



1 **Fractal-based numerical simulation of multivariate typhoon wind speeds**
2 **utilizing Weierstrass Mandelbrot function**

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18 **Abstract:** This paper proposes a fractal-based technique for simulating multivariate nonstationary
19 wind speed fields by the stochastic Weierstrass Mandelbrot function. Upon conducting a systematic
20 fractal analysis, it was found that the structure function method is more suitable and reliable than the
21 box counting method, variation method, and R/S analysis method for estimating the fractal dimension
22 of the stochastic wind speed series. Wind field measurement at the meteorological gradient tower with
23 a height of 356 m in Shenzhen was conducted during Typhoon Mangkhut (2018). Significant non-
24 stationary properties and fractal dimensions of typhoon wind speed data at various heights were
25 analyzed and used to demonstrate the effectiveness of the proposed multivariate typhoon wind speed
26 simulation method. The multivariate wind speed components simulated by the proposed fractal-based
27 method are in good agreement with the measured records in terms of the fractal dimension, standard
28 deviation, probability density function, wind spectrum and cross-correlation coefficient.



29 **Keywords:** Fractal dimension; Structure function method; Simulation of multivariate nonstationary
30 wind speeds; Weierstrass Mandelbrot function;

31 **1 Introduction**

32 Many patterns observed in nature, i.e. snowflake, involve invisible recurrent layers that are
33 connected through a scaling factor, resulting in self-similarity across different scales. This creates a
34 cascade of activity that repeats at smaller scales (Shlesinger, 1990). Processes with this feature were
35 regarded as fractals (Mandelbrot, 1983, 1994). It is worth noting that fractals focus on the
36 representation of complex physical systems that cannot be appropriately demonstrated in the
37 framework of Euclidean terms. The fractal dimension, which quantifies the degree of self-similarity in
38 natural processes, is a fundamental parameter for investigating the underlying simplicity in the
39 organization of these processes (Rubalcaba, 1997).

40 The fractal dimensional analysis on wind speed time series has received increasing attention
41 (Sakamoto et al., 2007; Chang et al., 2012; Fortuna et al., 2014; Harrouni, 2013, 2018; Cadenas et al.,
42 2019). At present, there are several algorithms available for estimating the fractal dimension of a given
43 wind speed time series, including the box counting method (Sarkar and Chaudhuri, 1994; Breslin and
44 Belward, 1999; Fortuna et al., 2014; Cadenas et al., 2019; Shu et al., 2021), variation method (Dubuc
45 et al., 1987; Syu and Kirchhoff, 1993), R/S analysis method (Peters, 1991; Zhong et al, 2012; Jiang et
46 al., 2017), and structure function method (Ganti and Bhushan, 1995; Zhong et al, 2012; Wang and
47 Xiang, 2013). Syu and Kirchhoff (1993) employed the variation method to obtain a fractal dimension
48 of 1.60 ± 0.03 for six different wind speed records from Altamont. Li et al (2001) calculated the fractal



49 dimension of the high-frequency part of the wind turbulence signal using the variation method and
50 found that it had a fixed dimension of 1.7 in average, which indicates a clear self-similarity feature of
51 the wind speed time history record. Sakamoto et al (2007) applied the Higuchi method (Higuchi, 1988)
52 and obtained the fractal dimensions, i.e., 2, 1.9 and 1.7 for the upwind, easterly and northerly winds,
53 respectively. Chang et al. (2012) found that the annual mean fractal dimension values extracted by the
54 box counting method ranged between 1.61 and 1.66. Tijera et al. (2012) observed that the fractal
55 dimensions of horizontal and vertical velocity fluctuations at different heights (5.8 m, 13.5 m, and 32
56 m) using the box counting method ranged from 1.30 to nearly 1.00. Harrouni (2013) used the
57 rectangular coverage method to collect the fractal dimension of daily wind speed series and found that
58 the average dimension for one year was 1.92. Fortuna et al. (2014) reported average fractal dimension
59 values of 1.19 and 1.41 for daily and hourly mean wind speeds, respectively, using mono-fractal, multi-
60 fractal, and power spectra approaches. It is evident that the estimation of the fractal dimension of the
61 wind speed records shows significant discrepancy due to the different methods used. Therefore, there
62 is a pressing need to find a suitable method for estimating fractal dimensions in practical applications,
63 and it is necessary to conduct a detailed comparative analysis of methods for fractal dimension
64 estimation.

65 Additionally, generating wind speed time series numerically is a topic of great interest in many
66 engineering applications, such as structural dynamic analysis, reliability estimation, fragility analysis
67 and resilience assessment in structural wind engineering design (Huang et al. 2020). Various methods
68 for generating time series of wind speed have been proposed, including the harmonic superimposing
69 method (HSM) (Shinozuka and Jan, 1972), linear filtering method (Mignoler and Spanos, 1987), fuzzy



70 set theory (Zhu et al., 2011), neural network techniques (Olaofe, 2014), support vector machines (Liu
71 et al., 2014), Kalman filtering method (Chen et al., 2014), and time-mapping technique (Yassin et al.,
72 2023). In wind engineering field, HSM has been widely used due to its simplicity and effectiveness. It
73 is noteworthy that these methods were developed by modelling the intrinsic characteristics of turbulent
74 wind (Shinozuka and Jan 1972; Yassin et al. 2023) or employing new kind of regression methods
75 (Mignoler and Spanos 1987; Chen et al. 2014). However, none of them could fully capture the fractal
76 characteristics of wind speed time series. Therefore, further research is needed to explore wind speed
77 simulation methods that incorporate fractal characteristics. For this purpose, the Weierstrass
78 Mandelbrot (WM) fractal function method is a suitable candidate, as it has been increasingly studied
79 and utilized to simulate fractal surface profiles due to its ability to describe the fractal characteristics
80 of time series (Berry and Lewis, 1980; Majumdar et al., 1990,1991; Ganti and Bhushan, 1995; Wang
81 and Xiang, 2013). Humphrey et al. (1992) used the deterministic multi-fractal WM function with
82 fractal dimensions of 1.95 and 1.62 to simulate the turbulent velocity records in the case of high-speed
83 flow over an obstruction. Barszcz et al. (2012) developed a wind speed modelling method based on a
84 deterministic WM function. Due to the randomness of wind, stochastic WM functions are more
85 appropriate for simulating turbulent wind speed time series than the deterministic WM functions. Liu
86 et al. (2013) discussed the use of stochastic WM function to simulate fractal wind fluctuations with a
87 constant fractal dimension of 1.7. Wu et al. (2015) employed the stochastic WM function to simulate
88 fluctuating wind speeds, and compared the results to the observed wind speed data in terms of fractal
89 dimension, probability distribution, power spectrum, and cross-correlation coefficients. Lyu et al.
90 (2018) proposed a combined simulation method based on weighted amplitude wave superposition and



91 stochastic WM function, but with a fixed fractal dimension of 1.7. Since the fractal dimension of wind
92 speed time series can vary with different wind conditions, it is recommended in this work to employ
93 stochastic WM functions with varying fractal dimensions for numerical simulation of wind speed time
94 series. Furthermore, natural winds may not satisfy the stationary assumption when dealing with wind
95 speed data during extreme weather conditions, i.e., typhoon, thunderstorms or tornadoes (Cai et al.
96 2022). The current fractal-based simulation method is lack of ability to capture the nonstationary
97 feature of wind speeds. In this paper, a new fractal-based numerical simulation method is developed
98 for generating multivariate nonstationary typhoon wind speeds.

99 The paper is organized as follows: Section 2 firstly discusses the fractal-dimension estimation
100 methods, then the stochastic WM function-based numerical simulation method (SWM method) is
101 proposed for synthesizing multivariate nonstationary typhoon wind speeds. Section 3.1 provides
102 details on the wind speed data collected during Typhoon Mangkhut. Section 3.2 compares the fractal
103 dimensions estimated by various methods for typhoon wind speed data recorded at different heights.
104 Section 3.3 presents the numerical simulation results of typhoon wind speeds using the proposed
105 fractal-based SWM method. Finally, some concluding remarks are provided in Section 4.

106 **2 Methodology**

107 **2.1 Fractal Analysis**

108 This section aims to compare the following four commonly used methods, i.e., the box counting
109 method, variation method, R/S analysis method and structure function method, based on their
110 performance in estimating fractal dimension of the stochastic WM functions. Its goal is to identify and



111 recommend the most appropriate fractal dimension estimation method for wind speed data.

112 **2.1.1 Methods for estimating fractal dimensions of wind speed series**

113 The box counting method mainly consists of placing the wind speed time series with grids, and
114 then counting the number of non-overlapping boxes completely covering the time series. The
115 relationship between the number of boxes, $N(L)$, and the width of the box, L , can be given by

$$N(L) \propto L^{-D} \quad (1)$$

116 The dimension D can be computed by the least-square fit of the curve $\log_2(N(L))$ versus $\log_2(1/L)$.

117 The variation method was originally proposed by Dubuc et al (1987) as a means of estimating the
118 fractal dimension of rough surfaces. Given a wind speed time series $u(x)$, boxes with a bottom edge
119 length of 2ϵ are used to cover the series. The side edge of the box $v(x, \epsilon)$ is defined by

$$v(x, \epsilon) = \sup u(x') - \inf u(x'), \quad x' \in [x - \epsilon, x + \epsilon] \quad (2)$$

120 The ϵ variation $V(\epsilon, u)$ of wind speed $u(x)$ is then calculated as the sum of the areas of all the boxes,
121 given by

$$V(\epsilon, u) = \sum v(x, \epsilon) \cdot 2\epsilon \quad (3)$$

122 The fractal dimension D will be obtained from the least square line passing through the points
123 $(\log_2(1/\epsilon), \log_2(V(\epsilon, u)/\epsilon^2))$. The detailed procedures were presented in the reference by Syu and
124 Kirchhoff (1993).

125 For the purpose of determining the fractal dimension, the R/S analysis method employs the
126 following measures. At a given scale n , the mean value is calculated by

$$\bar{u}_n = \frac{1}{n} \sum_{x=1}^n u(x) \quad (4)$$

127 and the total accumulative deviation is given by



$$u(x, n) = \sum_{x=1}^n [u(x) - \bar{u}_n] \quad (5)$$

128 The extreme difference, $R(n)$, is obtained as

$$R(n) = \max_{1 \leq x \ll n} u(x, n) - \min_{1 \leq x \ll n} u(x, n) \quad (6)$$

129 Additionally, the standard deviation is

$$S(n) = \sqrt{\frac{1}{n} \sum_{x=1}^n [u(x) - \bar{u}_n]^2} \quad (7)$$

130 Using the relationship $R(n)/S(n) \propto n^H$ (Peters, 1991), the Hurst exponent H could be obtained by
131 linear fitting between the values $\log_2(n)$ and $\log_2(R(n)/S(n))$, and the fractal dimension is then given by
132 $D=2-H$ (Rehman and Siddiqi, 2009).

133 The structure function of order p was defined as

$$S_p(r) = \frac{1}{L-r} \int_0^{L-r} \{u(x+r) - u(x)\}^p dx, \quad (8)$$

134 where r is called the interval scale, which was originally introduced to describe the fine structure of
135 turbulence in fluid mechanics (e.g., Shivamoggi, 1995; Arenas and Chorin, 2006)). Later, it became a
136 popular tool for investigating surface roughness (e.g., Ganti and Bhushan, 1995). Notably, the order-2
137 structure function, $S(r)$, is closely related to the autocovariance function, R , through $S(r)=2\{R(0)-R(r)\}$,
138 and includes the same information as R and its power spectral density function, but provides more
139 practical merit (Thomas et al, 1999). For a fractal profile, the $S(r)$ is a function of the fractal dimension
140 D , with

$$S(r) \propto r^{4-2D} \quad (9)$$

141 After plotting the $\log_2(r)$ versus the value $\log_2(S(r))$ and fitting a line to the plot curve, the fractal
142 dimension is obtained by $D = (4 - K)/2$, where the K is the slope of the fitted line. The more detailed



143 process could be found in Thomas et al (1999) and Zhong et al (2012).

144 For a pure random sequence, it is easy to get that the structure function almost keeps constant for
145 each interval scale. This results in a zero slope of the fitted line, indicating a fractal dimension of 2 for
146 the concerned random sequence. On the other hand, if the series vary slowly over time, the fractal
147 dimension is close to unit with a constant slope of $K=2$.

148 **2.1.2 Comparison of the fractal dimension estimation methods based on the WM function**

149 To determine the most appropriate method for estimating the fractal dimension of wind speeds, it
150 is necessary to introduce the WM function with the known fractal dimension D . Notably, the WM
151 function is continuous but non-differentiable at all points and possesses no scale (Berry and Lewis,
152 1980), as follows

$$W(t) = \sum_{n(l)=-\infty}^{\infty} \frac{(1 - e^{i\gamma^{n(l)}t})e^{i\phi(l)}}{\gamma^{(2-D)n(l)}} \quad (1 < D < 2, \gamma > 1, \phi = \text{arbitrary phases}) \quad (10)$$

153 where D represents the fractal dimension of the graph of $W(t)$; The frequencies γ^n form a ‘Weierstrass
154 spectrum’, spanning the range from zero to infinity; The phases ϕ could be chosen to make $W(t)$ show
155 deterministic or stochastic behavior. Berry and Lewis (1980) reported that the deterministic formula
156 including cosine series or alternating sign sine series shows a tendency to increase gradually with time.
157 On the other hand, considering the random characteristic of wind, the stochastic WM function is thus
158 more suitable for simulating fluctuating wind speed time series with the mean equal to zero. Since $W(t)$
159 is complex, the stochastic real part $R(t)$ adopted in this study can be expressed as

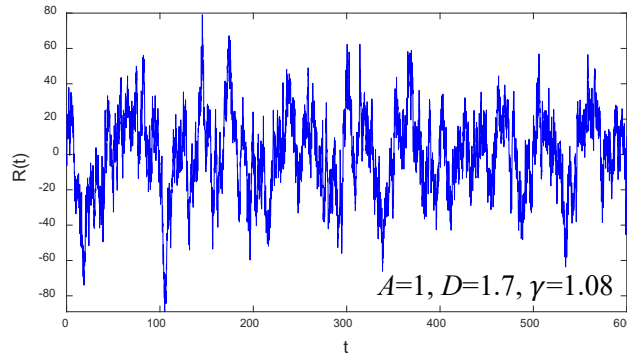
$$R(t) = A \sum_{n(l)=-\infty}^{\infty} \frac{\cos(\phi(l)) - \cos(\gamma^{n(l)}t + \phi(l))}{\gamma^{(2-D)n(l)}} \quad (1 < D < 2, \gamma > 1) \quad (11)$$

160 where ϕ is taken as a set of random numbers ranging from 0 to 2π ; A is an amplitude parameter to



161 be determined. The parameter γ of the WM function determines the density of the spectrum and the
162 relative phase differences between the spectral modes (Majumdar and Tien, 1990). It is suggested to
163 be 1.08 for the parameter γ in order to provide dense spectral information (Berry and Lewis, 1980).
164 For a given fractal dimension, Eq. (11) provides an efficient way to simulate random time series. More
165 details of simulation will be discussed in Section 2.3.

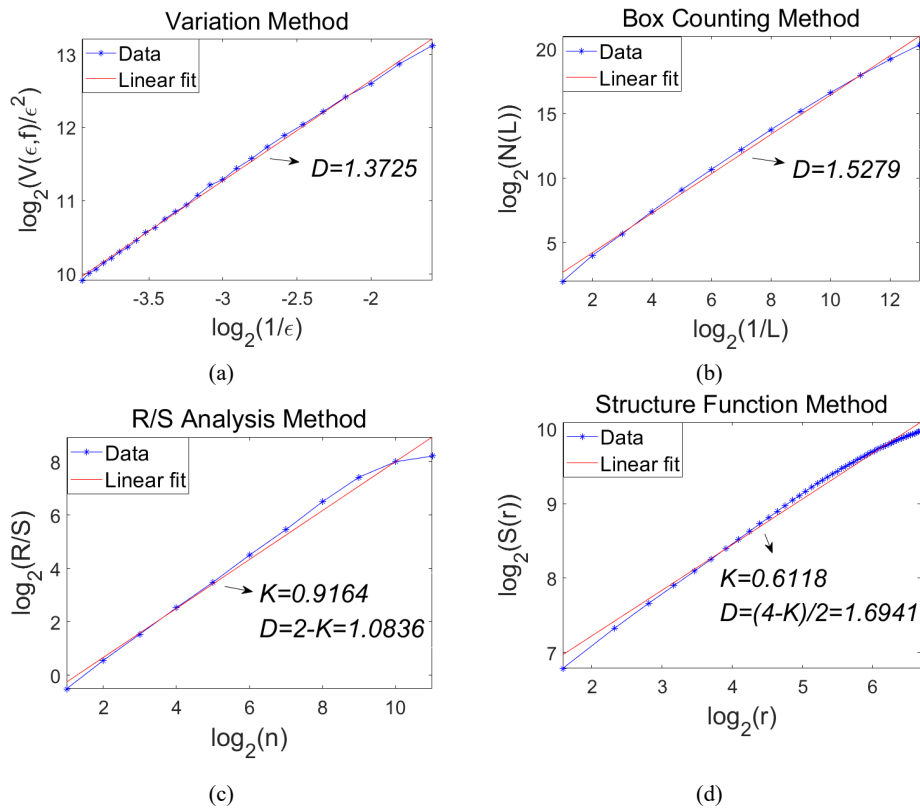
166 For this comparison study, a fractal dimension of 1.7, which is the common value for wind speed
167 series reported in the literature (Li et al., 2001; Cui et al., 2022), was applied in Eq. (11) to generate
168 the time series, as shown in Fig. 1. Four estimation methods were then used to estimate the fractal
169 dimension of the generated time series of Fig. 1, and the log-scale fitting plots corresponding to four
170 estimation methods were presented in Fig. 2. Fig. 2 shows that the structure function method provides
171 the most accurate result of 1.6941 with the smallest relative error of 0.35%. By randomly sampling the
172 phase number \emptyset in Eq. (11), 50 different time series have been generated with the same set of
173 parameters (i.e., $A=1$, $D=1.7$ and $\gamma=1.08$). Fig. 3 presents the estimated results of fractal dimensions
174 for 50 generated time series samples. The structure function method consistently obtained the best
175 estimates around 1.7 compared to other three methods, i.e., box counting method, variation method
176 and R/S analysis method. For a range of fractal dimensions from 1.4 to 1.8, different time series were
177 also generated by Eq. (11), and the fractal dimensions were estimated respectively by four methods
178 and reported in Fig. 4 against the given values. As shown in Fig. 4, the structure function method is
179 the most accurate method to estimate the fractal dimension of a given time series.



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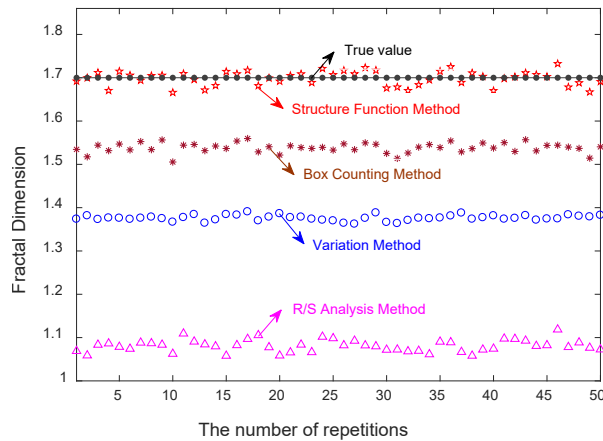
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Fig. 1 The generated stochastic function time series



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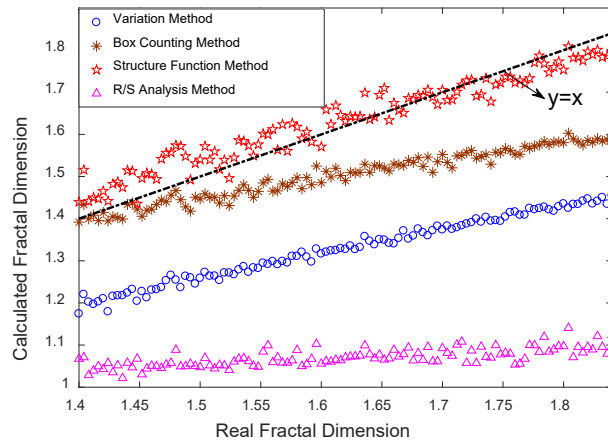
Fig. 2 Log-scale fitting plots corresponding to four fractal dimension estimation methods



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Fig. 3 Estimation results of fractal dimensions for 50 generated time series samples



185

186

Fig. 4 The estimated fractal dimensions with the actual value

187 **2.2 Time-varying mean of a non-stationary time series**

188 In extreme wind environments, such as tropical cyclones, thunderstorms, downbursts, and strong
 189 winds, the wind speed history exhibits significant non-stationary characteristics (Gurley and Kareem,
 190 1997; Wood et al., 2001; Pinelli et al., 2004; Jung and Masters, 2013; Solari et al., 2015). Therefore,
 191 the associated overall wind speed series in these environments need to be considered as the sum of the
 192 time-varying mean (TVM) component (i.e., non-fractal component, reflecting the non-stationarity of



193 the extreme wind speed field) and the fluctuating component (fractal component). Additionally, the
194 adopted WM function $R(t)$ is a zero-mean Gaussian random function because it is the sum of infinite
195 terms with random phases (Guariglia, 2017). Therefore, for simulation of non-stationary wind speeds,
196 the TVM of the overall wind speed time series should be firstly determined by an appropriate method.
197 It is desirable that the de-trended wind speed fluctuation components remain zero-mean over the entire
198 length of the time series.

199 Cai et al. (2022) proposed a wavelet transform-based method for determining the TVM of non-
200 stationary wind speed series. The measured wind speed time series $U(t)$ can be decomposed as the sum
201 of several detail functions $D_j(t)$ and the approximation function $AF(t)$ (Cai et al. 2022)

$$U(t) = \sum_{j=1}^M D_j(t) + AF(t) \quad (12)$$

202 where M represents the total number of decomposition levels. A series of TVMs of $U(t)$ can be
203 characterized as the superimposition of the approximation function $AF(t)$ and N (non-negative
204 integer) detail functions $D_j(t)$ of the original wind speed series as

$$TVM_N = \begin{cases} AF(t), & N = 0 \\ \sum_{j=M+1-N}^M D_j(t) + AF(t), & 1 \leq N \leq M - 1 \end{cases} \quad (13)$$

205 Subsequently, the relative fluctuating component $u(t)$ of the original wind speed $U(t)$ can be obtained
206 by subtracting the derived TVMs from the original wind speed series, as follows

$$u(t) = \sum_{i=1}^{M-N} D_i(t) \quad (14)$$

207 According to conditions proposed by Cai et al (2021a, 2021b), the optimal TVM for a wind speed
208 series with a 10-minute time interval has adequate local maxima points but less than six. For better



209 characterizing natural wind, stationary or nonstationary wind models could be classified based on the
 210 use of constant mean wind speed or the TVM in decomposing wind speed data (Cai et al. 2022).

211 2.3 Univariate simulation of fluctuating wind speeds

212 For practice, numerical implementation of Eq. (11) with finite terms can be approximated as

$$R(t) = A \sum_{l=l_{min}}^{l_{max}} \frac{\cos(\phi(l)) - \cos(\gamma^{n(l)}t + \phi(l))}{\gamma^{(2-D)n(l)}} \quad (15)$$

$$(\gamma^{n(l_{min})} = 2\pi f_{min}, \gamma^{n(l_{max})} = 2\pi f_{max})$$

213 where n_{min} and n_{max} could be determined by the minimum and maximum cut-off frequencies of
 214 the fluctuating wind speed spectrum, respectively. According to Cai et al. (2021a, 2021b), the main
 215 frequency of optimal TVM is slightly below 0.01Hz. Thus, n_{min} could be approximated as
 216 $n(l_{min}) = \ln(2\pi f_{min})/\ln\gamma = -35.96$. For wind engineering practice, a sampling frequency of 10 Hz
 217 is normally adopted for full-scale measurements and numerical simulation of turbulent wind. Due to
 218 Nyquist-Shannon sampling theorem, the maximum cut-off frequency of the wind speed signal is 5 Hz.
 219 Consequently, $n(l_{max})$ could be estimated as $\ln(2\pi f_{max})/\ln\gamma = 44.79$.

220 For the stochastic WM function $W(t)$, its time-average correlation $\langle |W(t + \tau)W^*(t)| \rangle_t$ is

$$\langle |W(t + \tau)W^*(t)| \rangle_t = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T W(t + \tau)W^*(t) dt \quad (16)$$

221 The power spectrum $S(\omega)$ is proportional to the Fourier transform of the $\langle |W(t + \tau)W^*(t)| \rangle_t$, and
 222 is presented, apart from a zero-frequency term, by

$$S(\omega) = \sum_{n(l)=-\infty}^{\infty} \frac{\delta(\omega - \gamma^{n(l)})}{\gamma^{(4-2D)n(l)}} \quad (17)$$

223 After averaging discrete spectrum $S(\omega)$ over a range $\Delta\omega$ including Δn frequencies γ^n , a
 224 continuous spectrum $\hat{S}(\omega)$ of the stochastic WM function can be obtained as

$$\hat{S}(\omega) = \frac{1}{\Delta\omega} \int_{-\frac{1}{2}\Delta\omega}^{\frac{1}{2}\Delta\omega} S(\omega + \omega') d\omega' \approx \frac{\Delta n}{\Delta\omega \gamma^{(4-2D)n\omega}}, \quad (18)$$



225 where $n_\omega = \frac{\ln(\omega)}{\ln(\gamma)}$. This leads to $\frac{dn_\omega}{d\omega} = \frac{1}{\omega \cdot \ln(\gamma)}$, so that

$$\hat{S}(\omega) \approx \frac{dn_\omega/d\omega}{\gamma^{(4-2D)n_\omega}} = \frac{1}{\ln\gamma \cdot (\omega)^{5-2D}} \quad (19)$$

226 The detailed derivation process is available in Berry and Lewis (1980). When the spectrum is inferred
 227 in the Hertz instead of the radian ω of Eq. (19), associated continuous Weierstrass spectrum $\hat{S}(f)$ is
 228 given as follows

$$\hat{S}(f) \approx \frac{2\pi}{\ln\gamma \cdot (2\pi f)^{5-2D}} \quad (20)$$

229 . As a result, the continuous Weierstrass spectrum $S_R(f)$ of the adopted stochastic real part of $W(t)$,
 230 presented in Eq. (15), is approximately estimated as

$$S_R(f) = A^2 \hat{S}(f) \approx \frac{2\pi \cdot A^2}{\ln\gamma (2\pi f)^{5-2D}} \quad (21)$$

231 Additionally, a general expression of the wind spectrum $S_u(f)$, given by Olesen et al (1984), was
 232 employed as the target spectrum of wind field simulation, as follows

$$\frac{f S_u(f)}{u_*^2} = \frac{a f_n^e}{(1 + b f_n^c)^d} \quad (f_n = \frac{fz}{\bar{U}}) \quad (22)$$

233 Where \bar{U} denotes the 10-min mean wind speeds; z is the height of the simulation point; u_* is the
 234 friction velocity; a, b, c, d and e are constants, depending on the atmospheric conditions. A
 235 coefficient $g(A)$ is newly defined to quantify the difference between the simulated wind spectrum
 236 and target spectrum of the fluctuating wind component, given by

$$g(A) = \sum_f (S_R(f) - S_u(f))^2 \quad (23)$$

237 After calculating the derivative of $g(A)$ with respect to A^2 , Eq. (24) can be directly obtained.

$$\frac{\partial}{\partial(A^2)} g(A) = \sum_f 2 (A^2 \hat{S}(f) - S_u(f)) \hat{S}(f) \quad (24)$$

238 By taking $\frac{\partial}{\partial(A^2)} g(A) = 0$, the amplitude parameter A is computed as



$$A = \sqrt{\frac{\sum_f S_u(f) \cdot \hat{S}(f)}{\sum_f (\hat{S}(f))^2}} \quad (25)$$

239 Then the univariate fluctuating wind speed time histories can be simulated by Eq. (15).

240 **2.4 Multivariate synchronous simulation of wind speeds**

241 Unlike the univariate wind speed simulation, the spatial correlations of wind velocity field should
 242 be accounted for the multivariate synchronous simulation of wind speeds (Huang et al, 2020). For this
 243 purpose, a following novel way was developed.

244 The commonly used cross-correlation coefficient to evaluate the correlation of synchronous wind
 245 speed time histories (i.e., $X_j(t)$ and $X_k(t)$) at two measured points (P_j and P_k) was given by

$$\rho_{jk} = \frac{E\{[X_j(t) - m_j(t)][X_k(t) - m_k(t)]\}}{\sqrt{E\{[X_j(t) - m_j(t)]^2\}E\{[X_k(t) - m_k(t)]^2\}}} \quad (26)$$

246 where $m_j(t)$ and $m_k(t)$ denote the constant means or TVM of wind speed time histories.

247 Assume that the univariate simulation of fluctuating wind speeds has been implemented by Eq.
 248 (15) at the first point P_j , and corresponding phase parameter ϕ_j has been temporarily stored. At this
 249 situation, the synchronous simulation at the second point P_k can be carried out by introducing a
 250 Gaussian random sequence φ with zero mean and standard deviation of σ_φ (i.e., $\varphi \sim N(0, \sigma_\varphi^2)$) in
 251 Eq. (15), as follows

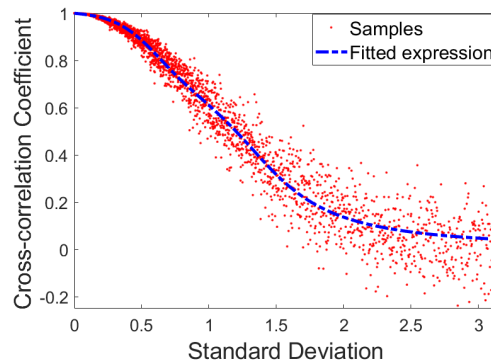
$$R_k(t) = A_k \sum_{l=l_{min}}^{l_{max}} \frac{\cos(\phi_j(l) + \varphi(l)) - \cos(\gamma^n t + \phi_j(l) + \varphi(l))}{\gamma^{(2-D_k) \cdot n(l)}} \quad (27)$$

252 where A_k is the amplitude parameter estimated by Eq. (15); D_k is the fractal dimension of wind
 253 speed series at the second point P_k . The value of $(\phi_j + \varphi)$ was converted to $[0 \ 2\pi]$ by applying the
 254 expression $\phi_j + \varphi - 2\pi \cdot \text{floor}(\frac{\phi_j + \varphi}{2\pi})$, where $\text{floor}(x)$ devotes the floor function and returns the
 255 greatest integer less than or equal to x . If the standard deviation parameter σ_φ of Gaussian distribution



256 approaches zero, the phase difference between $(\phi_j + \varphi)$ and (ϕ_j) becomes negligible, resulting in
 257 a perfect correlation between simulated fluctuating speed time histories at points $(P_j$ and $P_k)$ by using
 258 Eq. (15) and Eq. (27), respectively. Consequently, their cross-correlation coefficient ρ_{jk} computed
 259 using Eq. (26) approaches the unity. Additionally, as σ_φ increases, the larger phase difference φ
 260 weakens their correlation, leading to a smaller ρ_{jk} until they become irrelevant. To investigate this
 261 relationship, 10000 samples of σ_φ were taken from 0 to π , and corresponding variation of ρ_{jk} with
 262 the standard deviation parameter σ_φ was plotted in Fig. 5. The figure clearly shows a decreasing trend
 263 of ρ_{jk} with increasing σ_φ , and a fitted expression is provided as

$$\rho = \frac{1}{\pi} \arctan \left(-\frac{7}{6} \alpha^3 - \frac{1}{8} \alpha^2 - \frac{5}{4} \alpha + \frac{9}{25} \right) + \frac{1}{2} \quad (\alpha = \log_2(\sigma_\varphi)) \quad (28)$$



264

265 Fig. 5 The variation of cross-correlation coefficient ρ_{jk} with the standard deviation parameter σ_φ

266 It is easy to obtain that the value of ρ in Eq. (28) falls between 0 and 1, and decrease with the
 267 increase of σ_φ after proving $\partial\rho/\partial\alpha < 0$. So far, once the synchronous wind speed data was
 268 measured at two different spatial points P_k and P_j , ρ_{jk} can be easily calculated using Eq. (26). The
 269 corresponding unique value of σ_φ can then be determined by taking the inverse of Eq. (28), enabling
 270 the implementation of multivariate wind velocity field simulation using Eq. (15) and Eq. (27). It should
 271 be noted that if the estimated correlation of ρ_{jk} for the measured wind speed data sample is negative,



272 the expression of fluctuating wind speed in Eq. (27) could be modified by adding the phase π in Eq.
273 (27), as follows

$$R_k(t) = A_k \sum_{l=l_{min}}^{l_{max}} \frac{\cos(\phi_j(l) + \varphi(l) + \pi) - \cos(\gamma^{n(l)}t + \phi_j(l) + \varphi(l) + \pi)}{\gamma^{(2-D_k)n(l)}} \quad (29)$$

274 where the associated standard deviation σ_φ of Gaussian distribution φ was derived by taking the
275 inverse of Eq. (28) as $\rho = -\rho_{jk}$ was set.

276 It is worth noting that if measured wind speed data is not available, the classical spectra known
277 as the Davenport spectrum (Davenport, 2010), von Karman spectrum (Von Karman, 1948), Simiu
278 spectrum (Simiu and Scanlan, 1996), or Harris spectrum (Harris, 1968) can be considered as the target
279 spectrum in Eq. (22). In such situation, the mean fractal dimension $D=1.75$ estimated by the structure
280 function method in the following section 3.2 is suggested for use in Eq. (15), Eq. (27), and Eq. (29) to
281 simulate the wind speed field.

282 The detailed multivariate synchronous simulation of wind speed time histories in this paper
283 mainly includes the following steps, as shown in Fig. 6.

284 Step 1. To check the stationarity of the wind speed sample using the run test (Rouillard, 2014).
285 Subtract the constant mean component to obtain the fluctuating wind speed for stationary data, and
286 subtract the time-varying mean component for non-stationary sample.

287 Step 2. To estimate each fractal dimension D (D_k and D_j) of fluctuating wind speeds at two
288 different points (P_k and P_j) by using the structure function method.

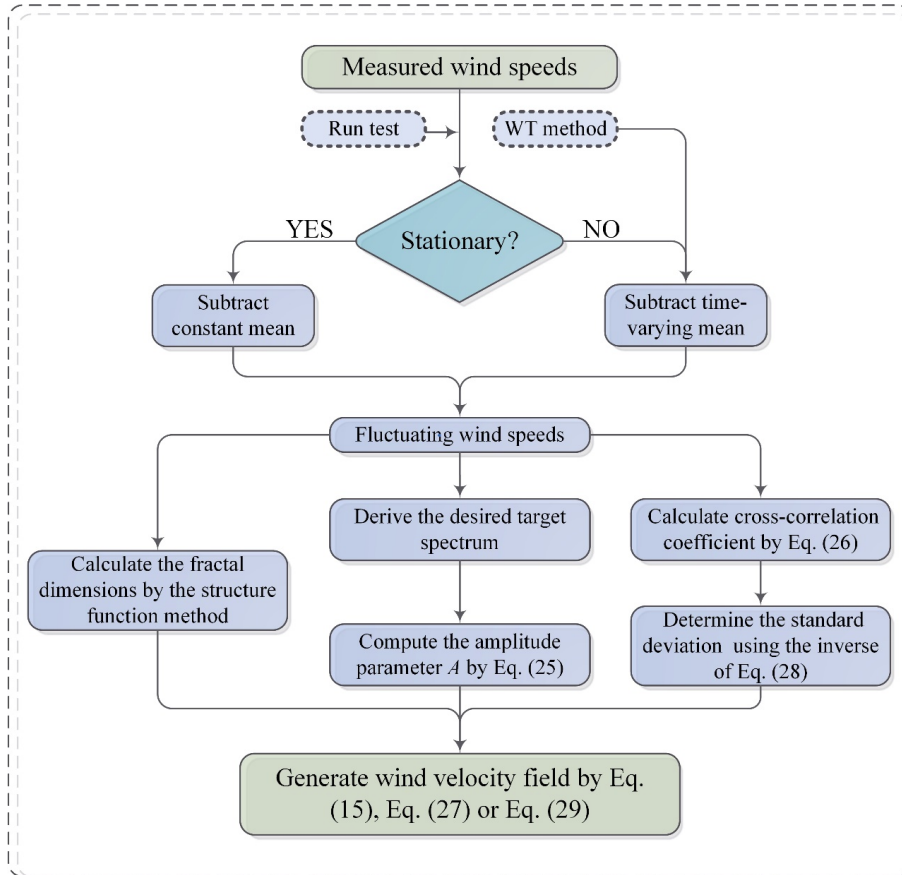
289 Step 3. To derive the desired target spectrum $S_u(f)$ based on the measured wind speed data, and
290 determine the parameter A (A_k and A_j) by Eq. (25).

291 Step 4. To simulate the fluctuating wind speed at reference point P_j by Eq. (15), and record the



292 phase parameter ϕ_j at this step.

293 Step 5. To evaluate the cross-correlation coefficient ρ_{jk} of measured fluctuating wind speeds at
 294 two points P_k and P_j ; determine the standard deviation σ_ϕ using the inverse of Eq. (28); generate a
 295 Gaussian random sequence $\phi \sim N(0, \sigma_\phi^2)$, and then simulate synchronous fluctuating wind speed time
 296 series at the point P_k by Eq. (27) for $\rho_{jk} < 0$ or Eq. (29) for $\rho_{jk} > 0$.



297

298 Fig. 6 Flowchart of the multivariate synchronous simulation of wind speeds

299 3 Results and discussions

300 3.1 Data source and description



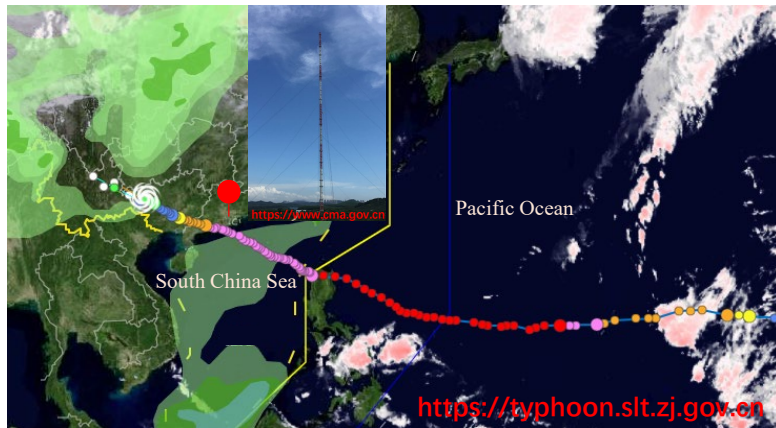
301 The wind speed data in this study were continuously recorded by four three-dimensional (3D)
302 sonic anemometers during the occurrence of super typhoon Mangkhut from September 15 to
303 September 18, 2018. The recorded data consists of 526 consecutive 10-minute wind speed samples,
304 with an accuracy of ± 0.1 m/s. Four sonic anemometers were installed at the meteorological gradient
305 tower with a height of 356 m in Shenzhen, China (22°38'59"N, 113°53'36"E), as shown in Fig. 7.
306 The technical parameters of the sonic anemometers and their install heights are detailed in Table 1.

307 Typhoon Mangkhut initiated as a tropical depression at 12°N, 170°E and ultimately made landfall
308 over Guangdong, China, on September 16, before moving inland. The associated typhoon track is
309 presented in Fig. 7. The means of longitudinal wind speed data with a fixed period of 10 min during
310 the passage of Mangkhut were recorded at length, as shown in Fig. 8. It is evident that the mean wind
311 speed increases gradually with the increase of recorded heights. Maximum wind speeds were
312 synchronously recorded for four anemometers around 14:00, on September 16, with a maximum of 35
313 m/s at the height of 320 m.

314 Table 1 Key parameters of the sonic anemometers.

Instrument	Measured height	Observation content	Sampling frequency	Measured range	Accuracy
CSAT3 3D sonic anemometers	10 m, 40 m, 160 m, and 320 m above the ground level	Three directional wind components and sonic virtual temperature	10Hz	0-75 m/s	± 0.1 m/s

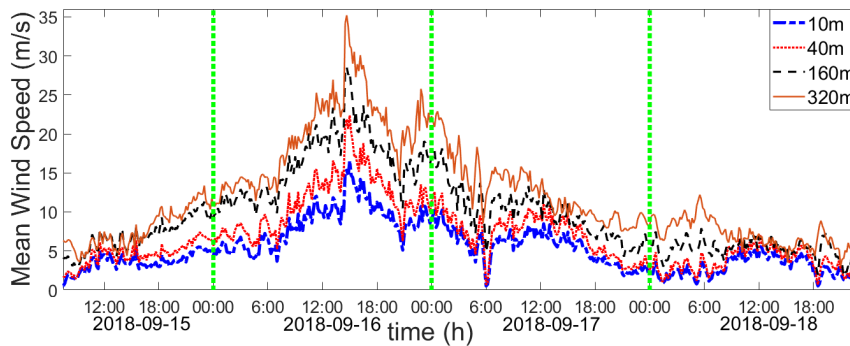
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316

317

Fig. 7 The location and ambient terrain of the meteorological gradient tower and the track of typhoon Mangkhut



318

319

Fig. 8 10-min longitudinal mean wind speeds at each height

320 3.2 Analysis of fractal dimensions

321 The fractal dimensions of the longitudinal fluctuating wind speed data during super typhoon
322 Mangkhut were estimated for both stationary and nonstationary wind models. Fig. 9 shows the
323 variation of the relative frequency value (RF-value) of obtained fractal dimensions, where the numbers
324 marked on the X axis are middle values of segment intervals. Furthermore, the difference values (D-
325 value) between corresponding RF-values utilizing stationary and nonstationary wind models lie in the
326 bottom line of each subgraph in Fig. 9. The zoom-in views of bottom graphs in the Fig. 9(a) and Fig.
327 9(d) are respectively presented in the interval of $[-0.02, 0.02]$ and $[-0.04, 0.04]$ to provide a more detailed
328 view. As shown in Fig. 9(a) and (d), the results of estimated fractal dimension seem no obvious



329 difference between stationary and nonstationary wind models when applying variation method or
330 structure function method. On the other hand, if box counting method or R/S analysis method is used,
331 significant difference of estimated fractal dimension could be observed between stationary and
332 nonstationary models, as shown in Fig. 9(b) and (c). Relevant statistical parameters including mean,
333 standard deviation, maximum and minimum values of fractal dimensions are given in Table 2. Fig. 10
334 presents the mean fractal dimensions by averaging results corresponding to four measurement heights.
335 Additionally, fractal dimension estimations using the same types of methods by other researchers are
336 reported in Table 3 for further comparison.

337 According to the findings presented in Fig. 9, there are notable discrepancies in the fractal
338 dimensions obtained from different methods. The variation method yielded a smaller fractal dimension
339 than the box counting method for the same Typhoon wind speed data depicted in Fig. 9(a) and Fig.
340 9(b). Its main concentration range of the fractal dimension is from 1.354 to 1.502, accounting for more
341 than 90%, and smaller than those calculated by Syu and Kirchhoff (1993) and Li et al (2001) for the
342 normal wind in Table 3 when the same variation method was adopted.

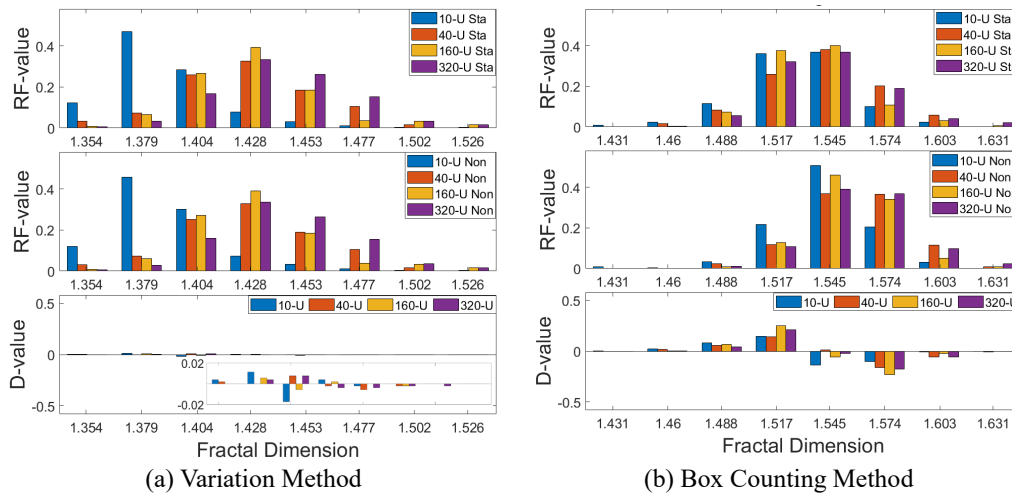
343 In the case of the box counting method, the mean fractal dimension of winds measured at four
344 heights of 10, 40, 160, and 320 m (i.e., 1.5296, 1.5412, 1.5351 and 1.5423) in Table 2 are close to the
345 values of seasonal monsoon reported by Shu et al. (2021) (i.e., 1.582, 1.570, 1.554 and 1.547) collected
346 from the same meteorological gradient tower. The fractal dimension estimated by the box counting
347 method for typhoon Mangkhut is ranged from 1.4026 to 1.6597, which are similar to the results given
348 by Chang et al (2012), Shu et al (2020), Yan et al (2020) and Cui et al (2022) as reported in Table 3.

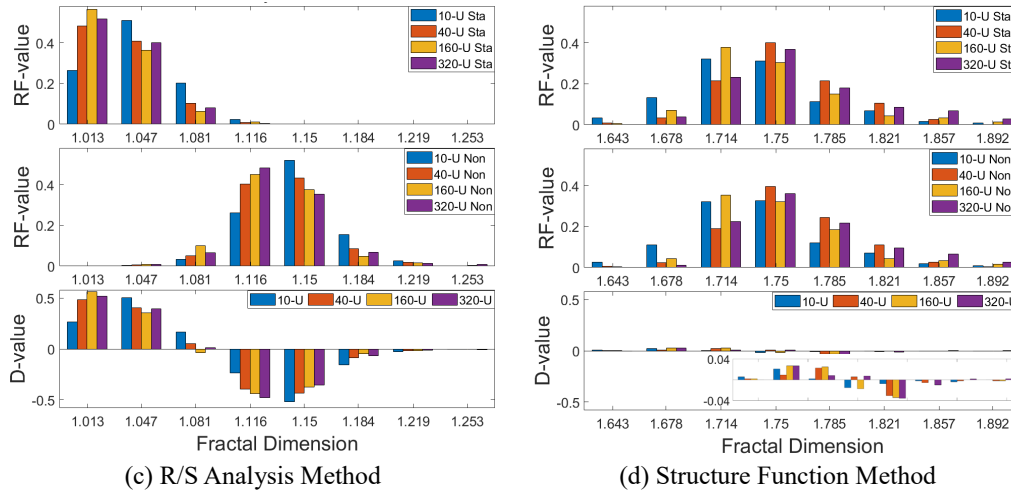
349 For the R/S analysis method, it produced a minimum estimate close to 1, as depicted in Fig. 9(c)



350 and Table 2. Although the fractal dimension obtained in this study was comparable to those reported
 351 by Tsekouras and Koutsoyiannis (2014) and Balkissoon et al. (2020), it was far lower than the values
 352 suggested by most of researchers in Table 3. Furthermore, since the extraction of TVM of nonstationary
 353 wind speeds greatly affects the dimension D obtained by the R/S analysis method from Fig. 9(c) and
 354 Fig. 10(c), it is not a reliable approach for determining fractal dimensions of wind speed series.

355 Regarding the structure function method, it yielded the mean fractal dimension of 1.7512 close to
 356 the representative value of 1.7. Additionally, the estimated fractal dimension by the structure function
 357 method is quite robust and insensitive to stationary or nonstationary wind models used. Therefore, it
 358 is reasonable to recommend the structure function method as the effective and reliable approach for
 359 estimating the fractal dimension of wind speed series.





(c) R/S Analysis Method

(d) Structure Function Method

360 Fig. 9 Relative frequency value of fractal dimensions of fluctuating wind speed samples at each measured height
 361 based on stationary and nonstationary wind models (Note: Sta: Stationary, Non: Nonstationary)
 362

363 Table 2 Statistical summary of fractal dimensions of 526 10-min wind speed samples at each measured height in
 364 longitudinal wind directions based on the stationary and nonstationary wind model

Measured height		10 m	40 m	160 m	320 m
		(Sta/Non)	(Sta/Non)	(Sta/Non)	(Sta/Non)
Structure Function Method	Mean	1.7374/1.7409	1.7575/1.7621	1.7453/1.7505	1.7647/1.7695
	Std	0.0461/0.0452	0.0405/0.0397	0.0469/0.0459	0.0516/0.0506
	Max	1.8800/1.8820	1.8730/1.8760	1.9100/1.9120	1.9270/1.9280
	Min	1.6069/1.6128	1.6316/1.6352	1.6470/1.6532	1.6723/1.6822
Box Counting Method	Mean	1.5296/1.5431	1.5412/1.5584	1.5351/1.5544	1.5423/1.5597
	Std	0.0289/0.0252	0.0298/0.0264	0.0256/0.0224	0.0288/0.0267
	Max	1.6068/1.6113	1.6180/1.6284	1.6334/1.6370	1.6372/1.6597
	Min	1.4137/1.4026	1.4466/1.4447	1.4704/1.4523	1.4514/1.4571
Variation Method	Mean	1.3907/1.3911	1.4272/1.4276	1.4278/1.4284	1.4401/1.4406
	Std	0.0246/0.0245	0.0308/0.0307	0.0292/0.0290	0.0299/0.0297
	Max	1.4940/1.4944	1.5428/1.5429	1.5356/1.5358	1.5508/1.5510
	Min	1.3299/1.3305	1.3458/1.3464	1.3430/1.3435	1.3564/1.3576
R/S Analysis Method	Mean	1.0474/1.1460	1.0342/1.1363	1.0306/1.1305	1.0327/1.1322
	Std	0.0239/0.0273	0.0228/0.0271	0.0231/0.0276	0.0228/0.0288
	Max	1.1162/1.2368	1.1177/1.2873	1.1308/1.2855	1.1217/1.2870
	Min	0.9942/1.0488	0.9784/1.0367	0.9899/1.0565	0.9822/1.0593

365
 366



367 Table 3 The fractal dimension estimation result for the wind speed data from different references

References	Applied method	Details about obtained fractal dimension	Type of wind
Syu and Kirchhoff (1993)	variation method	$D=1.60\pm 0.03$ for six different wind speed records from Altamont taken on different days	Normal wind
Li et al (2001)	variation method	average about 1.70	Normal wind
This study	variation method	Vary from 1.3299 to 1.5510	Typhoon wind
Barszcz et al (2012)	box counting method	mean fractal dimension of 1.3552 for the fluctuating wind speed	Normal wind
Chang et al (2012)	box counting method	Annual mean fractal dimension values ranging from 1.61 to 1.66	Normal wind
Tijera et al (2012)	box counting method	Fractal dimensions of 1.30 to nearly 1.00 for the 5-min horizontal and vertical velocity fluctuations	Normal wind
Fortuna et al (2014)	box counting method	$D=1.19$ for daily mean wind speeds $D=1.41$ for hourly mean wind speeds	Normal wind
Wu et al. (2015)	box counting method	$D=1.46, 1.35$ and 1.24 for the 10-min fluctuating wind speed at the measured height of 3.5 m, 6.5 m and 10 m, respectively.	Normal wind
Shu et al (2020)	box counting method	Mean fractal dimension varying from 1.31 at an offshore weather station to 1.43 at an urban station	Normal wind
Yan et al (2020)	box counting method	Daily fractal dimensions of 10-min wind speed time series estimated between 1.32 and 1.47 based on 6-year continuous anemometric data	Normal wind
Shu et al (2021)	box counting method	$D=1.582, 1.570, 1.554,$ and 1.547 for the 10-min vertical wind velocity of seasonal monsoon at the measured heights of 10, 40, 160, and 320 m, respectively.	Normal wind
Cui et al (2022)	box counting method	D varied from 1.55 to 1.75 for the measured 10-min horizontal wind speeds during the three typhoons landing (Typhoon Lionrock, Fanapi and Megi)	Typhoon wind
This study	box counting method	Vary from 1.4026 to 1.6597	Typhoon wind
Tsekouras and Koutsoyiannis (2014)	R/S analysis method	The majority of the D of wind speeds lying in the interval (1.1, 1.4)	Normal wind
Balkissoon et al (2020)	R/S analysis method	The fractal dimensions varying from 1.1 to 1.3 for the monthly wind speed time series.	Normal wind
This study	R/S analysis method	Vary from 0.9784 to 1.2873	Typhoon wind
This study	Structure Function Method	Vary from 1.6069 to 1.9280	Typhoon wind

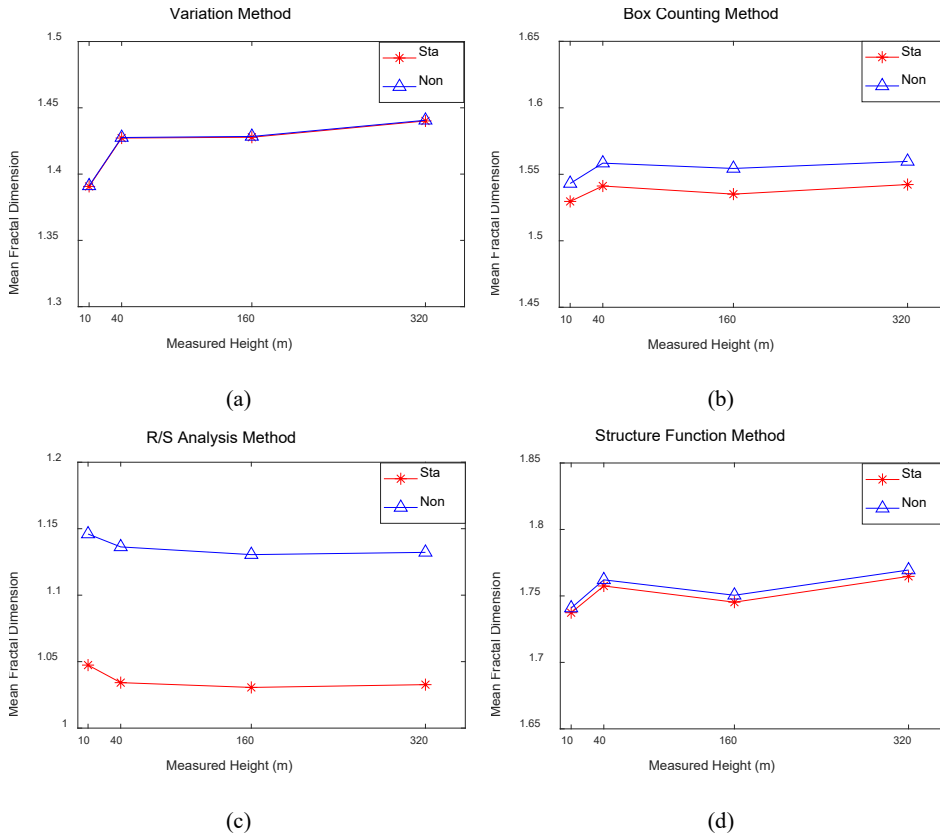


Fig. 10 Mean fractal dimensions under stationary and nonstationary wind models

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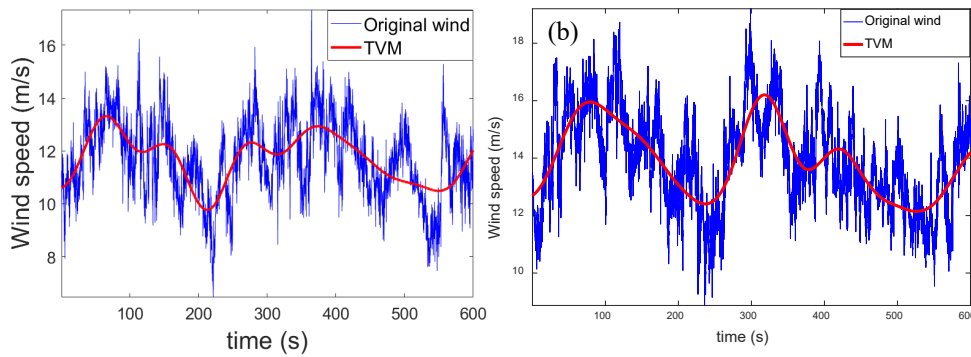
370 3.3 Simulation of fluctuating wind speeds

371 Fluctuating wind speeds at two heights of 160 m and 320 m were simulated based on two
 372 synchronously measured records. The optimal TVMs extracted by the wavelet transform-based method
 373 in section 2.2 are presented in Fig. 11 after determining that these two wind speed samples were non-
 374 stationary based on the run test method.

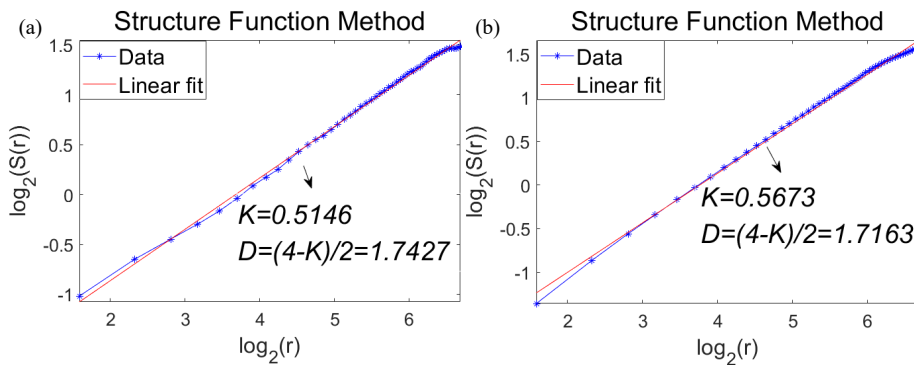
375 As for the fluctuating wind speed at the height of 320 m, the fractal dimension $D=1.7427$ was
 376 estimated by structure function method, and corresponding least-square fit result of the curve $\log_2(S(r))$
 377 with $\log_2(r)$ was presented in Fig. 12(a). After getting the fitted target spectrum $S_u(f)$ and calculating
 378 the amplitude parameter $A=0.0520$ by Eq. (25), the wind speed time series were then simulated using



379 Eq. (15), as illustrated in Fig. 13 and Fig.14. The fractal dimension of the simulated wind speed time
 380 series was determined using the structure function method, yielding a value of $D=1.7163$, as depicted
 381 in Fig. 12(b). These results indicate that the simulated wind speeds exhibit similar fractal
 382 characteristics with the original wind component. Moreover, the standard deviations of the actual and
 383 simulated fluctuating wind speeds were found to be 1.2030 and 1.2125, respectively, with a negligible
 384 relative error of 0.79%.



385
 386 Fig. 11 Measured 10-minute wind speed samples and their TVMs at the height of (a)160 m and (b)320 m

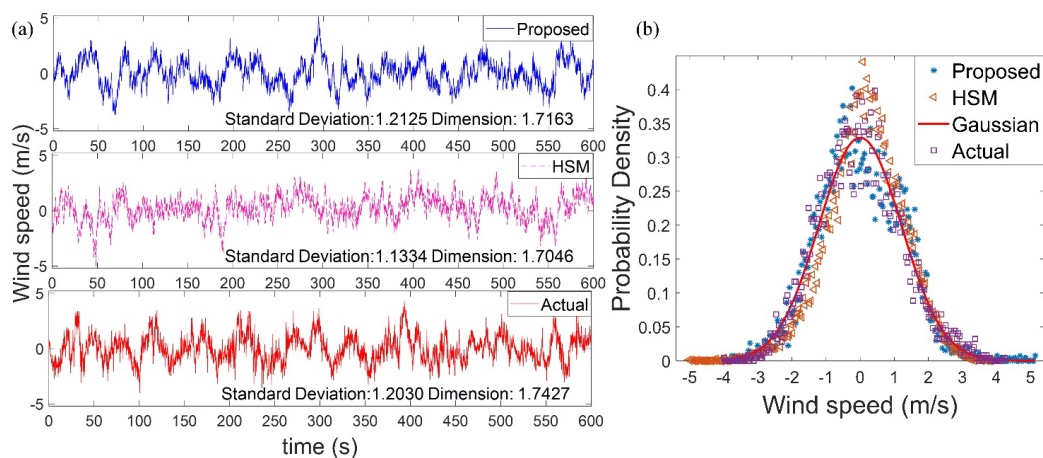


387
 388 Fig. 12 Plot of $\log_2(S(r))$ versus $\log_2(r)$ and relative least-square fitting result (red line): (a) Original fluctuating
 389 wind (b) Simulated fluctuating wind at the height of 320m

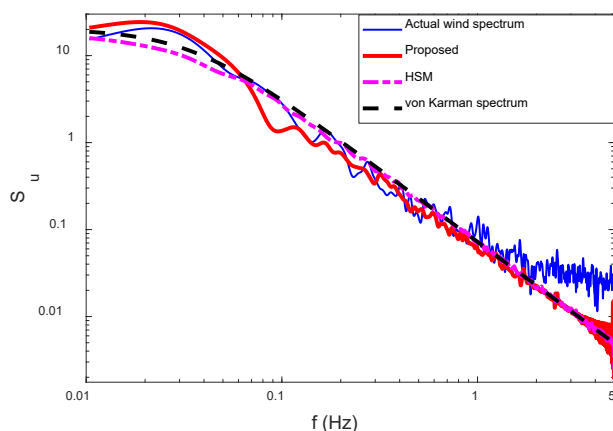
390 Additionally, wind speed time histories were also simulated using the conventional HSM for
 391 comparison with the proposed SWM method, as shown in Figs. 13 and 14. Fig. 13(b) demonstrates
 392 that the probability density functions of simulated fluctuating wind by the proposed SWM in this study



393 and commonly used HSM method are similar to that of the measured wind record, and each probability
394 distribution fits well with the Gaussian distribution. According to Fig. 14, it can be observed that the
395 original wind speed spectrum shows a tendency to deviate from the classical von Karman spectrum
396 beyond a frequency of 2 Hz, which might be attributed to the existence of Gaussian white noise in the
397 measured wind data as reported by Kaimal and Finnigan (1994). Fig. 15 shows the evolutionary power
398 spectral density (EPSD) of nonstationary wind speeds to reveal the turbulent energy distribution both
399 in time and frequency domain (Priestley, 1965). The similarity of wind spectra and EPSDs between
400 the actual and simulated wind in Figs. 14 and 15 provides the strong evidence for the effectiveness of
401 the proposed wind speed simulation method.

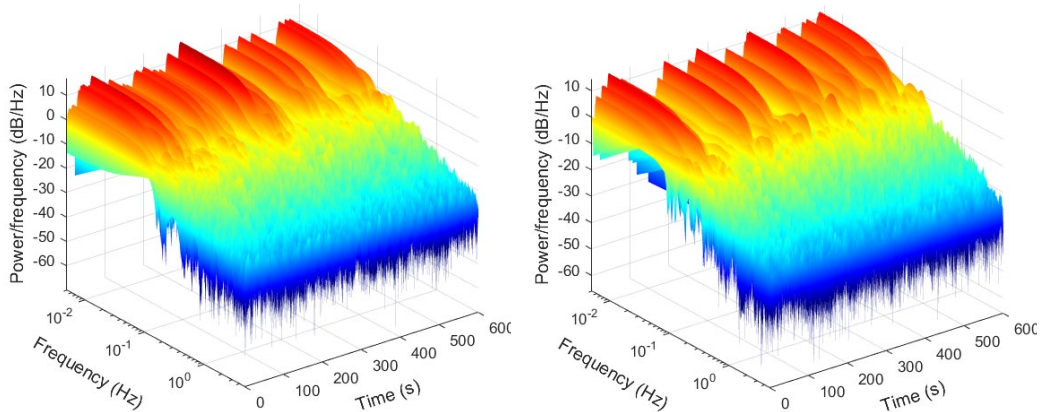


402
403 Fig. 13 (a) Simulated and original fluctuating wind speed time series, and (b) corresponding probability density
404 function at the height of 320m



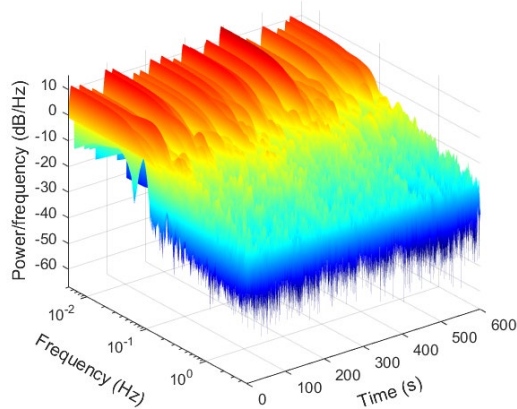
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Fig. 14 Wind spectra of the fluctuating wind speeds



(a) EPSD of the fluctuating wind simulated by SWM

(b) EPSD of the fluctuating wind simulated by HSM



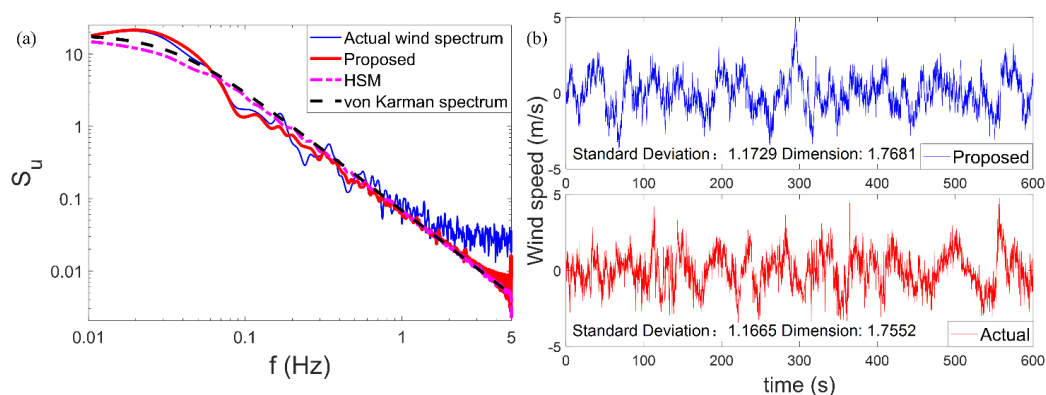
(c) EPSD of the actual fluctuating wind

407

Fig. 15 Estimated EPSD



408 Based on multivariate synchronous measurement at two heights of 160 m and 320 m, the cross-
409 correlation coefficient of two wind speed series in Fig. 11 was calculated by Eq. (26) as $\rho_{jk} =$
410 $0.115 > 0$. After the parameter $\sigma_\varphi=2.12$ was obtained by taking the inverse of Eq. (28), Eq. (27) could
411 be used to generate fluctuating wind series at the height of 160 m. Fig. 16 shows the simulation results
412 in terms of spectrum and fractal dimension. It was found the proposed SWM method can generate the
413 fluctuating wind series of second variate (at the height of 160 m) with very close properties to the
414 measured wind speed sample, i.e., wind spectrum, standard deviation, fractal dimension and the
415 specified cross-correlation to the first variate (at the height of 320 m).

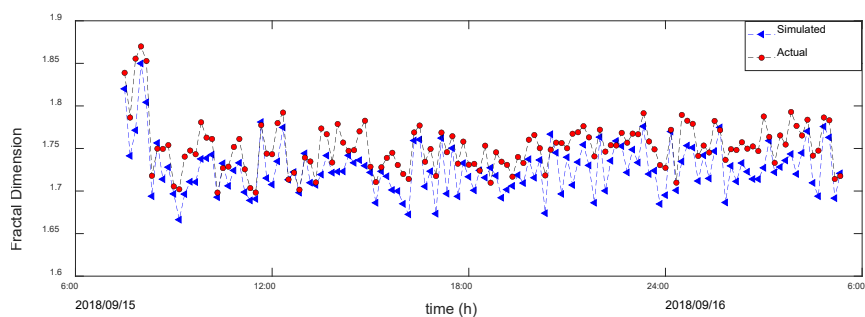


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417 Fig. 16 Simulation result of second variate at the height of 160 m (a) Wind spectra and (b) Fluctuating wind speeds

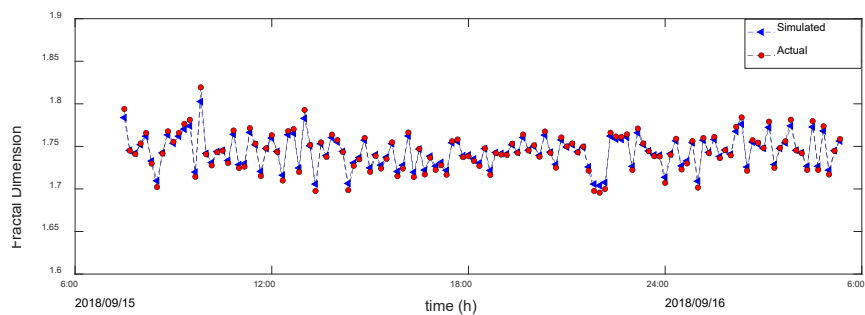
418 To further verify the effectiveness of the proposed SWM method, the 22-hour typhoon wind speed
419 samples from 7 am September 15 to 5 am September 16, i.e., 132 10-minute samples measured at two
420 representative heights of 160 m and 320 m were utilized. The 10-minute fluctuating wind series are
421 then recursively generated for the two different heights as time marching with a time step of 10-minute.
422 The fractal dimensions of the real and simulated fluctuating wind components were estimated by the
423 structure function method. Fig. 17 demonstrates that there is almost no difference in fractal dimensions
424 between the real and simulated wind fluctuations of the first variate (at the height of 320 m). For the



425 second variate, slight difference of fractal dimension was observed between the real and simulated
426 wind series due to the introduction of the Gaussian random phase variable φ in Eq. (27) or Eq. (29).
427 Fig. 18 shows that the evolution of standard deviation of the simulated wind series by the SWM method,
428 which are in close agreement with those of the real fluctuating winds during 7 am September 15 to 5
429 am September 16, 2018. By combining the TVM components, the proposed SWM is able to reproduce
430 nonstationary typhoon wind speed series effectively.

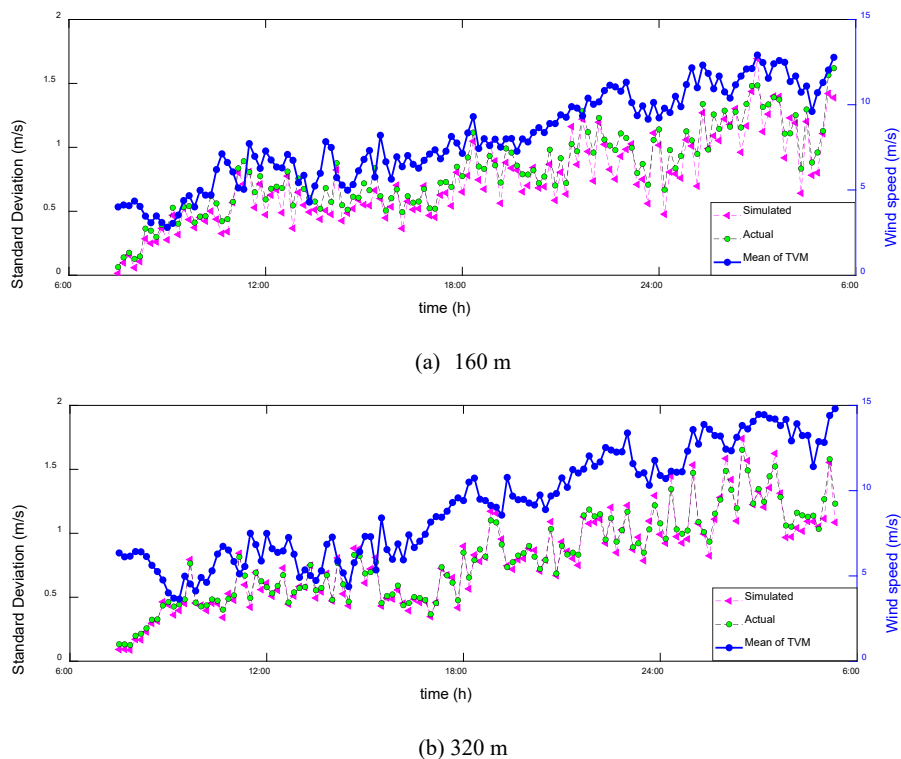


(a) 160 m



(b) 320 m

431 Fig. 17 Fractal dimensions of real and simulated fluctuating wind speeds



432 Fig. 18 Standard deviation of real and simulated fluctuating wind speeds with the mean of each TVM

433 4 Conclusions

434 This paper focuses on determining an appropriate method for the fractal dimension estimation of
435 wind speeds, and then propose the stochastic WM function-based numerical simulation method (SWM
436 method) for the multivariate wind speed simulation. The study shows that the structure function
437 method is a more suitable technique for estimating the fractal dimension than the box counting method,
438 variation method, and R/S analysis method. Field-measured wind data recorded during Typhoon
439 Mangkhut (2018) were used to present the performance of the proposed method. The specific findings
440 are as follows

441 (1) Various methods to determine the fractal dimension of winds affect the accuracy of the estimated



442 fractal dimension estimation. The mean fractal dimension of 1.75 obtained by the structure function
443 method is closest to the representative value of 1.7 than other three methods. Furthermore, the
444 estimated fractal dimension by the structure function method is quite robust and insensitive to
445 stationary or nonstationary wind models used.

446 (2) The multivariate wind speed components simulated by the proposed fractal-based SWM method
447 are in good agreement with the measured records in terms of fractal dimension, standard deviation,
448 probability density function, wind spectrum and cross-correlation coefficients. The proposed SWM
449 method combined with the TVM components is capable of generating nonstationary multivariate
450 typhoon wind speeds.

451 **Declaration of competing interest**

452 The authors declare that they have no known competing financial interests or personal
453 relationships that could have appeared to influence the work reported in this paper.

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