

Tall ~~Wind Profile Validation Using Lidar Observations~~ wind profile validation of ERA5, NORA3 and Hindcast Data NEWA, using lidar observations

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Abstract. The development of large offshore wind turbines and airborne wind energy (AWE) systems requires reliable wind speed datasets at heights far above the atmospheric surface layer. Traditional measurement approaches ~~-, primarily reliant-relying~~ on met-masts, fall short of addressing the needs of modern wind turbine design and AWE systems development. In this study, we validate three different model-based datasets, namely the 3-km Norwegian Hindcast archive (NORA3), the New European
5 Wind Atlas (NEWA), and ECMWF Reanalysis v5 (ERA5) using Doppler wind lidar data from several locations in Norway and the North Sea. The validation focuses on altitudes from 100 to 500 m above ground, covering the operational range of large wind turbines and AWE systems. Our findings indicate that ERA5 and NORA3 perform ~~remarkably-almost equally~~ well in offshore locations ~~-,with ERA5 showing the closest correlation to lidar data up to 200 m- in terms of bias, correlation coefficient, root-mean-square error and Earth's mover distance. However,~~ NORA3 outperforms the other two models in two coastal and
10 one complex terrain sites. ~~Finally, an increasing- In most cases, the~~ agreement between the models and lidar measurements ~~with height suggests that model-based datasets can be valuable for AWE systems research and development~~ increases with height. More generally, the choice of appropriate wind speed database depends on the topography, altitude and error metrics of interest.

1 Introduction

15 The hub height and rotor diameter of ~~offshore wind turbines (OWTs)-wind turbines~~ have been continuously increasing ~~over for~~ the past 20 years (Jahani et al., 2022; Jiang, 2021), reaching up to 150 m and over 200 m, respectively. This trend is driven by the need to capture stronger and steadier winds to reduce the ~~overall~~ levelized cost of energy (Wiser et al., 2021). In the near future, the top tip height of ~~offshore-such~~ wind turbines may reach almost 300 m ~~above-~~.

Airborne Wind Energy (AWE) systems harness wind energy using tethered aircraft operating at altitudes between 200 and
20 600 m. At these heights, wind speeds are generally stronger and steadier than near the surface.

Since the 2010s, ~~commercial airborne wind energy (AWE) systems have demonstrated notable advancements~~ AWE systems have made significant advances (Vermillion et al., 2021; Fagiano et al., 2022; Eijkelhof and Schmehl, 2022). Prototypes ~~of AWE systems~~ with capacities exceeding 600 kW (~~Vermillion et al., 2021~~) and ~~potentially developing into~~ have been developed, and scaling to multi-megawatt ~~have been proposed (Kruijff and Ruitkamp, 2018). However~~ systems has been proposed (Vermillion et al., 2021

25 . Despite this progress, AWE systems ~~remain~~ are still in the early ~~stage~~ stages of development compared to offshore wind turbines. ~~Recent efforts in performance assessment have relied mainly on ground-generation AWE systems, which is the most mature technology at the moment (Vermillion et al., 2021). Such studies used simulated wind speed profiles, with optimal operating heights~~

Two main concepts dominate current AWE designs: ground-generation systems and onboard-generation systems. Ground-generation systems, or “pumping power” systems, generate energy on the ground using a winch and generator. In this case, the tethered aircraft alternates between the energy-generation and recovery phases. Aircraft for this concept include soft kites, semi-rigid, and rigid wings. Each type offers trade-offs between adaptability and durability. Onboard generation systems, in contrast, produce energy in the air using onboard turbines and power is transmitted to the ground via conductive tethers. These systems typically use rigid-wing aircraft, quadrotors, or toroidal aerostats (Cherubini et al., 2015). While ground-generation systems

30 are relatively efficient, they require advanced automation for continuous operation (Elfert et al., 2024). Onboard-generation systems are better at harnessing high-altitude winds but face challenges in weight optimization and tether design. Flexible wings are adaptable to varying wind conditions but are less durable. Conversely, rigid wings provide higher power output but have greater mechanical complexity and costs (Fagiano et al., 2022). Key challenges remain for AWE systems ~~identified between 200 and 600 m above the surface (Sommerfeld et al., 2019b)~~, including managing wind variability, tether dynamics, and autonomous operation. A major limitation lies in the reliance on oversimplified wind speed approximations, due to the lack of detailed wind speed data at altitudes above 200 m (Sommerfeld et al., 2019a). Addressing this gap through tall wind profiling is essential for optimizing AWE system design and unlocking their full potential for large-scale deployment.

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Traditional approaches for estimating horizontal mean wind speed profiles rely on mast-based measurements, which are primarily applicable to studying the atmospheric surface layer (ASL). The ASL constitutes approximately the lowest 10% of

45 the atmospheric boundary layer (ABL). Under neutral and unstable atmospheres, the depth of the ASL ranges from 50 m to 100 m offshore and can extend up to 200 m onshore (Pal and Lee, 2019; Davis et al., 2020, 2022). Under a stable atmosphere, the ASL is shallow, with a depth sometimes close to a dozen metres (Mason and Derbyshire, 1990). Traditional logarithmic and power-law mean wind speed profiles, such as those used in IEC 61400-1 (IEC, 2005), are limited to the ASL and are likely inadequate for wind turbine design with hub heights of 150 m or more (Tieo et al., 2020; Cheynet et al., 2024). For wind

50 resource assessment, the height-dependent Weibull parameters (Kelly et al., 2014) require the characterization of wind speed profiles above 200 m. Therefore, the development of both AWE systems and future ~~OWTs~~ offshore wind turbines necessitates information on the mean wind speed at heights several hundred meters above the surface.

Tall wind speed profiles, as defined here, cover the entire atmospheric boundary layer (ABL) or at least the initial 500 -m above the surface, and their characterization remains a significant challenge (Veers et al., 2019). The term ‘tall wind profile’ is in line

55 with its use in boundary-layer meteorology (e.g. Peña et al., 2014; Kelly et al., 2014). Traditional tall masts often fall short of

this definition, as they are typically lower than 100 m. Only a limited number of masts exceeding 200 m exist globally (Ramon et al., 2020), and these are exclusively onshore masts (Table 1). Although tall-wind speed profiles can also be collected using manned aircraft (e.g. Zemba and Friehe, 1987) or drones (Egger et al., 2002; Reuder et al., 2009; Palomaki et al., 2017; Shimura et al., 2018), this approach has not been adopted for wind resource assessment, which requires several years of data. ~~Therefore, the characterization of mean~~ In offshore locations, the collection of tall wind speed profiles ~~above the marine surface layer is a major challenge (Shaw et al., 2022; Veers et al., 2019)~~ is further complicated by the harsh marine environment and the high costs of installation and maintenance (Shaw et al., 2022).

~~Commercial Doppler wind lidar (DWL)~~

Tall wind speed profiles can, in general, be measured using remote sensing technologies (Emeis, 2011), including Doppler wind radar (Lehmann and Brown, 2021), sodar (Bianco, 2011), and lidar (Pichugina et al., 2012). As commercial Doppler wind lidars (DWLs) have become the standard instrumentation for wind energy applications, we have based our study on corresponding available lidar data sets. Commercial DWL profilers measure wind speed and direction up to approximately 300 m above the surface (Peña et al., 2009). They operate using fixed beams at predetermined angles with ~~modes like~~ scan modes such as Doppler beam swinging (DBS) or velocity azimuth display, showing good performance against tall met masts (Knoop et al., 2021). Commercial DWL profilers, both ground-based and mounted on fixed platforms, have been used in wind energy research for over a decade, both onshore (Smith et al., 2006; Kumer et al., 2016) and offshore (Peña et al., 2009; Peña et al., 2015)(Smith et al., 2006; Kumer et al., 2016; Brune et al., 2021) and offshore (Peña et al., 2009; Peña et al., 2022) began to complement traditional offshore met-masts, offering cost reductions (Krishnamurthy et al., 2013).

Most commercial DWL wind profilers are still limited to studying the mean wind flow in the first up to 300 m above the surface. Scanning DWLs possess a more powerful laser than lidar profilers, allowing them to collect data up to 3 km under good aerosol conditions (Kumer et al., 2014). This technology, used in atmospheric research for over two decades (Pichugina et al., 2012; Banta et al., 2013; Dias Neto et al., 2023), saw commercial adoption mainly in the early 2010s (Vasiljevic, 2014; Kumer et al., 2014). Scanning DWLs with hemispherical scanning capabilities can adjust both azimuth and elevation angles and can be set to mimic profiler modes for direct atmospheric profiling. Despite their potential, scanning lidars are often-underutilized in developing airborne wind energy systems (AWE systems) AWE systems or next-generation multi-megawatt offshore wind turbines. Notable examples of wind speed data collection with such instruments for tall wind profile analysis include Kumer et al. (2014) in coastal terrain, Reuder et al. (2024) at the FINO1 offshore platform, Päscke et al. (2015) and Sommerfeld et al. (2019a) in Germany or Mariani et al. (2020) in the Arctic.

Recently, open-source datasets from wind hindcast or reanalysis databases such as the 3-km Norwegian Hindcast archive (NORA3) (Haakenstad et al., 2021), the New European Wind Atlas (NEWA) (Hahmann et al., 2020), and ECMWF Reanalysis v5 (ERA5) (Hersbach et al., 2020) have provided model-based wind speed profiles within the first 500 m above the surface. A hindcast is a numerical model simulation of a historical period without data assimilation, unlike a reanalysis. Reanalysis uses modern data assimilation techniques over decades, combining observations with models to create a consistent picture of weather and climate, even in areas without direct observations. NORA3 and ERA5 appear adequate for wind resource

Table 1. ~~Some Examples~~ of ~~the~~ tall met masts with top height above 200 m documented in Ramon et al. (2020) and in the scientific literature. None of these masts are offshore. The list includes both current and former masts.

Tower name	Top sensor (m)	Country
Walnut Grove	488	USA
Park Falls	396	USA
West Branch	379	USA
South Carolina	329	USA
Beijing Meteorological Tower	325	China
Gartow	341	Germany
Obninsk	301	Russia
Boulder Observatory	300	USA
Boseong	300	South Korea
Hamburg	280	Germany
Steinkimmen	252	Germany
Østerild	250	Denmark
KIT	200	Germany
Cabauw	200	Netherlands

assessment and structural design, for which a climatological description of wind conditions ~~over the first 500 m~~ spanning at least 30 years is necessary. ~~Note that NEWA falls slightly short of this definition, as it only covers 10 years of data.~~ Although these databases can complement ~~in-situ~~ measurements, they require proper validation for wider use in wind energy. Portions of these databases have undergone validation against near-surface measurements (e.g. Ramon et al., 2019), mast measurements at
95 levels below 100 m (Olauson, 2018; Jourdir, 2020; Solbrekke et al., 2021; Cheynet et al., 2022), or tall-masts measurements up to 200 m (Knoop et al., 2020; Gualtieri, 2021). Additional validation has been conducted using Doppler wind lidar technology for heights up to 300 m above the surface (Pronk et al., 2022; Hallgren et al., 2024). The comparison of lidar wind speed profiles with hindcast or reanalysis products at higher altitudes remains, however, limited. This motivates our study ~~in an attempt~~ to bridge this identified knowledge gap.

100 In this study, we validate datasets from ~~the~~ ERA5 ~~global reanalysis~~, NEWA and NORA3 against ~~in-situ~~ measurements from DWL systems across diverse terrain locations in the North Sea and Norway to evaluate their accuracy in capturing tall wind speed profiles. We also aim to quantify the performance of these databases as a function of altitude using multiple error metrics. The selection of different sites ~~offers the possibility~~ provides an opportunity to examine the impact of topography on local wind conditions. ~~Thus, the~~ The novelty of this study ~~resides in both, the collection of wind speed data in the entire ABL, and~~
105 lies in the inter-comparison of various hindcast or gathering of lidar tall wind speed profiles and their comparison with various hindcast and reanalysis wind databases at altitudes up to 500 ~~m, which has yet to attract significant attention m, a topic that has received little attention to date.~~ Moreover, this study ~~expands the validation to include~~ explores the use of wind-energy-related

metrics, such as the capacity factor ~~for modern offshore of hypothetical modern~~ wind turbines and AWE systems, to evaluate the wind speed databases. This research is believed to be valuable to both wind energy and wind engineering, as tall wind speed profiles can be used for both wind resource assessment (Schelbergen et al., 2020) and wind loading on structures (Kent et al., 2018).

This study is organised as follows: section 2 introduces the datasets extracted from the ERA5, NORA3 and NEWA databases, as well as the DWL data. Section 3 presents the metrics used for the error analysis and the data processing to collocate the modelled and measured data in space and time. Section 4 ~~studies the influence of the choice of the site and the height on~~ examines how site selection and measurement height affect the errors between ~~the~~ wind atlases and ~~in-situ data~~ remote-sensing measurements. Our findings underscore NORA3's and ERA5's reliability offshore, especially above 100 m. However, in coastal ~~locations areas~~ and complex terrains, regional model-based datasets ~~become necessary. In some instances, and sometimes~~ microscale wind models ~~may even be needed to more accurately capture the~~, are required to accurately capture local wind conditions. Section 4 ~~presents also~~ also presents the influence of the choice of the wind atlas on the estimation of the capacity factor of ~~a modern wind turbine and an~~ modern wind turbines and airborne wind energy ~~systems~~ systems. Finally, section 5 discusses the need for more powerful DWL profilers and the complementary role of mesoscale and microscale simulations for improved wind resource assessment.

2 Data collection and wind models

This section outlines the wind models and measurement campaigns considered to assess tall wind speed profiles. NEWA, NORA3, and ERA5 wind atlases are introduced with their spatial and temporal resolutions. Five lidar campaigns across offshore, coastal, and complex terrain sites provide validation data for the analysis.

2.1 Model data

A state-of-the-art wind atlas is defined herein as a climate dataset that provides the mean wind speed and mean wind direction at multiple heights above the surface. It provides a horizontal spatial resolution on the kilometre scale, a time resolution of 1 h or finer, and temporal coverage of at least ~~40-30~~ years. The definition of a wind atlas employed here relates to a hindcast or reanalysis database that is usable for wind resource assessment or the design of wind energy systems, including extreme value analysis. In this ~~context, both NEWA and NORA3 qualify as state-of-the-art wind atlases. They study, they~~ are regional downscaling products of the ERA5 reanalysis (Hersbach et al., 2020), covering overlapping areas in Europe (Fig. 1). Consequently, ERA5 data are also included in this analysis. Although wind atlases are sometimes defined as databases with microscale spatial resolution finer than 1 km, we choose to adopt a broader definition that includes model-based wind data with a kilometre-scale resolution. Hereinafter, z denotes the height in metres above the surface, and \bar{u} represents the horizontally averaged mean wind speed at height z .

The ERA5 reanalysis product from the European Centre for Medium-Range Weather Forecasts (~~ECMWF~~) superseded ERA-Interim in 2019 (Dee et al., 2011). ERA5 offers climate data with global coverage, a horizontal spatial resolution of

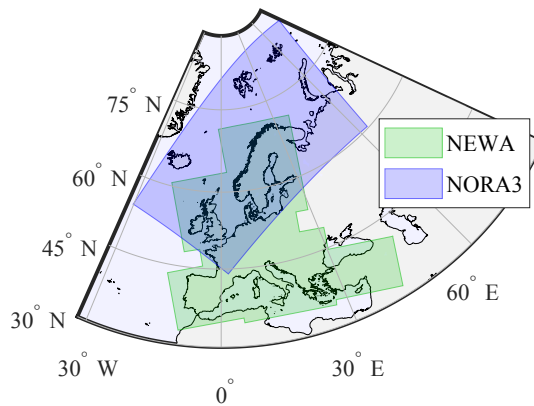


Figure 1. Illustration of the regions covered by NEWA and NORA3. ERA5 has global coverage and is thus not shown here.

140 approximately 31 km and a hourly output, extending from 1940 onward. As a reanalysis product, ERA5 uses a 4D-Var data assimilation scheme (Courtier et al., 1994) within a 12-hour assimilation window, incorporating both in-situ measurements and satellite observations (Hersbach et al., 2020). The ERA5 temporal resolution and extensive temporal coverage are valuable for wind energy research globally (Olauson, 2018), including the analysis of annual and decadal wind variability and potential trends due to climate change (Chen, 2024; Antonini et al., 2024; Martinez and Iglesias, 2024). Researchers and engineers in the wind energy sector increasingly rely on ERA5 for both historical analysis and future project planning (Olauson, 2018; Gualtieri, 2021; Hayes et al., 2021). This reliance underlines the importance of accurate, high-resolution climate reanalyses in advancing renewable energy technologies.

NEWA is an open-access European wind atlas released in 2019 and developed through collaboration among 30 European academic and industrial partners (Hahmann et al., 2020; Dörenkämper et al., 2020). NEWA uses the Weather Research and Forecasting (WRF) model and utilizes the ERA5 reanalysis as forcing, without further data assimilation. NEWA covers the period from 1989 to 2018 and aims to provide a detailed wind climatology of Europe with a spatial resolution of approximately 3 km and a temporal resolution of 30 min. In this study, data on mean wind speed and direction from the mesoscale output of NEWA were retrieved from for at eight altitudes, ranging from 10 m to 500 m above sea level (asl) mean sea level.

NORA3 is a regional downscaling of the ERA5 reanalysis and utilizes the HARMONIE-AROME non-hydrostatic regional numerical weather prediction model for its production (Haakenstad et al., 2021). The downscaling consists of nine-hour short integration runs initiated every six hours, employing the last run as the initial state for the new cycle. Surface observations in the CANARI-OI-Main assimilation system adjust the first-guess (Giard and Bazile, 2000; Taillefer, 2002), with ERA5 forcing applied in the free atmosphere following the boundary relaxation method (Radnoti, 1995; Termonia et al., 2018). NORA3 is built on NORA10's legacy, which has been used by the offshore industry in the North Sea for over a decade (Furevik and Haakenstad, 2012) and refines the description of the wind condition provided by NORA10 (Haakenstad et al., 2021). Validations of the NORA3 database against atmospheric data include comparisons with wind measurements from oil and gas platforms, as well as offshore masts in the North Sea and Norwegian Sea (Solbrekke et al., 2021). NORA3 provides wind data once per hour with a 3

Table 2. Metadata of the wind atlas data sets. Only z-levels above 100 m are shown [and used](#) hereinafter. ERA5 data were collected using the 100 m z-level with additional height levels retrieved using pressure levels and the geopotential height. Δh is the horizontal spatial resolution and Δt is the temporal resolution in minutes.

	Δh (km)	Δt (min)	z-levels (m)
NORA3	3	60	100, 250, 500, 750
NEWA	3	30	100, 150, 200, 250, 500
ERA5	31	60	100, geopotential heights

km spatial resolution ~~across 65 layers in a hybrid sigma-pressure coordinate scheme~~. A specific subset, released in 2021 by the Norwegian Meteorological Institute, has been selected for this study. This subset presents mean wind speed and direction data at seven heights, from 10 to 750 m ~~asl~~ [above sea level, extending from 1961 onward, as reflected in the database status at the end of 2024](#). Table 2 details the metadata for the different models, illustrating the variability in spatial and temporal resolutions, as well as available height levels above 100 m among NORA3, NEWA, and ERA5.

2.2 The measurement sites

The measurement data were collected by [reference](#) DWL instruments within the area covered by ERA5, NORA3, and NEWA (Fig. 2). Two lidar campaigns were conducted in the marine ~~atmospheric boundary layer at the ABL~~ (FINO1 and FINO3 ~~locations, two other campaigns took place in platforms, two others at~~ coastal sites (Sola and Lista airports in Norway), and one in complex [mountainous](#) terrain (Bjerkreim, Norway). ~~Offshore sites refer here to locations situated in open waters, typically over a few dozen kilometres from the coast, while coastal sites refer to flat onshore locations a few kilometres from the shoreline. Complex terrain refers to areas characterized by heterogeneous topography, such as hills or mountains. ??, characterized by rocky terrain and sparse vegetation. FINO1's proximity to wind farms enables an examination of discrepancies between lidar measurements and wind atlases due to wake effects. Analysing data from both the FINO1 and the FINO3 platforms highlights the challenges of assessing wind resources in such areas and underscores the need for cautious application of wind atlases near wind farms.~~

[Table 3](#) summarises the locations and measurement periods of the five campaigns selected for the validation of wind atlases. ~~The diversity of locations, comprising two offshore, two coastal, and one in complex terrain, offers additional possibilities to assess the performances of the wind atlases at higher altitudes. This study uses lidar data as reference datasets, given their suitability for capturing wind speed data across the entire ABL. Data availability above 500 m decreases due to factors such as low clouds and low aerosol content, as illustrated in Fig. 3. This figure defines data availability as a function of the carrier-to-noise (CNR) ratio. More specifically, missing data or data with a CNR under -27.5 dB for the scanning lidar instrument and under -22 dB for the DWL profiler are dismissed. The threshold value for the scanning lidar is lower than the value of -22 dB used in Peña et al. (2015), which is usually applied to DWL profilers. However, a lower threshold can~~

Table 3. Metadata of datasets from five lidar measurement campaigns. The lidar range gate denotes the along-beam spatial resolution.

	FINO1	FINO3	Lista	Sola	Bjerkreim
Latitude (N)	54.015	55.195	58.104	58.885	58.595
Longitude (E)	6.588	7.158	6.631	5.631	5.955
Terrain Type	Offshore	Offshore	Coastal	Coastal	Complex
Device	Windcube 100S	WLS70	WLS70	Windcube 100S	WindCube V1
Start Date	01.06.2015	10.09.2013	20.11.2020	04.03.2013	30.03.2010
End Date	05.10.2016	06.10.2014	06.09.2021	30.06.2013	06.05.2010
Hours Collected	1353	7997	6912	525	799
Min height (m)	78	125	100	133	40
Max height (m)	3528	2025	2000	2641	300
Range Gate (m)	25	50	100	75 <u>66</u>	20

be applied for scanning Doppler wind lidar (Cheynet et al., 2017). For simplicity, specific methods, e.g. those presented by Beck and Kühn (2017); Valdecabres et al. (2018); Cheynet et al. (2021) or Duseha et al. (2023) to rescue data with even lower CNR are not considered here, as only the mean wind speed was of interest. Location of the five measurement sites in the North Sea and along the Norwegian coast. Figure 2 geolocalises the five measurement campaigns and provides a close-up of the three onshore locations. The offshore sites are situated more than 40 km away from the coast. The coastal sites are located inland only a few kilometres from the shore and are characterised by sharp roughness changes as the terrain transitions from open water to flat, agricultural land with sparse vegetation. These abrupt roughness changes generate internal boundary layers, which can be challenging to capture accurately with hindcast and reanalysis databases. The complex site Bjerkreim is mountainous, with steep slopes and limited vegetation or trees. While distinct from the fjord-like landscapes found in other parts of Norway, this complex terrain features significant elevation changes that contribute to non-homogeneous wind conditions, particularly within the atmospheric surface layer.

The first measurement campaign was conducted took place in Bjerkreim, Southwest Norway, from March to May 2010. The site, characterized by rocky terrain and sparse vegetation, presented a complex topography. A WindCube V1 DWL (Leosphere) was deployed to capture wind profiles at altitudes ranging from 40 m to 300 m above the surface. Approximately 799 hours of mean wind speed data were collected. The mean wind speed with a temporal resolution of 10 min. The records were subsequently validated against sodar measurements taken 300 m away from the lidar’s location.

The second measurement campaign, known as the Lidar MEasurement Campaign Sola (LIMECS) (Kumer et al., 2014) was conducted at Stavanger Airport Sola, Norway, from March to June 2013–2013 (Kumer et al., 2014). The objective was to evaluate the capability of a long-range scanning pulsed lidar instrument in measuring mean wind speed at altitudes beyond the reach of traditional meteorological masts. A first-generation WindCube 100S lidar was deployed, operating in DBS scanning mode and capturing wind 10-minute mean wind speed profiles at a minimum height of 133 m above the surface.

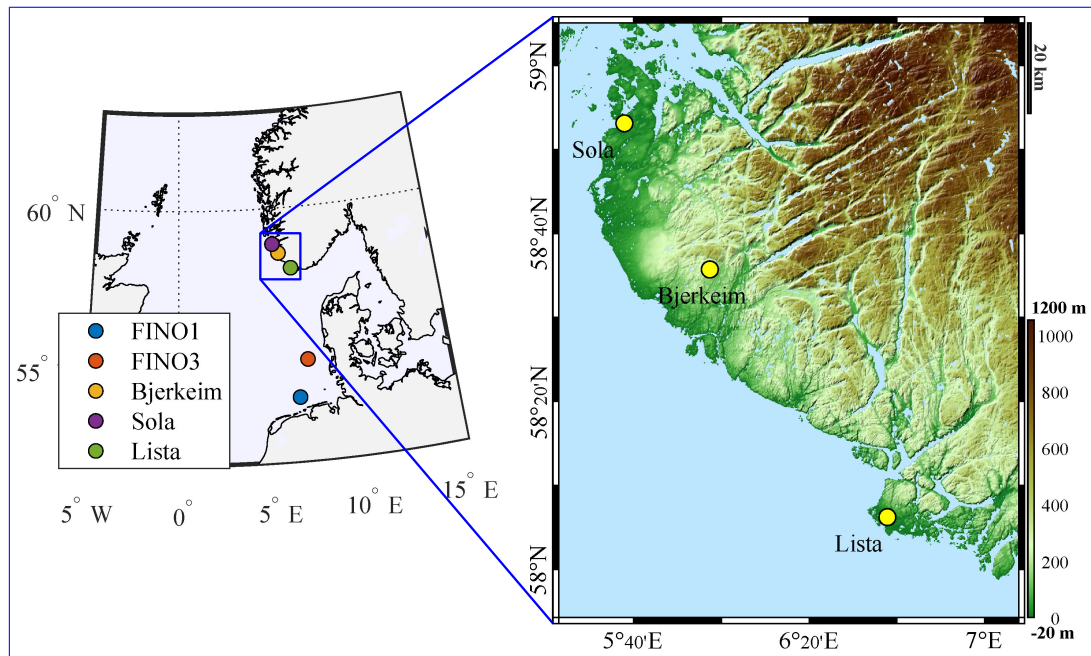


Figure 2. Locations of the five measurement sites in the North Sea and along the Norwegian coast (left panel), with a detailed view of the onshore sites (right panel). The right panel includes a digital elevation model of the three onshore measurement sites, generated using the toolbox by Beauducel (2024).

The measurement principle involves all lidar devices operating in DBS mode. This mode reconstructs horizontal wind speed and direction from the radial velocities of four beams, incorporating two volume averaging effects: one over the range gate length of each beam and another across the horizontal area over the lidar increasing with height, defined by the four beams at a given opening angle of typically 30 degrees. The DBS mode assumes horizontal homogeneity of the mean flow, a condition typically met in flat and homogeneous terrain but often violated in highly complex terrain (Pauser et al., 2016) or near obstacles, such as in the wake of a wind turbine. As altitude increases, the flow tends to become more homogeneous and horizontal, making DBS scanning suitable for measuring tall wind speed profiles.

This campaign resulted in the collection of approximately 525 hours of data. The lidar measurements were compared against radiosonde data, demonstrating a strong correlation with a Pearson coefficient $R > 0.95$, which improved with increasing altitude (Kumer et al., 2014).

The third measurement campaign took place at the FINO3 offshore platform offshore platform FINO3, located at 55.195°N, 7.158°E in the North Sea, approximately about 80 km from off the Danish coast. The platform hosted a Leosphere WLS70 DWL profiler by Leosphere (Cariou et al., 2009) from August (Cariou et al., 2009) which operated from September 2013 to October 2014. The lidar operated in DBS scanning mode with a scan angle of 14.7°, resulting This resulted in the collection of approximately 7997 hours of data with a temporal resolution of 10 min. The lowest measurement height, at of 125 m above sea level (asl), ensured no significant mast-induced flow distortion. The collected wind speed and direction data were validated and detailed in Peña et al. (2015).

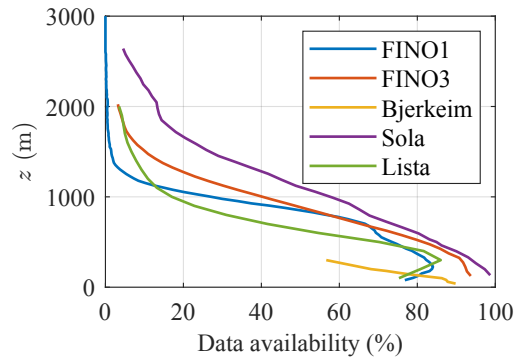


Figure 3. Data availability during the five measurement campaigns as a function of the altitude, based on the Carrier-to-Noise Ratio (CNR) of -27.5 dB for the scanning lidars and -22 dB for the lidar profilers.

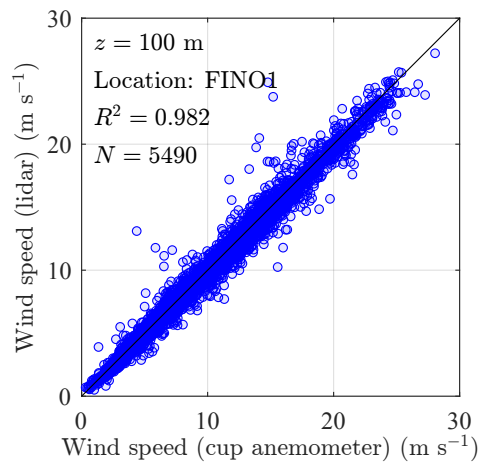


Figure 4. Comparison of 10-minute mean wind speed measurements recorded by the cup anemometer and the WindCube 100S at 100 m above sea level, collected between June 2015 and October 2016 during the OBLEX-F1 campaign at the FINO1 platform (5490 samples).

The fourth measurement campaign was conducted at the FINO1 offshore platform, ~~located at 54.014°N, 6.587°E~~ located at 54.015°N, 6.588°E in the southern North Sea, approximately 45 km north of ~~Borkum Island~~ the island of Borkum, Germany. The platform hosted a Windcube 100S (Leosphere) long-range scanning DWL from ~~01~~ June 2015 to ~~05~~ October 2016 (Reuder et al., 2024). The lidar operated in DBS scan mode with a fixed elevation angle of 70°, performing scans twice ~~every~~ per hour to collect 10-minute mean wind speed profiles. ~~A total of~~ In total, approximately 1353 hours of data were recorded, with the lowest measurement height at 78 m above ~~the sea surface~~ sea level. A preliminary comparison with a reference cup anemometer mounted at the top of the FINO1 mast ~~(at 100 m above the sea surface)~~ at 100 m above the sea surface (Fig. 4) showed excellent agreement, with a squared Pearson coefficient (R^2) of 0.98, similar to results from a study conducted at the FINO3 platform (Peña et al., 2015). ~~The lidar data collected at FINO1 are therefore considered reference data in this study (Fig. 4).~~

The fifth measurement campaign took place at Farsund Airport (Lista, Norway) from November 2020 to September 2021, focusing on the study of the ~~atmospheric boundary layer~~ ABL for airborne wind energy applications. A WindCube WLS70 lidar was deployed and operated in DBS mode with measurement heights ranging from 100 to 2000 m above the surface. ~~This paper analyses nearly one year of wind speed records, resulting in~~ The measurements resulted in the collection of approximately 6912 hours of data with a temporal resolution of 10 min.

It should be noted that the measurements at Bjerkreim and Sola were conducted over short time periods and are therefore not representative of the typical, annual wind variations at these sites. Instead, the data should be interpreted within the context of this study, which aims to compare tall wind speed profiles from wind atlases with lidar observations.

Figure 3 displays the lidar data availability as a function of the altitude, which decreases substantially above 500 m due to low clouds and low aerosol content. The data availability is defined here by the carrier-to-noise ratio (CNR). Data with a CNR below -27.5 dB for the scanning lidar instrument and below -22 dB for the DWL profiler were excluded. A threshold of -27.5 dB allows for increased data availability and is empirically robust for scanning Doppler wind lidar (Cheynet et al., 2017). For simplicity, specific methods, e.g. those presented by Beck and Kühn (2017); Valdecabres et al. (2018); Cheynet et al. (2021) or Duscha et al. (2023) to rescue data with even lower CNR are not considered here, as only the mean wind speed was of interest.

All lidar instruments operated in DBS mode with an opening angle of 30 degrees. This mode reconstructs horizontal wind speed and direction from the radial velocities of four beams. It also incorporates two volume averaging effects: one over the range gate of each beam and another across the scan horizontal area, which increases with height. The DBS mode assumes horizontal homogeneity of the mean flow, a condition typically met in flat and homogeneous terrain but violated in highly complex terrain (Pauscher et al., 2016) or near obstacles, such as in the wake of a wind turbine. As the altitude increases, the flow tends to become more homogeneous and horizontal (Emeis, 2013), making DBS scanning suitable for measuring tall wind speed profiles.

3 Methods

This section outlines the methods used to compare lidar wind speed data with predictions from NORA3, NEWA, and ERA5. It covers the four error metrics employed, data preprocessing techniques, and the evaluation of power curves and capacity factors for wind turbines and airborne wind energy systems.

3.1 Error metrics

To quantify discrepancies between mean wind speed data obtained from lidar instruments and those predicted by wind atlases, four metrics are employed: the ~~squared Pearson correlation coefficient~~ (R^2) coefficient, the bias, the Root-Mean-Square Error (RMSE), and the first Wasserstein distance, also known as the Earth Mover's Distance (EMD). The ~~squared Pearson correlation coefficient~~ (R^2) coefficient measures the linear correlation between the measured and modelled wind speeds. The bias quantifies the average difference between the predicted and observed values, providing a measure of systematic error ~~and the~~. The

Root-Mean-Square Error (RMSE) quantifies the average magnitude of the error. The EMD quantifies the dissimilarity between two probability distributions, making it well-suited for analysing wind atlases that represent the climatology of a site in terms of the probability distribution of mean wind speed and direction (Hahmann et al., 2020). For brevity, only the EMD equation is introduced, as the equations for the R^2 coefficient, RMSE, and bias are assumed to be familiar to the reader. For one-dimensional distributions, the EMD can be represented by the area between two cumulative distribution functions (CDFs), F_1 and F_2 :

$$\text{EMD} = \int_{-\infty}^{+\infty} |F_1(x) - F_2(x)| dx. \quad (1)$$

To complement these metrics, the Taylor diagram (Taylor, 2001) provides a summary of model performance by integrating the correlation coefficient, standard deviation, and RMSE into a single plot. This graphical representation is particularly useful for comparing multiple models against observed data in a visually intuitive way.

3.2 Data preprocessing

The data preprocessing is similar for all campaigns: Hindcast data are Wind atlases data were initially interpolated from their original horizontal grid to the GPS coordinates of the lidar campaign locations at each vertical height level. The interpolation scheme follows the method described in Amidror (2002), specifically a linear scattered data interpolation, as the data from the wind atlases are not necessarily on a Cartesian grid.

The datasets from NORA3 and NEWA datasets are provided at specific height levels, whereas the (Table 2). The ERA5 data were collected at five pressure levels (1000, 975, 950, 925, and 900 hPa), as well as at 10 and 100 m above the surface. Combining height and pressure levels ensured robust data retrieval and high vertical resolution. The pressure levels were converted into geopotential height levels using the geopotential variable available in the ERA5 database. Although geopotential height slightly differs Geopotential height differs slightly from geometric height, this as it accounts for variations in Earth's gravity, while geometric height is the actual vertical distance. This study focuses on wind speed data within the first 500 m above the surface, where the approximation of geopotential height to geometric height is expected to be sufficiently accurate two heights are approximately equivalent.

A linear interpolation method was employed for vertical spatial collocation between model and lidar data. The wind atlas data were linearly interpolated to the measurement heights of each lidar range gate. Since each lidar has different range gates, the comparison cannot always be conducted at the exact same altitude across all sites. Alternative non-linear interpolation schemes were also tested, such as spline, piecewise cubic Hermite interpolating polynomial methods, and the modified Akima method (Akima, 1974), but they yielded similar results while being less robust than the linear interpolation. Appendix A presents the error metrics quantified at specific heights and as vertical profiles using a non-linear regression. The non-linear regression shows minor differences in the error metrics compared to linear interpolation but does not change the conclusions of the study. The comparison in appendix A supports our decision to use linear interpolation for additional height levels in this study.

Following the spatial collocation, the model data were then temporally collocated with the lidar data. The lidar data consist of 10-minute averaged time histories series, while the model data are provided at 60-minute or 30-minute resolutions. The first

approach (Approach A) involves [interpolating a temporal interpolation of](#) the model data to align with the 10-minute averages from the lidar. An alternative approach (Approach B) would be to interpolate the lidar data to an hourly timestep. However, Approach B is more complex than Approach A and did not yield significant differences. Therefore, for simplicity and to avoid overprocessing the data, Approach A was adopted.

295 Finally, for the lidar data, the initial outlier detection and removal method, which relied on CNR threshold values of -27.5 dB for the scanning DWL and -22 dB for the DWL profiler, was found to be sufficiently effective, eliminating the need for additional outlier tests.

3.3 Power curves and capacity factor

This subsection outlines the methodology used to evaluate how [data from](#) different wind atlases influence the estimated capacity factors of wind turbines and AWE systems at the five selected sites. The ~~turbines examined include a range of models from wind turbine models examined include~~ the NREL 5 MW ~~with a~~ (90 m hub height ~~to the~~, 126 m rotor diameter), IEA 15 MW (150 m hub height, 240 m rotor diameter), and NREL 18 MW ~~with a~~ (156 m hub height, ~~detailed in~~ 263 m rotor diameter), the details of which are provided by NREL (2020). The power curves for these turbines are defined by a rated wind speed typically between 10 and 12 m s⁻¹, ~~with a~~ cut-in speed of 3 to 4 m s⁻¹ and a cut-out speed of approximately 25 m s⁻¹. [Capacity factor calculations in this study are based on wind speed at hub height. While modelling rotor-averaged \(or equivalent\) wind speed, which accounts for shear, turbulence intensity, and wind veering \(Wagner et al., 2009; Antoniou et al., 2009; Murphy et al., 2019\) could yield more realistic capacity factor estimates, such an analysis falls beyond the scope of this work.](#)

The power curve for AWE systems depends on flight height and trajectory, complicating the estimation of annual energy production and capacity factors. To address this challenge, various approaches are possible, such as clustering methods for faster computation of AWES production (~~Schelbergen et al., 2020~~) (Schelbergen et al., 2020; Sommerfeld et al., 2023) or simplified power curves (Eijkelhof and Schmehl, 2022; Ranneberg et al., 2018). In this study, we opted to use simplified power curves as we focus primarily on validating tall wind speed profiles using scanning lidar instruments, without delving into AWE systems flight trajectory optimization. Two simplified power curves for AWE systems are considered: one developed for a 3 MW rigid body (Eijkelhof and Schmehl, 2022) and one for a smaller 100 kW AWE system (Ranneberg et al., 2018). The power curves of the 3 MW and 100 kW systems are displayed in the middle and bottom panels of Fig. 5, respectively. These power curves represent a balance between simpler ones, such as those used in Vos et al. (2024), where the rated power remains constant above the rated wind speed, and more advanced path-dependent approaches studied in Eijkelhof and Schmehl (2022) or Sommerfeld et al. (2023).

In the middle panel of Fig. 5, we smoothed the 3 MW power curve using non-linear regression with smoothing splines, leading to cut-in and cut-out [operating](#) wind speeds of 9.0 and 29.9 m s⁻¹, respectively. These values slightly differ from those in the study by Eijkelhof and Schmehl (2022), which were based on ten optimized flight paths. Notably, we adopted a lower cut-in wind speed of ~~9 m m~~ 9 m s⁻¹, compared to their 10 m s⁻¹, ~~a distinction that~~. [This distinction](#) may be significant in the North Sea, where median wind speeds ~~typically range between at 250 m above the surface typically range from 9 and 10 m to 11 m~~ typically range between 9 and 10 m to 11 m s⁻¹ (Cheynet et al., 2024). The smoothed power curve for the 3 MW AWE system does not account for negative power output at the

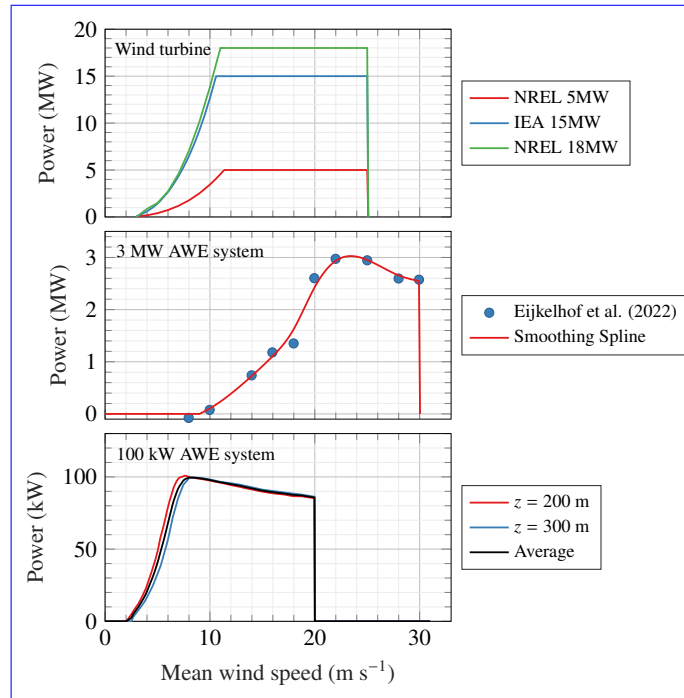


Figure 5. Power curves of the wind turbines investigated (top panel), the 3 MW airborne wind energy system presented in Eijkelhof and Schmehl (2022) (middle panel) and power curves for the 100kW AWES from Ranneberg et al. (2018) with averaged operating value between 200 and 300 m (bottom panel).

325 lowest wind speed of 8 m s^{-1} because ~~it is assumed~~ we assume that the AWE system will not operate at such wind speeds. For the 100 kW AWE system, we averaged two power curves computed at 200 m and 300 m above the surface based on Ranneberg et al. (2018), resulting in a cut-in wind speed of 2 m s^{-1} , a cut-out wind speed of 20 m s^{-1} and a rated wind speed of 7.5 m s^{-1} . Unlike a wind turbine, the rated power in this curve decreases with increasing wind speed due to power consumption during the retraction phase, ~~which leads to a loss of power~~ (Eijkelhof and Schmehl, 2022). Note that because the two power curves for the
 330 AWE system systems display significantly different rated wind speeds, they ~~are likely to~~ lead to large differences in capacity factors, which is discussed in section 4.

In this study, the wind speed values used for the power curve of the AWE systems (Fig. 5) are based on the median spatial average of mean wind speeds recorded at altitudes between 200 and 500 m. A similar approach was adopted in Vos et al. (2024) using a single height of 350 m above the surface. ~~However, at sites with complex terrain, such as Bjerkreim, we limited~~
 335 ~~measurements to between 200 and~~ At the complex site of Bjerkreim, however, the profiler lidar's maximum scanning height was 300 m due to lidar profiler constraints, so measurements in this case were limited to the 200–300 m range. The choice of averaged wind speed values from altitudes between 200 and 500 m serves a dual purpose. Firstly, these altitudes align with the operational heights of large AWE systems (Eijkelhof and Schmehl, 2022). Secondly, this selection facilitates the approximation

of capacity factors for AWE systems, avoiding the time-consuming task of calculating an optimal flight path for each wind speed profile.

~~Summary of wind turbine models tested with ERA5, NORA3, and NEWA datasets, available at: Model Name Hub Height (m) Rotor Diameter (m) NREL 5 MW 90 126 Leanwind 8 MW 110 164 NREL 10 MW 119 198 DTU 10 MW 119 178 IEA 10 MW 119 198 IEA 15 MW 150 240 NREL 18 MW 156 263~~

~~At each site, a reference capacity factor was calculated using lidar data. This reference was then compared to the capacity factors estimated from the wind atlases, providing a measure of the accuracy of these models in capturing the wind energy potential.~~ The capacity factor (CF) represents the ratio of the expected output power to the maximum or nominal power output P_{\max} . ~~Therefore, it~~ It can be calculated using time-averaged power output as

$$CF = \frac{\overline{P(t)}}{P_{\max}} \quad (2)$$

where the overline denotes the temporal average and P_{\max} is the nominal power output. If enough data is collected to construct reliable probability density functions, the capacity factor can be derived by integrating the product of the wind speed's probability density function $f_{\text{pdf}}(u)$ and the power curve $P(u)$ across all possible operating wind speeds:

$$CF = \frac{1}{P_{\max}} \int_0^{\infty} f_{\text{pdf}}(u) \cdot P(u) du \quad (3)$$

In this study, eq. (2) was used for simplicity but also because some of the data collected were recorded over only one month five weeks, which may be insufficient to construct robust probability density functions as required by eq. (3). ~~At each site, a reference capacity factor was calculated using lidar data. This reference was then compared to the capacity factors estimated from the wind atlases, providing a measure of the accuracy of these models in capturing the wind energy potential.~~

4 Results

~~This section presents the key findings from the comparison between lidar wind speed measurements and model datasets. The analysis includes the five sites, each representing different wind conditions. We first examine the collected wind speed time series and their alignment with model predictions. Next, we assess the performance of NORA3, ERA5, and NEWA for each site using vertical profiles of error metrics and capacity factor estimates.~~

4.1 ~~Overview of data collection~~ Error metrics across sites

~~This section~~ Figure 6 presents the time series data collected from lidar measurements and model databases during distinct campaigns at ~~the five sites~~: FINO1 (offshore, 2015-2016), FINO3 (offshore, 2013-2014), Bjerkreim (complex terrain, 2010), Sola (coastal terrain, 2013) and Lista (coastal terrain, 2020-2021). Each time series ~~, illustrated in Fig. 6,~~ corresponds to wind speed data collected at the ~~height nearest to the hub height of a 15 MW offshore wind turbine at approximately 150~~ range gate closest to 200 m. ~~We remind that~~ NEWA does not cover the period ~~during which the lidar data were collected at Lista. Due to~~

occasional data loss, lidar data series are discontinuous, and comparative analysis with model databases (NORA3 of lidar data collection at Lista, limiting the comparative analysis to NORA3 and ERA5, NEWA) is restricted to periods where lidar data are available. Time series of mean wind speed data recorded at the five reference sites (FINO1, FINO3, Bjerkeim, Sola and Lista) at the range gate nearest to 150 m. These are superposed with the corresponding time series from the ERA5, NEWA, and NORA3 databases, highlighting periods where lidar data are available.

A qualitative analysis of the time series shows that the agreement between the lidar measurements and wind atlases is generally good, with the best match observed at the offshore sites FINO1 and FINO3 but also the coastal site Lista. At the coastal site Sola and the complex terrain Bjerkeim, NORA3 seems to perform better than NEWA and ERA5, partly because it was specifically designed for applications in Northern Europe. This direct comparison underscores the need for careful selection of wind atlases in wind resource assessment.

4.2 Error metrics across sites

Figure 7 compares and Fig. 8 compare four error metrics describing the discrepancies between in-situ measurements and modelled mean wind speed data across five sites: FINO1, FINO3, Sola, Bjerkeim and Lista at a single height, corresponding to the range gate of the lidar nearest to the five sites at range gates closest to 150 m and 300 m, respectively. These results complement the profiles shown in Fig. 9. Notably, the variability in these metrics across the models observed in Fig. 7 and Fig. 8 aligns with trends at other altitudes, reinforcing the consistency of our findings.

In terms of bias, ERA5 tends to underperform in coastal and complex terrains (Figs. 7 and 8, panels m and q), while NORA3, specifically developed for Norway, consistently shows the lowest bias across all the sites except at FINO1, where it is approximately 0.3 m s^{-1} . This contrasts with earlier studies, such as those by Solbrekke et al. (2021), which reported a smaller bias with a value of 0.14 m s^{-1} at the same site. A similar bias of 0.11 m s^{-1} was obtained by Cheynet et al. (2022) for 2009 alone, both at the same site and altitude at 100 m. The positive high bias observed at FINO1 during the campaign represents an underestimation of the wind speed by the wind atlases. This bias is also found when replacing the lidar data with the cup anemometer data at 100 m above sea level. This larger-than-expected bias may be attributed to the local depletion of wind resources caused by the construction of multiple wind farms around the mast since 2009. This finding is consistent with the study by Podein et al. (2022), which identified an increased wind speed bias between geostrophic modelled wind speeds and in-situ measurements at FINO1 after 2009, coinciding with the start of wind farm development in the area.

In panels b and f of Figs. 7 and 8, NORA3 and ERA5 demonstrate good performance metrics for offshore sites, achieving R^2 coefficients close to 0.9, consistent with findings from Cheynet et al. (2022). In complex terrain, NORA3 surpasses NEWA and ERA5, providing the most accurate wind speed estimates as indicated by the highest R^2 coefficients, which range from 0.7 to 0.8 for NEWA and ERA5 (Figs. 7 and 8, panel j). NORA3 also provides, on average, one of the lowest RMSE across different types of terrains. Interestingly, for the two offshore sites, ERA5 marginally outperforms and NORA3 perform nearly equally well in terms of RMSE (Figs. 7 and 8, panels c and g). Thus, NORA3's performance is fairly consistent across diverse topographies, whereas ERA5 may be reliably applied at far offshore sites, particularly where region-specific wind atlases are not available.

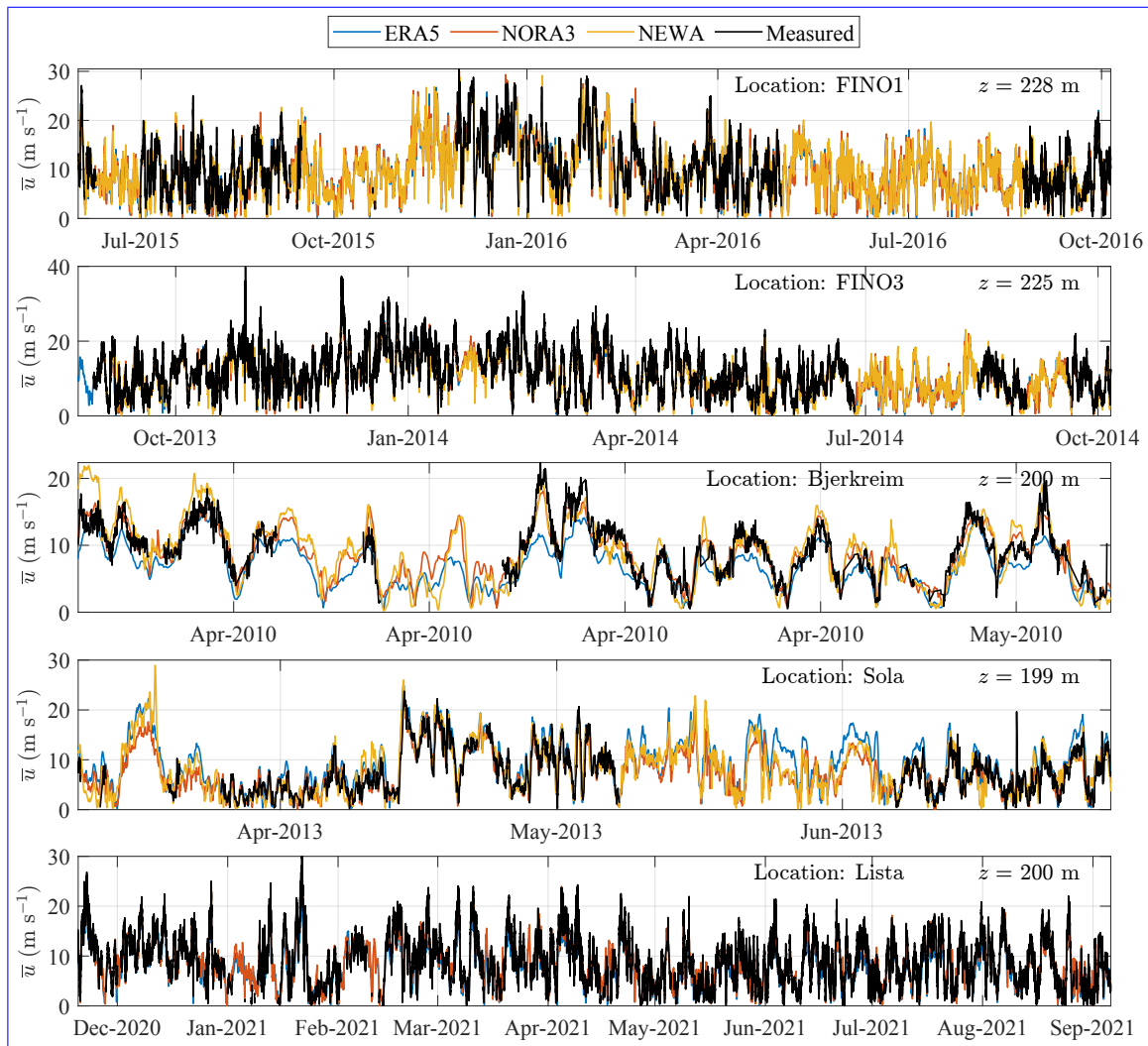


Figure 6. Comparative analysis Time series of error metrics for in-situ measurements versus modelled mean wind speed data across \bar{u} recorded at the five reference sites (FINO1, FINO3, Sola, Bjerkreim, Sola and Lista) at the range gate nearest to 200 m. Each row represents one of These are superposed with the sites and each column represents a different error metric, arranged corresponding time series from left to right: Bias, R^2 Coefficient the ERA5, RMSE (Root Mean Square Error) NEWA, and EMD (Earth Mover's Distance) NORA3 databases, highlighting periods where lidar data are available.

The fourth column of Fig. 7 analyses Figs. 7 and 8 displays the EMD. Offshore, NEWA exhibits the lowest EMD at FINO1 and the highest at FINO3 (panels d and h). Although NEWA was specifically engineered with this error metric in mind (Hahmann et al., 2020), the inconsistent EMD values at these two offshore sites may be attributed to the presence of multiple offshore wind farms around FINO1 at the time of data collection. At the coastal sites, the EMD values are comparable across all models, indicating similar performance among them. At the complex terrain Bjerkreim (Sola and Lista) and complex terrain (Bjerkreim),

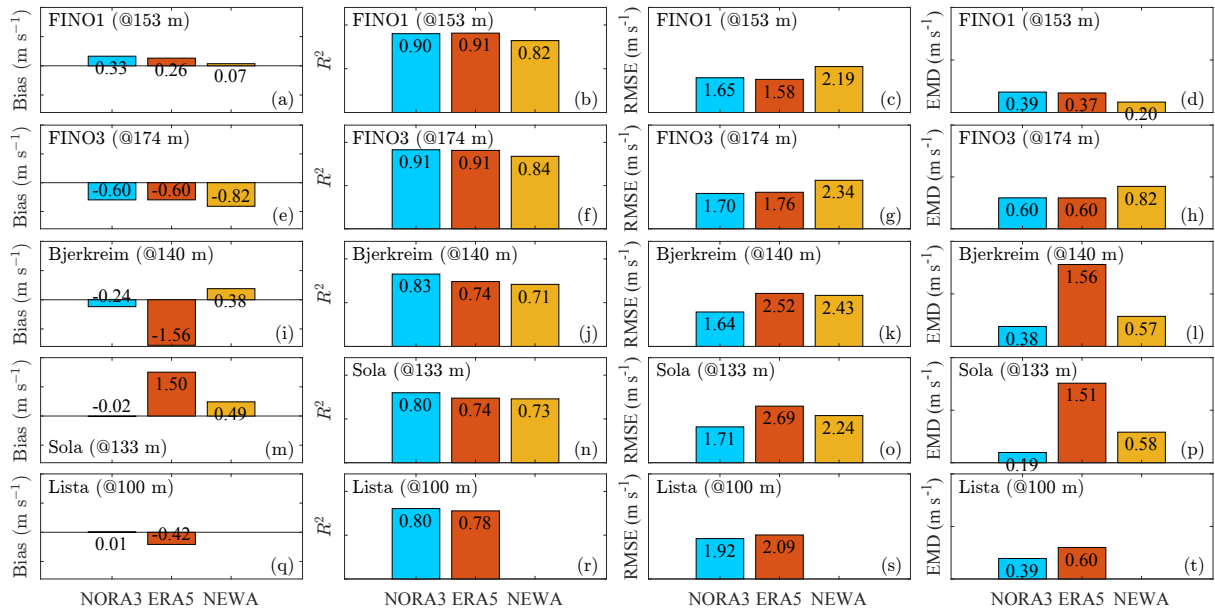


Figure 7. Error metrics at the range gate closest to 150 m for measured and modelled mean wind speed data across five sites (FINO1, FINO3, Sola, Bjerkreim, and Lista). Rows represent sites, and columns represent error metrics: Bias, R^2 , RMSE, and EMD.

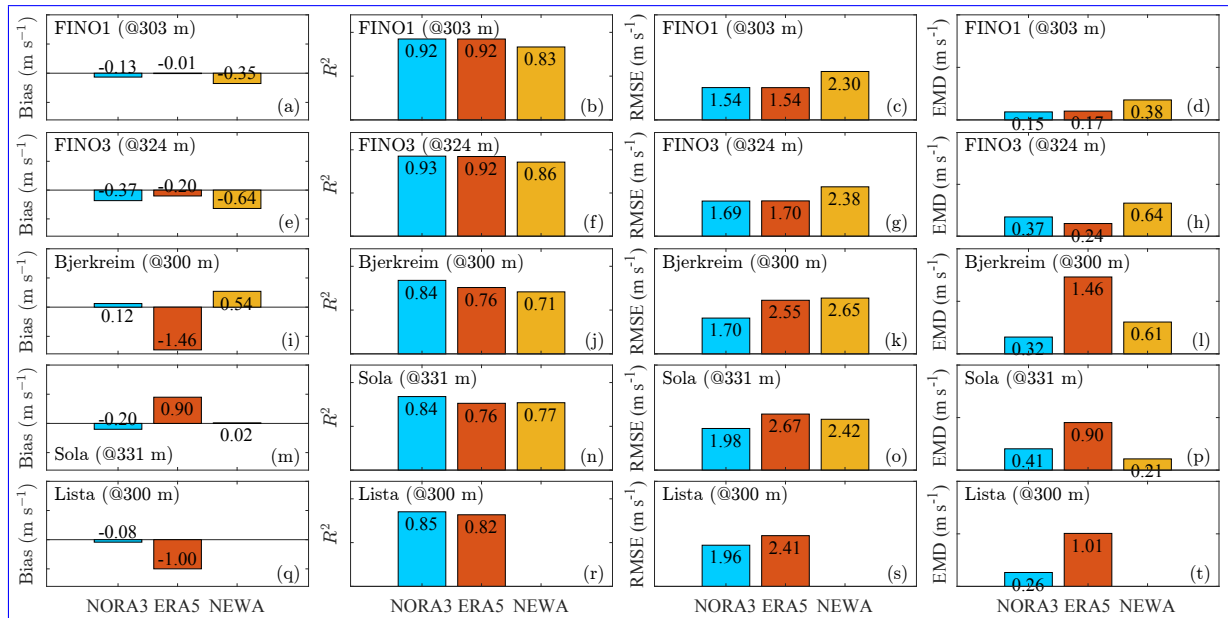


Figure 8. Error metrics at the range gate closest to 300 m for measured and modelled mean wind speed data across five sites (FINO1, FINO3, Sola, Bjerkreim, and Lista). Rows represent sites, and columns represent error metrics: Bias, R^2 , RMSE, and EMD.

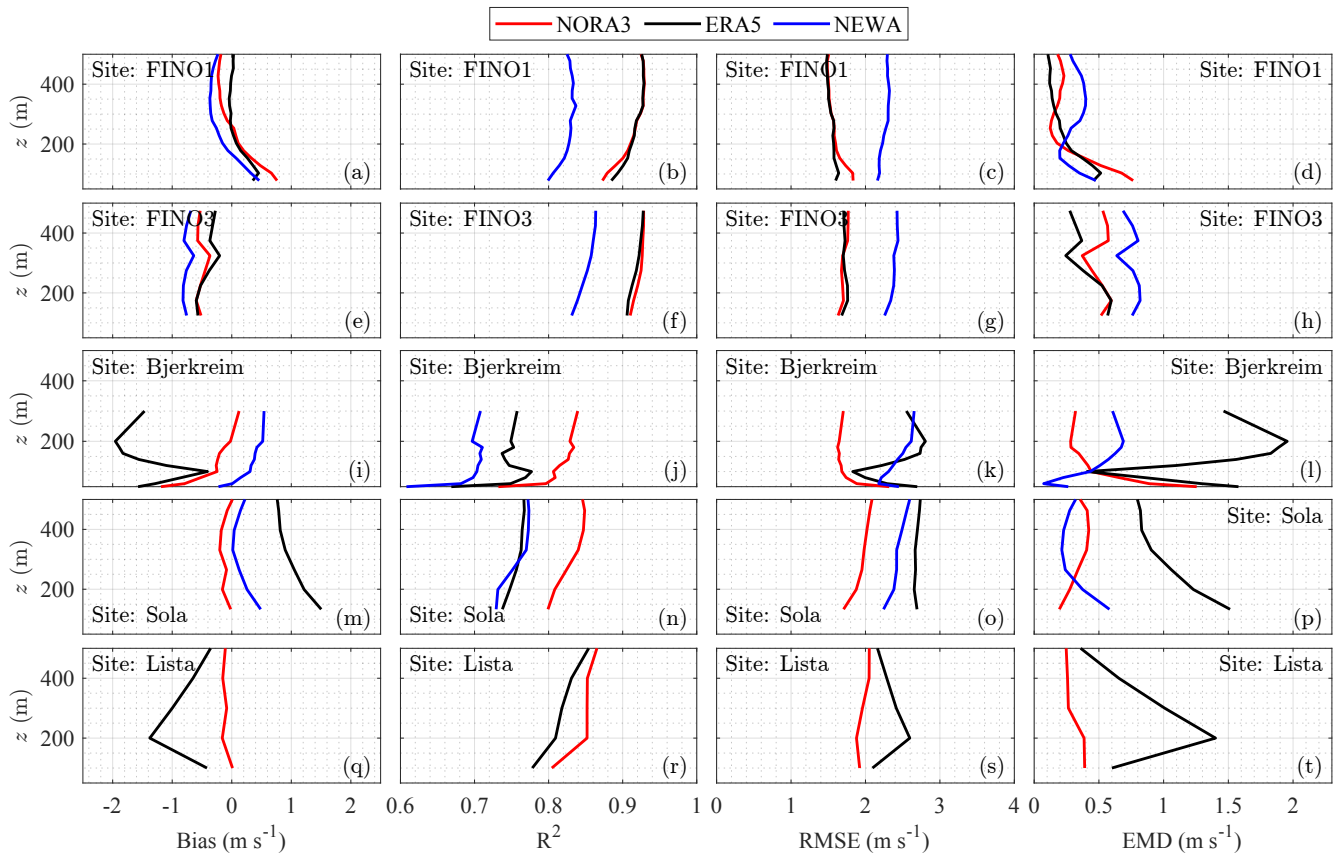


Figure 9. Comparative analysis of vertical profiles of Bias, R^2 Coefficient, RMSE (Root Mean Square Error), and EMD (Earth Mover's Distance) across of the wind speed across five sites (FINO1, FINO3, Sola, Bjerkreim, and Lista). Each row represents one site. Rows represent sites, and each column represents one column represents error metrics.

NORA3 achieves most of the time the lowest EMD, underscoring its potential in heterogeneous topographies (Figs. 7 and 8, panels l, p and t). As expected, ERA5 shows significantly higher EMD values than the other two models onshore, which is attributable to its lower horizontal spatial resolution.

The choice of the best model database is not straightforward as it depends on the specific error metrics and the location being analysed (Fig. 7). Furthermore, these error metrics are influenced by the height at which measurements are taken, further challenging the selection of an optimal database for specific applications (Fig. 9).

Figure 9 displays the vertical profiles of Bias, R^2 Coefficient, RMSE and EMD of the wind speed for the five sites (FINO1, FINO3, Sola, Bjerkreim and Lista) using the three model databases (NEWA, NORA3 and ERA5) at heights up to 500 m. It is reminded We remind that the data collection was limited to up to 300 m at the complex terrain site Bjerkreim and that data from NEWA were not available during the lidar campaign at Lista. Bias profiles show generally a decrease with increasing height across the different sites, except at Bjerkreim. In most cases, the agreement between the models and lidar measurements

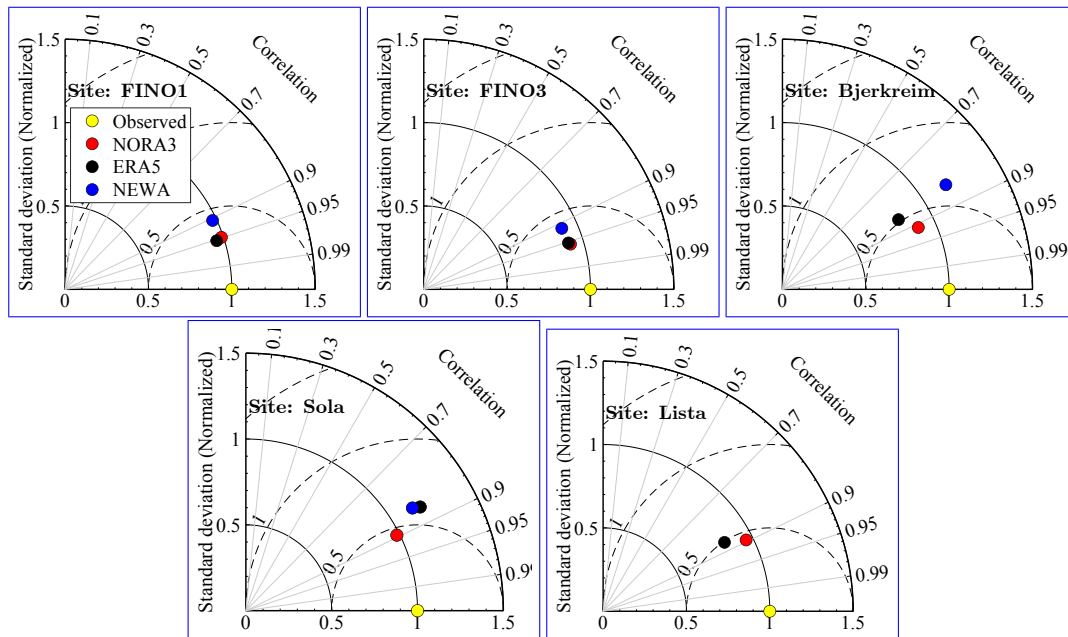


Figure 10. Taylor's diagrams for the five sites at the range gate closest to 150 m: FINO1 ($z = 153$ m), FINO3 ($z = 174$ m), Bjerkreim ($z = 140$ m), Sola ($z = 133$ m), and Lista ($z = 100$ m).

improves with height. However, this trend is not consistently observed at coastal and complex terrain sites, where deviations can occur, depending on the error metric and model database.

In Fig. 9, the bias profiles generally decrease with height at all sites except Bjerkreim, where the results are more nuanced (panel i); NORA3's bias decreases significantly, nearing zero at higher elevations, whereas NEWA's bias increases. In contrast, ERA5's bias is strongly dependent on height. For the R^2 and RMSE metrics, NORA3 and ERA5 demonstrate closely matched results at the offshore sites FINO1 and FINO3 across all heights, likely due to NORA3's utilization of ERA5 inputs as forcing. At the coastal site Sola, NORA3 consistently surpasses-outperforms NEWA and ERA5 in R^2 values at every height. In the complex terrain of Bjerkreim, NORA3 generally exhibits the lowest RMSE. Meanwhile, NEWA and ERA5 show varying RMSE results based on height, complicating the choice of the most appropriate wind atlases for wind resource assessment.

Taylor's diagram across the five sites: FINO1, FINO3, Bjerkreim, Sola and Lista, at a height of 150 m above the surface.

The analysis of EMD further challenges the selection process. Offshore, if the EMD is chosen as the preferred error metric, ERA5 appears to be the preferred option emerges as an excellent option offshore, especially for taller wind turbines with hub heights around near 150 m. In contrast, however, in complex terrains like Bjerkreim, terrain such as Bjerkreim, ERA5 performs worst, probably due to its low horizontal spatial resolution. In these areas, NEWA performs best below 100 m but is outperformed by m, but NORA3 outperforms it at higher altitudes. The Taylor diagram shown in Fig. 10 summarizes another performance assessment.

Figure 10 presents Taylor's diagrams, which provide an alternative indicator of the models' performance with respect to the lidar data. ~~This diagram visualizes~~ These diagrams visualize the standard deviation and correlation coefficient of modelled mean wind speed data ~~versus in-situ compared to~~ measurements at the five sites: ~~FINO1, FINO3, Bjerkreim, Sola and Lista.~~ In this figure, NORA3 ~~usually has the best match~~ typically shows the best agreement with the measurements, ~~especially as its marker is closest to the reference marker representing the observed data, particularly~~ in complex terrain and coastal areas. ~~It performs well across various tests but~~ However, ERA5 ~~performs~~ and NORA3 perform nearly equally well offshore.

The selection of the most suitable wind ~~atlases is highly contextual, depending on specific site conditions, measurement heights, and atlas depends on the topography, the measurement heights and the~~ desired error metrics. ERA5 ~~might be considered for broader applications~~ can be considered a versatile choice for offshore wind energy ~~and applications, extending beyond European waters.~~ NEWA may be appropriate when focusing on specific error metrics like EMD ~~while,~~ and NORA3 may deliver ~~consistent high performance in~~ consistently high performance at the Norwegian onshore and offshore sites. It should also be noted that the variability in model performance across the sites may partly be attributable to the different lidar instruments used. The DWL profiler deployed in Bjerkreim in 2010 was a now-discontinued WindCube V1, ~~whereas;~~ a scanning lidar WindCube 100S was used at the coastal site Sola and the FINO1 platform, and a discontinued WindCube WLS70 was deployed at the offshore site FINO3 and the coastal site Lista. Furthermore, each lidar's performance is inherently unique due to the fine-tuning of the hardware during the manufacturing and calibration process, the discussion of which is beyond the scope of this study. The discrepancy between the modelled wind speed data and lidar-based measurements in the complex site Bjerkreim or the coastal sites Sola and Lista is also influenced by the higher occurrence of non-homogeneous flow fields at onshore sites compared to offshore, particularly within the first 300 m above the surface, which can exacerbate the measurement uncertainties of lidar retrievals using DBS or velocity-azimuth display scanning modes (Klaas-Witt and Emeis, 2022).

4.2 Capacity factor estimates

This section ~~analyses the CFs for different turbine models~~ analyzes the CFs of the turbine models and AWE systems (section 3.3) at the five sites. ~~These estimates are based on the use of the~~ The estimates are derived from time series of ~~the~~ wind speed measured by lidars and provided by the three wind atlases. ~~For the case of wind turbines, each~~ Hereinafter, wind speeds from both the lidar instruments and the wind atlases are interpolated to the hub height of the wind turbines or spatially averaged over the operational height of the airborne wind energy (AWE) systems, ranging from 200 to 300 m above the surface (Fig. 5).

Each row of Fig. 11 represents a specific location, while each column refers to a different turbine type. ~~The~~ For the coastal and complex terrain sites, we calculated capacity factors for turbines with larger nameplate capacities than typical onshore models. Also, the CFs presented are not indicative of the sites' climatology, as the measurement campaigns were significantly shorter than the standard 30-year period. ~~Also, lidars tend to have low data availability under weak wind conditions, resulting in a higher estimated CF compared to long-term, continuous measurements. Consequently~~ Thus, the CF ~~here~~ should serve solely for comparison between the model and the measurement data, and not for evaluating the wind energy potential at these sites. ~~Estimated capacity factors for different turbine models at five sites, using lidar and three model datasets as wind inputs.~~

The offshore site FINO3 (Fig. 11, panels d, e and f) demonstrates the best agreement between model datasets and lidar measurements in terms of CF. However, the NREL 5 MW and the IEA 15 MW wind turbines exhibit substantial differences in CF, largely due to variations in hub heights. Higher hubs capture stronger winds, which could also explain the smaller discrepancies between measured and modelled data at these altitudes. For the 15 MW wind turbines at FINO3, the estimated CFs differ by a maximum of 0.03 between measurements and ERA5. At FINO1 (Fig. 11, panels a, b and c), the discrepancies between the model and measurements are greater than at FINO3, which might be due to the presence of wind farms around the mast. These findings align with those from Figure 11, which shows decreasing discrepancies at higher altitudes in terms of bias, EMD, and correlation coefficient lidar.

At the coastal sites Sola and Lista (Fig. 11, panels j-o), the NORA3 database provides nearly identical CFs to the lidar data. In contrast At Sola, ERA5 significantly overestimates the CF by approximately about 40% for the NREL 5 MW wind turbine and 38% for the IEA 15 MW wind turbine. In contrast, ERA5 slightly underestimates the CF of all turbine models at Lista. The NEWA hindcast also overestimates the CF at Sola, though but to a lesser extent: around about 16% for the NREL 5 MW turbine and 14% for the IEA 15 MW turbine.

At the complex terrain site Bjerkreim (Fig. 11, panels g, h and i), the NORA3 and ERA5 datasets slightly underestimate the CFs for the NREL 5 MW wind turbine. However, the NEWA dataset NEWA provides CFs that are closest to those measured by lidar. This finding is supported by Fig. 9, which indicates that the Earth Mover's Distance (EMD) EMD, a good metric for wind resource assessment, is lower for NEWA than that for ERA5 and NORA3 below 100 m at Bjerkreim.

Figure 12 presents shows the CFs for the 3 MW AWE system, which range from 0.15 MW and 100 kW AWE systems at the five sites of interest. Offshore, the CFs range from 0.13 to 0.22 offshore. In contrast, ?? shows CF values between 0.64 and 0.72 for the 3 MW system and from 0.66 to 0.71 for the 100 kW AWE kW system. This significant difference is primarily due to the varying cut-in wind speeds and rated wind speeds. The arises from the 100 kW system has a kW system's lower cut-in wind speed of (2 m m s^{-1} and a rated wind speed of approximately) and rated (7 m m s^{-1} , while) wind speeds compared to the 3 MW system has a MW system's cut-in wind speed of (9 m m s^{-1} and a rated wind speed of) and rated (22 m m s^{-1} . A) wind speeds. Trevisi et al. (2021) used a less conservative power curve was used in Trevisi et al. (2021) for a 3 MW AWE system with a cut-in wind speed of 2 m m s^{-1} and a rated wind speed between 7 and 8 m m s^{-1} , which led to a CF = 0.64. Although the 3 MW system used in our study displays a higher cut-out wind speed (30 m m s^{-1}) than the 100 kW system, it does not sufficiently compensate for the lower CF. Thus Therefore, the economic success of larger AWE systems depends may depend on incorporating lower cut-in and rated wind speeds.

Estimated capacity factors for the 3 MW AWE system from Eijkelhof and Schmehl (2022) at five sites, using lidar and three wind atlases as wind inputs. Estimated capacity factors for the 100 kW AWE system from Ranneberg et al. (2018) at five sites, using lidar and three wind atlases as wind inputs.

Regardless of the performance differences between the two AWE systems, the CFs at At the offshore sites FINO1 and FINO3 are similar when using reanalysis and lidar datasets. As noted in the previous section, NEWA slightly underestimates the CF at FINO1 and FINO3 compared to NORA3 and ERA5 (Fig. 12, panels a, b, f and g), the CFs of AWE systems derived from wind atlases and lidar datasets show similar values, whereas larger differences emerge when using wind turbine data (Fig. 11). The

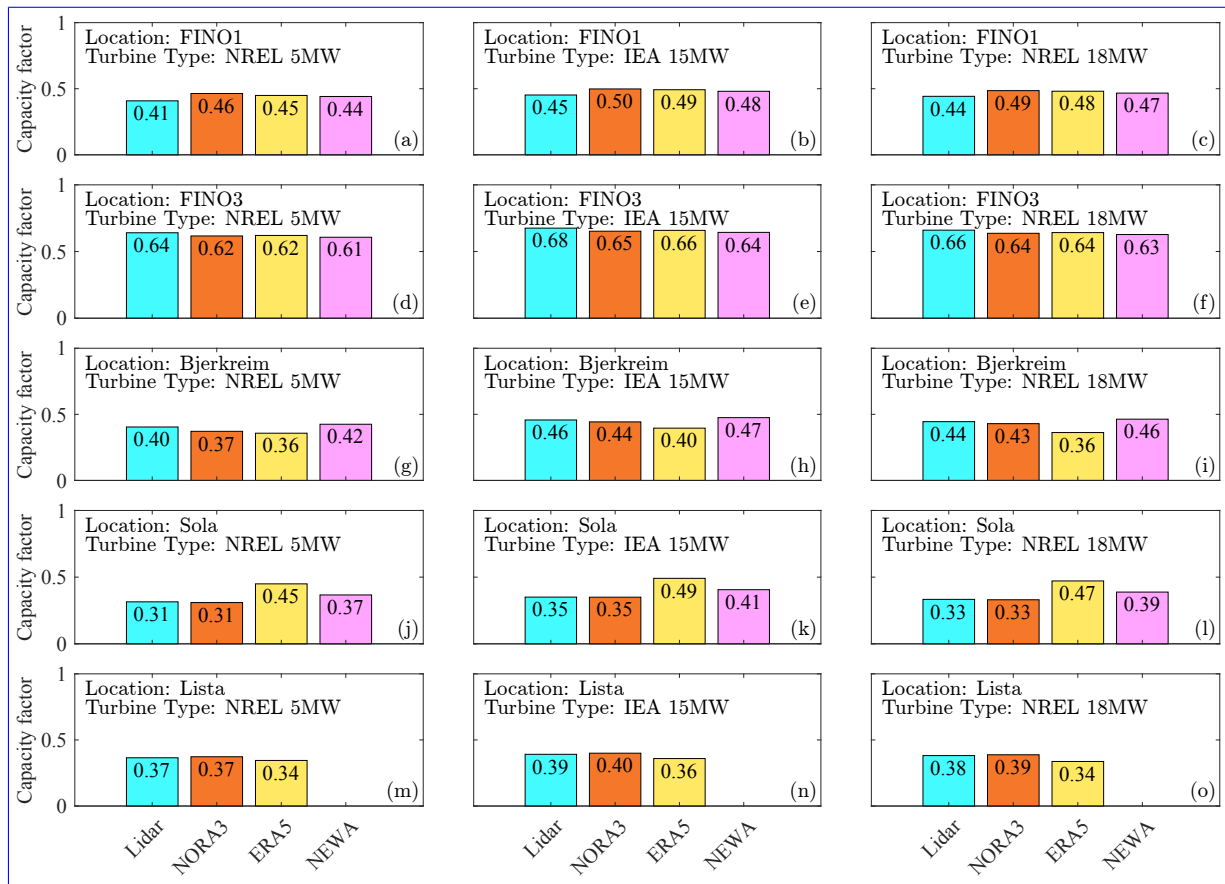


Figure 11. Estimated capacity factors for different turbine models (NREL 5 MW, IEA 15 MW and NREL 18 MW) at the five sites, using lidar and three model datasets as wind inputs.

small CF discrepancies between simulated and lidar data at FINO1 indicate that the data are collected at sufficient altitudes to minimise for AWE systems suggest that measurements at higher altitudes effectively reduce the influence of local wind resource depletion due to wind farm clusters at altitudes above 200 m on wind flow. Figure 12 implies also that discrepancies between measured and modelled wind speed in terms of CF may decrease with increasing altitude.

505 For the coastal sites (Sola and Lista (Fig. 12, panels d, e, i and j)) and the complex terrain site (Bjerkreim-Bjerkreim (Fig. 12, panels c and h)), the discrepancies in CF for the 3 MW AWE system are also minor. This is likely because wind speeds below 9 m s^{-1} , which fall below the system's cut-in speed, are not included in the CF calculation. Wind atlases thus capture moderate winds more accurately than weak winds. However, deviations This avoids erroneous flow modelling at moderate and low wind speeds, which sometimes reflect strongly stable atmospheric boundary layers that are not always well captured by wind atlases
 510 (Holtslag et al., 2013). Deviations between the model and measurements are also documented at wind speeds above 20 m s^{-1} , either near the surface (Bentamy et al., 2021; Gandoin and Garza, 2024) or within the first 100 m above the surface (Solbrekke

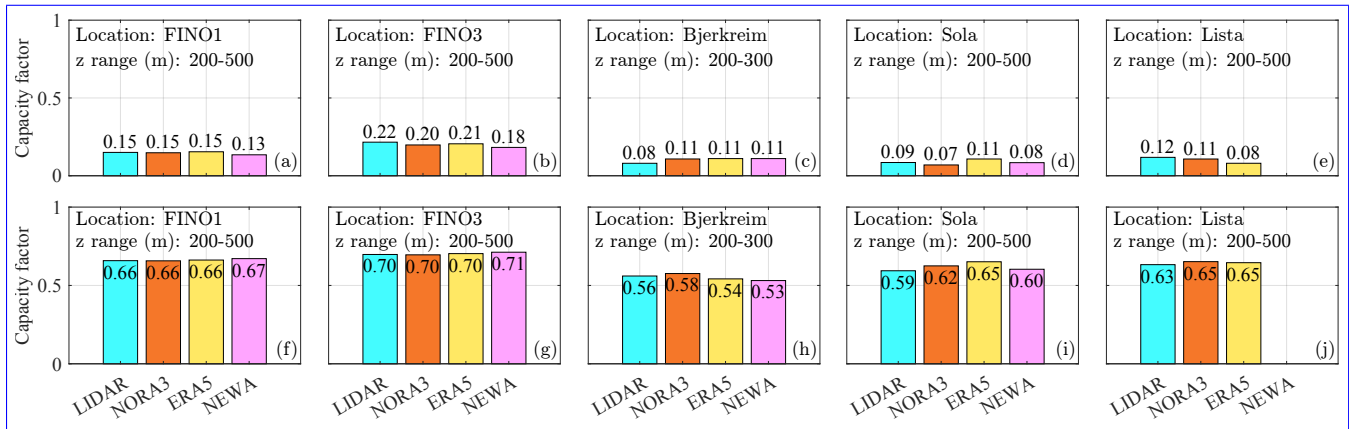


Figure 12. Estimated capacity factors for the 3 MW (top panels) and the 100 kW (bottom panels) AWE system at the five sites, using lidar and three wind atlases as wind inputs.

et al., 2021). ~~The underperformance of wind atlases under strong wind conditions may, however,~~ Nevertheless, such deviations may have a limited impact on the CF of wind energy systems with a relatively low cut-out speed of around 20 to 25 m s⁻¹.

515 While Although this subsection primarily ~~examined~~ examines the CF, which is ~~directly related~~ to the levelized cost of energy, it represents just one of several metrics used to assess the performance of intermittent renewable energy systems (Simpson et al., 2020). Alternative metrics, such as the Gini coefficient (Malz et al., 2020) and the correlation coefficient between different renewable energy sources such as solar and wind (Malz et al., 2020; Jurasz et al., 2020), also provide valuable insights into the variability of power output in AWE systems and wind turbines. ~~Although the tall wind speed profiles established in this study could assess~~ However, examining the complementarity of AWE systems with other energy sources like, such as wind and solar, ~~such discussions fall~~ falls outside the scope of this study.

520

5 Discussions

This section explores the challenges and opportunities for improving wind energy assessments. We first address the need for more capable wind profilers to meet the demands of larger turbines and AWE systems. We then discuss the limitations of mesoscale models in complex and coastal terrains and the potential benefits of integrating them with microscale models. These considerations suggest some pathways for improving wind flow simulations and instrument design in future research.

525

5.1 A need for more powerful wind profilers?

When commercial DWL profilers became available in the 2000s, wind turbines had a nominal capacity of about 5 MW, with tip heights around 150 m. This made the typical lidar scanning range of 200–300 m sufficient at the time. However, wind turbine sizes have grown significantly since then. For instance, in 20232024, Mingyang Smart Energy ~~proposed~~ installed a 20 MW turbine with a tip height potentially reaching 300 m ~~-The increasing-~~ (Casey, 2024). This growth, coupled with the rising

530

interest in AWE systems ~~further highlights the technical limitations of traditional lidar operating at heights between 200 and 600 m, underlines the need for potentially more powerful wind~~ profilers. While scanning lidars can extend profiling range, they are often heavier, more expensive, and less reliable, as they contain more moving parts and are not specifically designed for wind profiling.

535 ~~This raises concerns that the development of DWL profilers is not keeping pace with the growing size of wind turbines and AWE systems.~~ There is a clear need for a new generation of DWL instruments capable of reliably profiling winds up to 500 m above the surface or even higher. Such instruments remain uncommon among commercial lidar producers. One notable exception is Halo Photonics by Lumibird, which has developed the BEAM 6X series, capable of measuring wind speeds up to 500 m. ~~However, up to date we cannot find studies demonstrating~~ (Halo Photonics, 2024). ~~To date, however, we have not been~~
540 ~~able to find any studies that demonstrate~~ the validity of measurements from this lidar.

5.2 Mesoscale limitations and microscale needs

~~This study primarily focuses on~~ In wind energy, wind simulations are typically performed using two types of models: mesoscale models, which provide wind speed data ~~derived from mesoscale~~ over spatial scales ranging from a few kilometres to hundreds of kilometres, and microscale models, which ~~have certain limitations, particularly for applications~~ operate at smaller scales,
545 from a few metres to approximately one kilometre. While these models are complementary, microscale models are particularly useful in capturing wind flow variability in complex terrain. ~~In offshore sites, such as FINO1 and , where topographic features significantly influence wind conditions or near structures such as buildings and wind farms.~~

This study primarily focuses on mesoscale-derived wind speed data, which can be limited in capturing fine-scale flow features in complex terrains or near coastal sites. For offshore sites like FINO3, microscale effects ~~may be~~ are likely negligible.
550 However, ~~in coastal sites like~~ for coastal sites such as Sola and Lista, ~~microscale models could~~ and the complex terrain at Bjerkeim, microscale modelling may improve the agreement between ~~modelled~~ simulated and measured wind speeds. ~~In complex terrain, such as at~~ At Bjerkeim, computational fluid dynamics ~~models may be necessary to account for phenomena like~~ (CFD) models could help capture complex phenomena, such as flow recirculation and detached downslope flow, which are ~~common in the mountainous terrain of~~ prevalent in mountainous terrain like Southeastern Norway. ~~Future research should~~
555 ~~explore the potential~~

At FINO1, microscale flow simulations may also be needed to model wake effects on measurements. Future studies should investigate the benefits of coupling mesoscale and microscale models to ~~improve~~ enhance performance metrics at ~~the~~ coastal and complex sites. ~~We expect this coupling might cause the near-zero bias of NORA3 to shift toward a negative or positive value, while possibly reducing the current bias of NEWA and ERA5 toward zero. However, such an investigation falls outside~~
560 ~~the scope of this study.~~

The comparison conducted in this study remains valuable because microscale models, while potentially more precise than mesoscale models in complex terrain, depend on accurate initial and boundary conditions that can be provided by the mesoscale models. ~~Finally, it should be noted that the discrepancy between the modelled wind speed data and lidar-based measurements in the complex site Bjerkeim or the coastal sites Sola and Lista is not solely attributable to the lower grid resolution of the~~

565 mesoscale wind model. It is also influenced by the higher occurrence of non-homogeneous flow fields at onshore sites compared
to offshore, particularly within the first 300 m above the surface, which can exacerbate the measurement uncertainties of lidar
retrievals using DBS or velocity azimuth display scanning.

6 Conclusions

This study examines the capability of three ~~state-of-the-art~~ wind atlases, NORA3, NEWA, and ERA5, in accurately modelling
570 wind speed profiles up to 500 m above the surface for wind energy applications. Reference wind speed profiles were obtained
from Doppler wind lidar (DWL) measurements conducted at five distinct sites in Northern Europe. These sites encompass
diverse topographies such as flat coastal terrain, mountainous regions, and offshore environments. The objective of the study is
to broaden the validation scope to altitudes critical for large wind turbines and airborne wind energy (AWE) systems. This study
addresses a significant challenge in wind energy, as there has been relatively limited investigation into tall wind speed profiles
575 using scanning DWL in profiler modes for wind resource assessment at heights up to 500 m above the surface.

The study found that all three wind atlas datasets (NORA3, NEWA, and ERA5) ~~exhibit high quality~~ perform well in offshore
locations, with ERA5 showing the closest correlation to lidar data up to 200 m. From 200 m to 500 m, NORA3 and ERA5
perform equally well in terms of correlation coefficient and root mean square error (RMSE), though NORA3 has a lower bias
and lower earth mover's distance (EMD) above 200 m. Onshore, NORA3 outperforms ERA5 and NEWA at all heights for most
580 error metrics. While the agreement between the models and lidar measurements generally improves with height, this trend is
less consistent at coastal and complex terrain sites, where deviations occur, especially for ERA5 and NEWA.

In terms of the capacity factor (CF) for large wind turbines, all datasets show good agreement with CF derived from lidar data
offshore, particularly for the largest turbines. However, at the FINO1 site, CF is overestimated by all models, likely due to local
wind resource depletion from surrounding offshore wind farms. In coastal terrain, NORA3 provides excellent CF agreement
585 with lidar data, NEWA performs reasonably well, but ERA5 overestimates the CF. In complex terrain, NEWA and NORA3 both
perform well, while ERA5 substantially underestimates the CF.

For AWE systems, the CF was fairly consistent across all the wind atlases but showed considerable dependency on the
power curve. ~~In particular, the efficiency of~~ Smaller AWE systems with lower cut-in and rated wind speeds achieved higher CFs
and efficiency, whereas the larger 3 MW AWE system considered in this study ~~is penalized by a~~ was penalised by its high
590 cut-in and rated wind ~~speed compared to the smaller 100 kW system~~ speeds. Therefore, designing larger AWE systems with
lower cut-in wind speeds is essential to reduce the levelised cost of energy for such systems. Finally, the development of DWL
profiler technology must keep pace with the growing size of wind turbines, necessitating more powerful profilers to avoid the
increased costs associated with using scanning lidar instruments for tall wind profiles.

~~It should be noted that this study was conducted using~~ This study was based on relatively limited datasets, ~~which do not~~
595 ~~cover a:~~ the temporal coverage is insufficient to represent a full climatology timescale and ~~include measurements from the~~
spatial coverage is restricted to a few locations in Norway and the North Sea. Although the sites selected in this study provide a
diverse range of topographies, having more locations from additional countries would enhance the robustness of the findings.

600 Additionally, the wind atlases have a limited temporal resolution of ~~the dataset may not fully~~ 30 to 60 minutes, which may not
adequately capture short-term variability variations in wind speed profiles, ~~which~~. This aspect needs to be considered in regions
where non-stationary boundary layers are prevalent.

The general conclusion is that NORA3 excels onshore, while ERA5, with its global coverage, performs equally well offshore. Onshore data quality is slightly lower ~~across for~~ all datasets due to the complexity of wind patterns over land, ~~with~~. In particular,
ERA5 ~~showing shows~~ significant height-dependent errors, possibly due to ~~inaccuracies in geopotential height and pressure~~
~~level data over mountainous terrains~~ lower spatial resolution compared to NEWA and NORA3. These findings ~~underscore~~
605 highlight the importance of selecting the appropriate wind atlas and wind models for specific sites and altitudes to ~~enhance wind~~
~~speed predictions and wind energy estimates~~. ~~Performance variations across different locations and heights highlight the need~~
~~for tailored wind resource assessments, especially in complex terrains~~. ~~Smaller AWE systems with lower cut-in and rated wind~~
~~speeds achieve higher CFs and efficiency compared to multi-megawatt systems~~. ~~Therefore, designing larger AWE systems with~~
~~low cut-in wind speeds is crucial for broader adoption~~. Finally, the development of DWL profiler technology must keep pace
610 ~~with the growing size of wind turbines, requiring more powerful profilers to avoid the higher costs associated with the use~~
~~of scanning lidar instruments for tall wind profiles~~ improve wind resource assessment, considering performance variations of
wind turbines and AWE systems at different locations.

Appendix A: Error metrics with non-linear wind speed regression

A non-linear regression was also tested ~~instead of an as an alternative to~~ interpolation for smoothing the vertical wind speed
615 profiles up to 500 m ~~above the surface for NEWA and for NEWA~~, NORA3 and ~~for the first six height levels for~~ ERA5. The
regression relies on fitting a modification of the wind profile model by Deaves and Harris (1982). This modified analytical
function combines a classic logarithmic profile with a third-order polynomial function and is expressed as

$$\bar{u}(z) = \frac{u_*}{\kappa} \log \left(\frac{z}{z_0} \right) + p(z), \text{ with} \quad (\text{A1})$$

$$p(z) = a_1(z) + a_2(z)^2 + a_3(z)^3, \quad (\text{A2})$$

620 where z is the height above the surface; $\kappa \approx 0.4$ is the von Kármán constant and z_0 is the roughness length. The coefficients a_i ,
where $i = \{1, 2, 3\}$, are determined empirically by least-squares fit (Cheynet et al., 2024). For the coastal and complex terrain
sites, the roughness length is approximated by the values 0.01 m and 0.1 m, respectively, following the traditional roughness
length classification onshore (Wieringa, 1980, 1986). These values are realistic enough to ensure a reasonable fit in the lower
part of the ~~atmospheric boundary layer~~ ABL. Above the ocean, the roughness length is estimated using Charnock's relationship
625 (Charnock, 1955), which quantifies the dependency of the roughness length on the sea state ~~(Charnock, 1955)~~:

$$z_0 = \frac{a}{g} u_*^2 \quad (\text{A3})$$

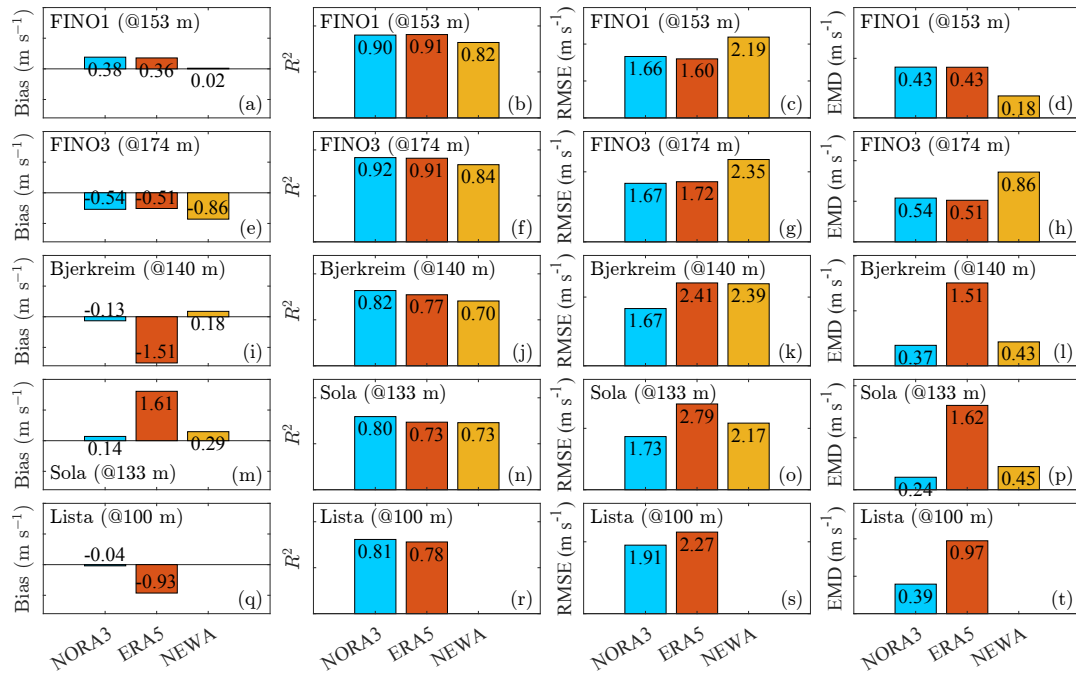


Figure A1. Comparative analysis of error metrics at the range gate closest to 150 m for in-situ measurements versus measured and modelled mean wind speed data speeds across the five sites (FINO1, FINO3, Sola, Bjerkreim, and Lista). Each row represents one site. Rows represent sites, and each column represents a different error metric, arranged from left to right: Bias, R^2 Coefficient, RMSE (Root Mean Square Error), and EMD (Earth Mover's Distance). The spatial collocation was obtained by Wind speed profiles were aligned using non-linear regression instead of linear interpolation.

where $g = 9.81 \text{ m s}^{-2}$ is the gravitational acceleration, and $a \approx 0.014$ is an empirical coefficient (Kraus and Businger, 1994). Equation (A3) is combined with the neutral logarithmic wind speed profile (Kaimal, 1994)

$$\bar{u}(z) = \frac{u_*}{\kappa} \ln\left(\frac{z}{z_0}\right) \quad (\text{A4})$$

630 into a new equation:

$$z_0 - \frac{a}{g} \left[\frac{\kappa \bar{u}(z_r)}{\ln(z_r/z_0)} \right]^2 = 0, \quad (\text{A5})$$

which is solved for $z_r = 10$ m and provides an estimate of the roughness length in the marine atmospheric boundary layer (ABL).

635 Figure A1 and Fig. A2 present the wind speed error metrics used to assess/evaluate the performance of the wind atlases compared to against lidar measurements, based on wind speed data, at a specific height and both at the range gate nearest to 150 m and across multiple heights up to 500 m across m at the five investigated sites, respectively. The non-linear regression produces smooth profiles of error metrics that show less variance around their mean but does not necessarily reduce/minimise the error metrics themselves. Several hundreds or thousands of samples are thousand samples were used to compute these ensemble-

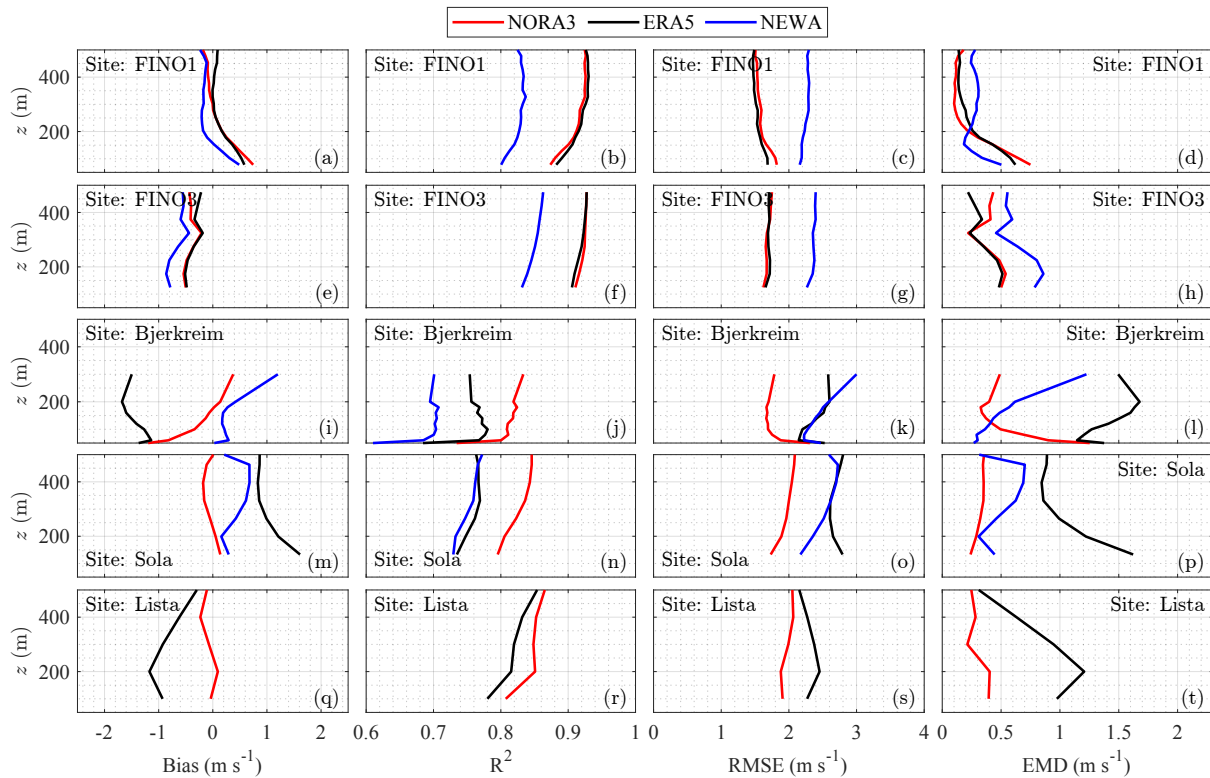


Figure A2. Comparative analysis of vertical profiles based on non-linear regression for of Bias, R^2 Coefficient, RMSE (Root Mean Square Error), and EMD (Earth-Mover's Distance) of horizontal wind speed based on non-linear regression across the five sites: FINO1, FINO3, Sola, Bjerkreim and Lista. Each row represents one site and each column represents one error metric.

averaged error metrics, which tend to smooth out possible discrepancies due to help smooth out potential discrepancies caused by linear interpolation. Therefore Consequently, when sufficiently large datasets are available, linear interpolation of the vertical wind speed profiles at additional height levels produces good yields reliable results and was found to be the most reliable identified as the most robust approach in this study.

Data availability. The NEWA data were collected from the "New European Wind Atlas", which is a free, web-based application developed, owned and operated by the NEWA Consortium. For additional information see www.neweuropeanwindatlas.eu. The ERA5 reanalysis data used in this study are publicly available through the Copernicus Climate Change Service (C3S) Climate Data Store (CDS) at <https://cds.climate.copernicus.eu/>. The NORA3 reanalysis data used in this study are publicly available through the Norwegian Meteorological Institute's THREDDS server at <https://thredds.met.no/thredds/projects/nora3.html>. The modified datasets used to generate the figures in this study will be made publicly available on Zenodo under a BSD-3 open-access license.

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650 EC and JMD, and all authors participated in the review and editing process. Supervision was provided by JR and EC, and JR was responsible for funding acquisition.

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