~show the~~ YSU~~d) wind speed at 139 m~~, e~~b) wind shear defined as bulk wind speed difference between 234 and 26 m~~MYNN, and ~~f) wind veer defined as the difference in the inflow angle between 234 and 26 m. Black contours in a~~c) ~~mark circles of 60, 120, and 400 km distances from the cyclone center~~MYJ simulation.
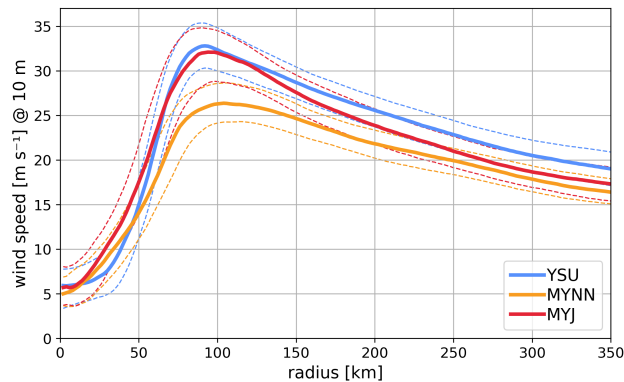
Figure 7. 10 m wind speed as a function of distance from the cyclone center for the YSU, MYNN, and MYJ simulation: median (solid line) and 0.25 and 0.75 percentiles (dashed lines). ~~Black bars mark the eyewall region (60-120 km) and the rainband region (200-400 km).~~ The values are obtained from all grid points within 144 output ~~time-steps~~ time steps between 12 UTC on 25 September and 12 UTC on 26 September, analyzed in bins of 2 km radius.

and the MYNN and MYJ ~~simulation~~simulations. Secondly, the slope of the logarithmic wind profile is larger in the MYJ simulation, than in the profiles from Vickery et al. (2009), the MYNN simulation, and particularly in the YSU simulation. ~~The~~ To evaluate the change in wind speed with height ~~is given in terms of α in Fig. 10 and~~ Table 2 lists the median α between rotor top and rotor bottom. The simulated median α ranges from 8.3×10^{-2} to 1.1×10^{-1} in the eyewall. This is in good agreement with the α ~~values~~ values obtained from the profiles form Vickery et al. (2009), which are within 9.1×10^{-2} and 9.6×10^{-2} for the selected profiles. Compared to the eyewall region, the simulated α ~~values~~ values are smaller in the ~~raindband~~ outer

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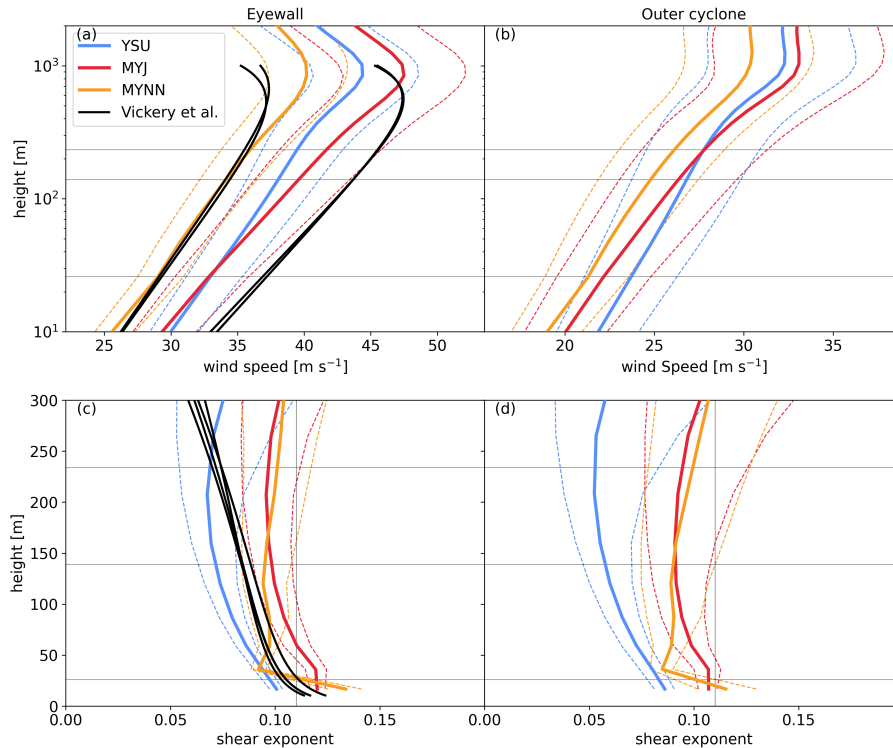
Figure 8. Profiles of a,b) wind speed, and shear exponent c,d) for the a,c) eyewall region, and b,d) outer cyclone region. Solid lines show the median and dashed lines show the 0.25 and 0.75 percentiles. Horizontal lines show the heights of 26, 139, and 234 m. A shear exponent of 0.11 is indicated by vertical lines. The values are obtained from all grid columns within defined regions in 144 output time steps, between 12 UTC on 25 September and 12 UTC on 26 September.

cyclone region, where they are in the range of ~~to~~ 7.0×10^{-2} to 9.8×10^{-2}. The larger slope in the MYJ ~~simulation~~ wind speed

335   profile with respect to ~~the~~ YSU reflects in a 2.7×10^{-2} to 2.8×10^{-2} larger median shear exponent. While the wind profile in the IEC standard is based on a constant α over the rotor diameter, this simplification might not be given for large turbine sizes. To analyze how α varies with height, profiles of α are shown in panels c and d of Fig. 8. According to Vickery's wind speed model (Eq. 6), α decreases monotonically with height. This is different in the simulations. The YSU and MYJ simulations show a similar behavior of α with height. In these simulations, α decreases with height only below the hub height. Between

340   the hub height and the rotor top the median α changes less with height. Yet, along the spiraling rainbands, α increases around 3×10^{-2} between the hub height and the rotor top (not shown). The MYNN simulation produces a pronounced change in wind speed between the first and second model levels. This results in an enhanced α between these levels. Above the second model level α increases slightly. Over the rotor diameter the increase in α is 7×10^{-3} (~~) larger shear exponent in the exponent in the eyewall (rainband~~ 2×10^{-3}) in the outer cyclone (eyewall) region.

Table 2. Median and interquartile range (IQR) of wind speed at 139 m, wind shear exponent, and wind veer, as well as the percentage of shear exponent values larger than 0.11. The values are listed for the eyewall region and outer cyclone region for the YSU, MYJ, and MYNN simulation.

Region	Scheme	Wind speed [m s^{-1}]		Shear exponent			Wind veer [° m^{-1}]	
		median	IQR	median	IQR	% > 0.11	median	IQR
Eyewall	YSU	38.0	5.4	8.3×10^{-2}	1.1×10^{-2}	0.9	1.4×10^{-2}	7.8×10^{-3}
	MYNN	34.1	4.3	9.6×10^{-2}	1.2×10^{-2}	6.5	1.6×10^{-2}	7.1×10^{-3}
	MYJ	39.5	7.1	1.1×10^{-1}	1.3×10^{-2}	43.6	1.7×10^{-2}	7.6×10^{-3}
Outer cyclone	YSU	26.8	6.1	7.0×10^{-2}	1.6×10^{-2}	3.8	9.1×10^{-3}	8.0×10^{-3}
	MYNN	24.8	5.6	8.9×10^{-2}	1.8×10^{-2}	10.4	1.2×10^{-2}	7.8×10^{-3}
	MYJ	26.3	6.5	9.8×10^{-2}	1.9×10^{-2}	22.3	1.2×10^{-2}	8.4×10^{-3}

The difference in the slope of the wind profile is important for wind turbines because it controls the wind speed at hub height and the wind shear over the rotor plane. At hub height, the horizontal wind speed has an analog structure as the surface wind field but an increased magnitude ~~(Fig. 6 d). With the larger gradient in wind speed with height, the~~. The MYJ simulation has a 1.9 m s^{-1} larger eyewall wind speed at hub height than the YSU ~~scheme, while having a similar wind speed at 10 m (see Fig. 10 and~~ simulation (see Table 2). Note, that this is different at 10 m, where the two simulations have similar wind speeds in the eyewall. The difference between the two heights is a direct result of the larger shear exponent in the MYJ simulation with respect to the YSU simulation. At hub height, the MYNN simulation has a 7.9 m s^{-1} (6.0 m s^{-1}) smaller wind speed than MYJ (YSU). The wind speed in the ~~rainbands at hub~~ outer cyclone region at hub height is similar in the MYJ and the YSU and smaller in the MYNN simulation.

The inflow angle is shown as a function of height in Fig. ~~8~~9. All schemes exhibit a median inflow with a depth of around 1000 m. The surface inflow angle is ~~clearly~~ smaller in the MYNN simulation than in the YSU and the MYJ ~~simulation~~simulations. Within the inflow layer, the mean wind turns outward with respect to the cyclone center with height. The change in the inflow angle with height is relatively constant in the lowest 400 m of the boundary layer and comparable between the three simulations. The resulting median wind veer is in close agreement between the three simulations (see Table 2). The simulated median wind veer ranges from ~~to~~1.4 × 10^{-2} ° m^{-1} to 1.7 × 10^{-2} ° m^{-1} in the eyewall region and from ~~to in the rainband region(see~~ 9.1 × 10^{-3} ° m^{-1} to 1.2 × 10^{-2} ° m^{-1} in the outer cyclone region. Similar to our analysis of α, we analyze the change in wind veer over the rotor diameter in Fig. ~~10 and Table 2).~~ 9 c and d. Wind veer is maximal close to the surface. Below the hub height veer generally decreases with height. The difference in wind veer between rotor bottom and hub height is 18 % in the MYJ simulation and around 8 % in the MYNN and YSU simulations. Above the hub height wind veer is nearly constant for the MYJ and slightly increases with height for the YSU and MYNN simulations. MYNN produces strongly enhanced wind veer between the lowest two model levels.

Figure 9. Profiles of a,b) inflow angle and wind veer c,d) for the a,c) eyewall region, and b,d) outer cyclone region. Solid lines show the median and dashed lines show the 0.25 and 0.75 percentiles. Horizontal lines show the heights of 26, 139, and 234 m. The values are obtained from all grid columns within defined regions in 144 output time steps, between 12 UTC on 25 September and 12 UTC on 26 September.

3.3 Wind variability

Apart from the ~~large-scale~~ typhoon-scale structure, the simulations also produce mesoscale variability in the wind field. ~~Finer-scale~~ Mesoscale wind fluctuations can be seen in all simulations within and outside of the eyewall in Fig. 6. ~~To compare~~
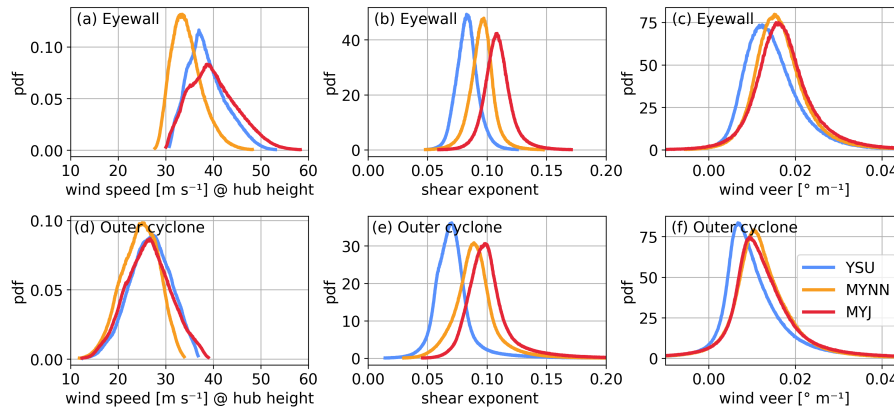
Figure 10. Probability density of a,d) wind speed at 139 m, b,e) wind shear exponent, and c,f) wind veer. The probability density is given for the a-c) eyewall region, and c-f) outer cyclone region for the YSU, MYJ, and MYNN simulation.

~~the~~ Variability caused by turbulence is however not resolved in the mesoscale simulations. To address the resolved variability
of wind speed, wind shear, and wind veer, we show the probability density functions of these sizes in Fig. 10. In Sect. 3.2
differences in median values were commented. Here, we focus on the spread of the distributions. The hub height eyewall
wind speed ranges between 30 to 60 ~~speed between the simulations~~$\mathrm{m\,s^{-1}}$ (28 to 50 $\mathrm{m\,s^{-1}}$) in the MYJ and YSU (MYNN)
simulation. Note, that the lower boundary of the distribution is controlled by our definition of the eyewall region (see Sect. 2).
The wind speed distribution is broader for the MYJ simulation than for the YSU and particularly the MYNN simulation.
Concretely, the IQR of the eyewall wind speed is 7.1 $\mathrm{m\,s^{-1}}$ in the MYJ simulation, 5.4 $\mathrm{m\,s^{-1}}$ in YSU, and 4.3 $\mathrm{m\,s^{-1}}$ in MYJ
(see Table 2). Similarly, the wind speed distribution is broader in the outer cyclone region for the MYJ simulation, than for the
other two simulations.

To investigate which scales contribute to the larger wind speed variability in the MYJ simulation, the one-dimensional
wind speed power spectra in the wave number domain ~~is~~ are analyzed in Fig. 11. In agreement with the wider wind speed
distribution, MYJ shows the highest power spectral density and MYNN the lowest over the calculated wavelength range of 6
to 300 km~~and MYNN the lowest~~.

The spectra can be divided into two parts:

1. For wavelengths larger than 15 km, the YSU and MYNN simulated spectra have a slope of approximately minus five-
   thirds and a slightly smaller slope for MYJ. The smaller slope in the MYJ simulation particularly increases the spectral
   power density contribution from higher wave numbers. The MYJ slope in this range fits the mean spectral slope obtained
   from the SAR images the best. Also, the magnitude shows the best fit for the MYJ simulation.

2. For wavelengths smaller than 15 km the simulated spectra have a ~~smaller~~ steeper slope than minus five-thirds. Differently,
   the spectra from the SAR images have ~~larger~~ flatter slopes than minus five-thirds. In other words, the energy level of the
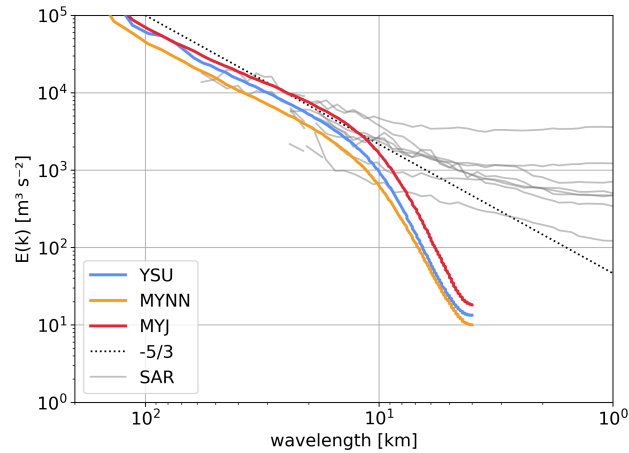
Figure 11. One-dimensional power spectrum in the wave number domain for the three simulations (color) and eight SAR wind scenes (~~grey~~gray). The slope of minus five-thirds is shown for reference (dashed). For better readability, logarithmic averaging is applied to the spectra.

simulations drops stronger with increasing wave number than observed. This ~~shows~~suggests, that the spectral tails are damped in the simulations consistent with Skamarock (2004) and Larsén et al. (2012).

~~For the scenes analyzed , namely,~~

For wind shear, it is of interest how the simulated α differ from 0.11, which is used in the IEC maximal wind speed model. While the IQR of the α values varies little between the different simulations, the percentage of α values larger than 0.11 depends on the simulation, as well as the specific parts of a tropical cyclone. For the YSU simulation, α is mostly smaller than 0.11 for the analyzed scenes, namely before being affected significantly by land~~,~~. Only 3.8 % (0.9 %) of the values are larger than 0.11 in the outer cyclone (eyewall) in the YSU simulation. The fraction is larger for the MYNN simulation. MYNN produces 10.4 % of the α values larger than 0.11 in the outer cyclone region. For MYJ with the largest median α, a large fraction of α exceeds 0.11: the percentages larger than 0.11 are 43.6 % in the eyewall and 22.3 % in the outer cyclone region. The tails of the ~~IQR of wind veer and wind shear are nearly insensitive to the boundary layer scheme~~α distribution include values larger than 0.11. In the eyewall of the MYJ simulation, 14.2 % of the α values are larger than 0.12, and 0.7 % are larger than 0.15. In the outer cyclone region, 12.6 % of the α values are larger than 0.12, 4.1 % are larger than 0.15, and 1.0 % are larger than 0.2.

For all the simulations, wind veer is mostly confined within 0 and 0.03 $^\circ\,\mathrm{m}^{-1}$. However, the tails of the distribution are thick. To show where large α and veer values occur in the tropical cyclone, the horizontal field of α and veer at 00 UTC on 26 September is shown in Fig. 12. In all simulations, the spatial distribution of shear and veer is not uniform and varies between different regions of the tropical cyclone. In the ~~rainband~~outer cyclone region, the maximal values of shear and veer are found along the spiraling rainbands (Fig. 6). Along the rainbands, there is a zone of lower horizontal wind speed. Within this zone, local maxima and minima of wind shear are alternating. The wind veer changes from ~~negative~~positive values (inflow angle
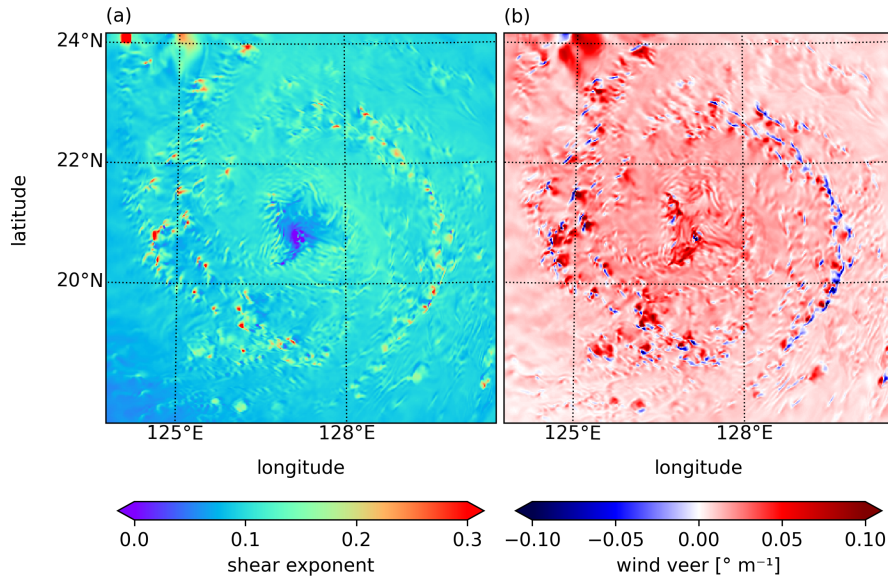
Figure 12. Horizontal fields taken from the MYJ model output at 00 UTC on 26 September of a) the shear exponent and b) wind veer.

decreasing with height) on the radially inward side of the rainbands to ~~positive~~ negative values (inflow angle increasing with height) on the outside.

To further assess the horizontal asymmetry, wind speed, shear, and veer are analyzed in four quadrants relative to the storm motion. Median values are listed for the MYJ simulation in each quadrant in Table 3. Note, that the MYJ simulation resulted in the most severe wind speed, shear, and veer. In the Eyewall wind speed, shear and veer show less variation between the quadrants than between the different simulations. However, the asymmetry of the wind field reflects in the area forming the eyewall region in each quadrant. The two right quadrants have a larger eyewall area than the two left quadrants. The difference in the area is 65 % between the larger eyewall area in the back right quadrant and the smaller eyewall area in the front left quadrant. Different from the eyewall region, in the outer cyclone wind speed shear and veer show clear variations between the quadrants. Wind speed and wind shear are larger in the right quadrants than in the left quadrants. The difference in the median wind speed is $4.3 \, \mathrm{m \, s^{-1}}$ between the front left and the back right quadrant. For α the difference is 8.6×10^{-3} between the two right sectors and the back left sector. In the back right sector, 27.3 % of the profiles have α values larger than 0.11. Different from wind shear, wind veer is larger in the two front quadrants than in the back quadrants. The largest median wind veer, in the front right quadrant, is 1.3×10^{-2}.

4 Discussion

The three WRF simulations using the MYNN, YSU, and MYJ boundary layer schemes ~~are able to~~ can produce a typhoon with a physically realistic track in terms of propagation speed and direction. Track position discrepancies are within $130 \, \mathrm{km}$. As the

Table 3. Median of wind speed at 139 m, wind shear exponent, and wind veer, as well as the percentage of shear exponent values larger than 0.11. The values are listed for the eyewall region and outer cyclone region for four motion-relative storm quadrants for the MYJ simulation. The area falling into the eyewall and outer cyclone region is further listed for each quadrant.

Region	Quadrant	region size [km^2]	Wind speed median [m s^{-1}]	Shear exponent median	% > 0.11	Wind veer median [° m^{-1}]
Eyewall	front right	6.2×10^4	39.4	1.1×10^{-1}	41.0	1.7×10^{-2}
	front left	3.9×10^4	38.7	1.0×10^{-1}	29.2	1.8×10^{-2}
	back left	4.9×10^4	39.7	1.1×10^{-1}	41.0	1.6×10^{-2}
	back right	7.2×10^4	39.9	1.1×10^{-1}	53.4	1.6×10^{-2}
Outer cyclone	front right	2.2×10^5	27.0	1.0×10^{-1}	31.1	1.3×10^{-2}
	front left	2.4×10^5	24.1	9.2×10^{-2}	14.6	1.2×10^{-2}
	back left	2.2×10^5	24.6	9.5×10^{-2}	17.0	1.1×10^{-2}
	back right	1.9×10^5	28.4	1.0×10^{-1}	27.3	1.0×10^{-2}

track of the ERA5 reanalysis data shows good agreement with the best track data sets, it is evident that the track errors develop within the simulations. The higher SLP at the end of the MYNN simulation indicates, that this simulation underestimates Megi's intensity. However, this doesn't directly lead to the conclusion that the MYNN boundary layer scheme produces overly weak cyclones in general. On one hand, the best track datasets data sets are mainly based on satellite observation, without direct in-situ measurements. This leads to uncertainty in the data as reflected by the spread of the JMA and JTWC data sets. On the other hand, the results of this study cannot readily be generalized to tropical cyclones with different intensities and storm sizes. At last, accounting for atmosphere, ocean, and atmosphere wave interactions may further improve model performance and simulated tropical cyclone intensity.

Given that many factors play into the model results, one may question how representative the selected case is, regarding the effect of the boundary layer scheme. We argue that the differences between the MYNN simulation on the one hand and the YSU and MYJ simulation on the other hand strongly agree with documented sensitivity studies. Similar to our case, Rajeswari et al. (2020) found weaker storms for MYNN than for YSU, and most intense storms for MYJ, related to weaker low-level inflow in the MYNN scheme for five cyclones over the Bay of Bengal using WRF version 3.8. MYNN's lower intensity most likely relates to higher vertical diffusion in the MYNN scheme, which has been found to result in less intense storms, larger radius of maximal wind speed, and weaker radial inflow (Kepert, 2012; Gopalakrishnan et al., 2013; Zhang et al., 2020). The differences in the radius of maximal wind speed between the three simulations (see Fig. 7) most likely relate to the cyclone intensity and eddy-viscosity eddy diffusivity (Gopalakrishnan et al., 2013; Zhang et al., 2020).

For extreme wind conditions In the extreme wind speed model (Eq. 1), the IEC standard proposes to use a α of (?)1.1×10^{-1} (IEC, 2019a). The simulated α is in the median equal to or less than the IEC standard 1.1×10^{-1} for all boundary layer

445 schemes. ~~This suggests, thatthe~~ With that, the median shear for extreme wind defined in the IEC standard is as steep or steeper when compared to the mesoscale simulation of typhoon Megi before landfall. This ~~conclusion~~ is in agreement with the α ~~-values~~ values obtained from Vickery et al. (2009). The ~~mean shear profiles from LES simulations in Kapoor et al. (2020) have even smaller α-values, than those obtained in our study. This supports the conclusion, that the current IEC standard is sufficiently similar in terms of wind shear during tropical cyclones. The simulated~~ simulated median α are similar in their

450 order of magnitude and in their sensitivity to the boundary layer scheme to simulations during neutral atmospheric stability at an offshore location in Denmark ~~Krogsæter and Reuder (2014)~~(Krogsæter and Reuder, 2014). In neutral atmospheric stability Krogsæter and Reuder (2014) find that the YSU scheme produces simulation with smaller α (7.7×10^{-2}) compared to the MYNN (8.8×10^{-2}) and the MYJ (1.09×10^{-2}) ~~simulation~~ scheme, similar to the results of our study.

Further, the simulated wind veer is relatively small in comparison with wind veer found in low-wind regimes and particularly
455 during stable conditions. This supports the conclusion, that the current IEC standard may be sufficiently similar in terms of wind shear and veer during tropical cyclones over open water. However, there are clear limitations to this conclusion as discussed in the following.

1. Larger values for α and veer are found in LES simulations over open water. Gomez et al. (2023) find in LES simulations, that the mean α is about 0.2 near the eyewall. Both Kapoor et al. (2020) and Gomez et al. (2023) find significant wind
460 veer in LES simulations. Concretely, Gomez et al. (2023) report a mean wind veer between $5.3 \times 10^{-2\,\circ}\,\mathrm{m}^{-1}$ and $6.9 \times 10^{-2\,\circ}\,\mathrm{m}^{-1}$. The differences between the study from Gomez et al. (2023) and the simulated wind veer in our simulations can come from higher resolved wind veer variability in LES simulations or an overall shifted wind veer distribution due to differences in the mean wind field. In fact, Li et al. (2021) and Ren et al. (2022) find that the inflow layer was shallower and stronger in LES simulation compared to mesoscale simulations. Such a stronger, shallower inflow layer directly
465 leads to a larger mean wind veer.

2. The analysis is based on mesoscale simulation and cannot resolve scales smaller than 15 km. With that structures such as large-scale vortices are not resolved. Such unresolved structures may contribute to enhanced shear and veer.

3. The study analyzes a typhoon case over the open ocean, before being affected significantly by land. In contrast to our simulations over the open ocean, He et al. (2016) and Tse et al. (2013) use wind observations in coastal areas. Both
470 studies find wind shear larger than in the current IEC standard during typhoon conditions. He et al. (2016) find α in the range of 0.152 to 0.175 for profiles with marine exposures during 22 typhoons over Hong Kong. Tse et al. (2013) find α ~~-values~~ values of 0.14 to 0.25 during typhoon Fengshen and Molave for profiles with marine exposure. The larger wind shear in these two studies could be a suggestion that wind shear may increase during the landfall of a tropical cyclone. Further studies are needed to understand how wind shear and veer evolve during landfall.

475 ~~The simulated wind veer is relatively small in comparison to wind veer found in low-wind regimes and particularly in stable conditions. This result stands in contrast to Kapoor et al. (2020) and He et al. (2016) who find significant wind veer in LES simulations and observations respectively. The maximal 10-minute wind veer from during tropical cyclone conditions from LES simulations in Kapoor et al. (2020) is in the order of over the rotor diameter and with that around~~

 Similarly, He et al. (2016) finds wind veer in the order of $2.8 \times 10^{-2}\,^\circ\,\mathrm{m}^{-1}$ from the surface to the height of maximal wind speed from wind direction measurements with an open water fetch over a coastal area. This is around $0.003^\circ\,\mathrm{m}^{-1}$ larger than the wind shear in the YSU and MYJ simulation between the surface and $800\,\mathrm{m}$ (the height of simulated maximal wind speed) and around $0.01\,^\circ\,\mathrm{m}^{-1}$ larger than in the MYNN simulation. ~~Similar to the larger wind shear in the study from He et al. (2016)~~The difference between the studies may originate from the different locations with respect to land.

4. The fraction of profiles with α larger than 0.11 is substantial in the MYJ simulation. In the eyewall region of the MYJ simulation, 43.6 % of the α values are larger than 0.11. Values up to 0.15 are reached in 0.7 % of the eyewall and 4.1 % outer cyclone region. In the outer cyclone region, 1.0 % of the α values are larger than 0.2. Such large α values in the tails of the distribution impact the wind speed above and below z_{hub} in the extreme wind speed model (Eq. 1). As an example, we take the extreme wind speed model with a z_{hub} of 140 m, and a V_{ref} of 57 $\mathrm{m\,s}^{-1}$. The wind speed from the extreme wind speed model at 180 m is 0.6 $\mathrm{m\,s}^{-1}$ (1.3 $\mathrm{m\,s}^{-1}$) larger with an α of 0.15 (0.20) than with an α of 0.11.

5. The analysis of the shear and veer distribution is sensitive to the definition of the eyewall and outer cyclone region. At the inner edge of the eyewall and along the rainbands larger α and veer values are simulated.

6. Wind veer and wind shear vary between the different sectors. Using the extreme wind speed model the difference in median α between the four quadrants leads to differences in the wind speed at above and below the hub height. For example, with a z_{hub} of 140 m and a V_{ref} of 57 $\mathrm{m\,s}^{-1}$, the difference ~~between the studies may originate from the different locations with respect to land.~~ at 180 m between the quadrants in the MYJ simulation is 0.2 $\mathrm{m\,s}^{-1}$.

7. Veer and α are larger close to the surface. In particular, wind veer is up to 18 % larger at the rotor bottom than at hub height in the MYJ simulation. In the extreme wind speed model α is assumed to be constant. Using two different α values below and above the hub height instead of assuming a constant α, the median wind speed at the rotor bottom varies up to 0.5 $\mathrm{m\,s}^{-1}$ in the eyewall region. In the outer cyclone region, the median difference is up to 1.5 $\mathrm{m\,s}^{-1}$.

The simulated profile structure qualitatively agrees with the structure of dropsonde measurements from Vickery et al. (2009). However, the structure of the jet nose in the YSU simulation differs from their engineering model (Eq. 6). The engineering model describes a decreasing slope in a semi-log plot with height. Differently, the profiles of the YSU simulation have an increase in their slope below the height of the jet. This can be seen in Fig. 8 between $250\,\mathrm{m}$ to $800\,\mathrm{m}$ ($300\,\mathrm{m}$ to $1000\,\mathrm{m}$) in the eyewall (~~rainband~~outer cyclone) region. However, it is not given that the empirical formulation holds for typhoon Megi because the MBL wind speed in the YSU simulation is larger than $40\,\mathrm{m\,s}^{-1}$. For such high wind speed profiles, an increase in slope with height below the jet nose is detectable in Fig. 2 and 8 in Vickery et al. (2009). Likewise, He et al. (2022) observed that the curvature of the typhoon wind profile is larger than predicted by the logarithmic law at heights of around 200 m. However, they suggest that this relates to an internal boundary layer forming over land. This enhanced vertical wind speed gradient in

the YSU simulation is located at heights not relevant for current wind turbines. More relevant for the analysis of shear is a small derivation from the logarithmic wind profile in the MYNN simulation. The slope of the semi-log wind profile is higher between the first and the second model layer than above. ~~The difference is only slightly detectable in Fig. 8a) at .~~ This change
515 in slope was more pronounced in model runs with larger vertical grid spacing (not shown). ~~The change in wind shear makes the analysis of wind shear using Eq. 2 sensitive to the selection of the heights z_1 and z_2 and to the vertical model resolution. The same analysis with a coarser vertical grid spacing, using the first instead of the second model level for z_1, resulted in increased wind shear values for the MYNN simulation (not shown). However, from the second model level upwards to all simulations closely follow a logarithmic wind profile and have a constant change in inflow angle with height. The qualitative differences in~~
520 ~~modeled shear and veer are therefore consistent for model heights above the second model level.~~ For completeness, we report on finding discontinuous profiles with the MYJ boundary layer scheme in simulations with more vertical model levels (WRF version 3.7.1, fixed domains, 80 vertical layers). The discontinuities were found between 40 and 300 m and appeared to be related to the fine vertical grid spacing. This gave an incentive to lower the number of vertical levels in the current study.

525 The maximal 10 m wind speed of the simulations lies within the given values of the two best track data sets. This shows that the maximum of the 10 m wind speed from a $2\,\mathrm{km}$ grid is a valid approximation for the maximal ~~ten-minutes~~ ten-minute sustained wind field. In contrast, the maximal wind speed in the ERA 5 reanalysis has ~~clearly~~ lower maximal wind speeds. Following Nolan et al. (2009b), a relative agreement between the simulated maximal wind speed and the ~~then-minute~~ ten-minute sustained wind field in the studied simulations is expected as explained subsequently. As seen in Fig. 11, the horizontal variability can be reproduced to scales of around $X = 15\,\mathrm{km}$. The fastest simulated wind speeds at $10\,\mathrm{m}$ are in the order of $WS = 40\,\mathrm{m\,s^{-1}}$ (see Fig. 7). The associated resolved simulated temporal resolution corresponds to $X/WS \simeq 6$ minutes. The effective spatial resolution of approximately 15 km corresponds to $7.5 \times$ the horizontal grid spacing (2 km in our simulations) in agreement with Skamarock (2004). The loss of variability on scales smaller than 15 km is related to horizontal diffusion in WRF (Skamarock, 2004).

535 The spectral slope of minus five-thirds found for both simulations and SAR data for wavelength larger than 15 km, agrees with Gage and Nastrom (1986). At smaller wavelengths, the spectral energy density in the SAR products increases with decreasing wavelength. This can be attributed to the superposition of three-dimensional turbulence on top of the mesoscale quasi-two-dimensional turbulence (Karagali et al., 2013; Larsén et al., 2016). The mean magnitude of the SAR spectra agrees best with the MYJ spectra for wavelengths larger than 15 km. However, the magnitude of the SAR spectra depends on what
540 typhoon area is covered in the SAR image and ~~of the analysed~~ on the analyzed time step. Because the area differs from the area covered by the simulation domain, comparing their magnitude provides only limited insight. Furthermore, the mean wind speed obtained by the SAR product might be subject to uncertainty, as SAR calibration over extreme wind areas is rare. In fact, SAR products with significantly higher wind speeds are given by Jackson et al. (2021). These were in good agreement with the JTWC best track data, as opposed to the here-used SAR product being closer to the JMA data set, which of course depends on
545 the algorithms for the specific SAR retrievals for their case.

5 Conclusions

Due to the potentially large influence on wind turbine loads, we analyze hub height wind speed, wind shear, and wind veer over the rotor plane. The horizontal distribution and variability of these parameters are analyzed in the eyewall and ~~rainband~~ outer cyclone region of typhoon Megi (2016) using a mesoscale modeling framework. To evaluate model uncertainty related to the boundary layer parametrization, three frequently used boundary layer schemes (MYJ, MYNN, and YSU) are analyzed in WRF(~~V4.4~~version 4.4).

Our analysis showed that:

1. All three simulations can reasonably reproduce the typhoon track and cyclone structure. The storm intensifies in all model realizations and the spread of the simulated storm intensity is comparable to the spread between best track data sets. With that, the spread between the models in wind speed, wind shear, wind veer and their variability can be regarded as model uncertainty.

2. ~~Simulated~~ The simulated hub height wind speed is sensitive to the boundary layer parametrization and its median varies between the schemes by ~~21% (7~~15 % (8 %) in the eyewall (~~rainband~~outer cyclone) region.

3. Regardless of the boundary layer parametrization the simulated median wind shear exponents (α) is smaller or equal to 0.11 ~~suggested~~ used in the extreme wind model in the IEC standards ~~(?)~~(IEC, 2019a). However, in the MYJ simulation, 43.6 % of the wind profiles in the eyewall region exceed 0.11. The simulated median wind shear is in good agreement with the study from Vickery et al. (2009), but ~~clearly~~ smaller than observed in coastal areas during tropical cyclone conditions (Tse et al., 2013; He et al., 2016). The difference in the median α between the simulations using different boundary layer schemes is ~~(~~2.5×10^{-2} (2.9×10^{-2}) in the eyewall region (~~rainband~~ outer cyclone region). This difference is small compared to the difference between the simulated offshore ~~typhoon~~ typhoons and observations over coastal areas (Tse et al., 2013; He et al., 2016).

4. Median wind veer is up to ~~(~~$1.7 \times 10^{-2\,\circ}\,\mathrm{m}^{-1}$ ($1.2 \times 10^{-2\,\circ}\,\mathrm{m}^{-1}$) in the eyewall (~~rainband)region and nearly constant in the lowest of the boundary layer~~outer cyclone). It is up to 18 % larger at the rotor bottom than at hub height. The simulated wind veer is relatively small compared to wind veer in moderate wind speed regimes. This stands in contrast to studies from Worsnop et al. (2017), Kapoor et al. (2020) and He et al. (2016) who found strong wind veer in tropical cyclone ~~simulations~~LES. The difference in wind veer between the ~~different simulations is (~~simulations with different boundary layer schemes is $3.0 \times 10^{-3\,\circ}\,\mathrm{m}^{-1}$ ($2.5 \times 10^{-3\,\circ}\,\mathrm{m}^{-1}$) in the eyewall (~~rainband) regionand small relative to the wind veer found in He et al. (2016), Worsnop et al. (2017) and Kapoor et al. (2020).~~ outer cyclone) region.

5. Spectral analysis of the three simulations with a 2 km horizontal grid spacing shows, that horizontal wind speed variability is resolved on scales larger than 15 km as expected. The variability is largest in the MYJ simulation followed by the YSU simulation and smallest in the MYNN simulation. The produced horizontal difference in variability between the three schemes is evident over the analyzed wavelength range (4-100 km). Because the spectral energy density decays less

with increasing wavenumber in the MYJ scheme, the difference in horizontal wind speed variability is most pronounced at the smallest resolved wavelengths.

6. ~~The distribution of shear and veer are nearly insensitive to the boundary layer schemes and the interquartile range varies up to 11% between the schemes.~~

7. Overall hub hight wind speed, wind shear, and wind veer are larger in the eyewall region than in the ~~rainband~~ outer cyclone region. Within the ~~rainband~~ outer cyclone region, a clear spatial organization of wind shear and veer is found along the spiraling rainbands. In fact, local maxima in shear and veer along the rainbands are larger than the maximal simulated values in the eyewall region. On the radially inward side of the rainbands, positive veering angles reach their maximum over the tropical cyclone structure. On the outward side, either small wind veering angles or backing (negative wind veer) dominate. Wind shear maxima and minima on scales of around 20 km alternate along the rainband. This spatial organization likely leads to rapid coherent changes in the wind profile at a possible wind turbine location.

Based on these conclusions ~~we suggest further investigating, 1.~~, further investigation is needed to address 1) how wind speed, shear, and veer in tropical cyclones evolve during landfall, ~~2.~~2) how much wind shear and wind veer vary between tropical cyclones with different intensities and radii, and ~~3.~~3) how much wind turbine load estimates based on the current IEC standard differ between load estimates based on the simulated wind speed, shear, and veer distributions.

Code and data availability. The source code of the WRF model is available at https://www.mmm.ucar.edu/models/wrf (Skamarock et al., 2021). WRF namelists used for the simulations are available at https://zenodo.org/records/10202995 (Müller, 2023). The ERA 5 data used as boundary conditions for the WRF simulation is available at https://doi.org/10.24381/cds.bd0915c6 (Hersbach et al., 2018). The JTWC best track data set is available at https://www.metoc.navy.mil/jtwc/jtwc.html?best-tracks (Chu et al., 2002) and the JMA best track data set is available from https://www.jma.go.jp/jma/jma-eng/jma-center/rsmc-hp-pub-eg/trackarchives.html. The SAR data is available at https://doi.org/10.11583/DTU.19704883.v1 (Badger et al., 2022).

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