

Periods of constant wind speed: How long do they last in the turbulent atmospheric boundary layer?

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Abstract. ~~A non-investigated feature of the atmospheric turbulent wind, named~~ We perform a statistical analysis of the occurrence of periods of constant wind speed ~~, is introduced and investigated in atmospheric turbulence.~~ We hypothesize that such periods of constant wind speed are related to characteristic wind field structures (e.g., ramps or jets), which, when interacting with a wind turbine, may induce particular dynamical responses. Therefore, this study focuses on ~~the characterization of the~~ characterizing the constant wind speed periods in terms of their lengths, probability of occurrence, and ~~extreme events~~ extremes. Atmospheric off-shore wind data are analyzed. Our findings reveal that the statistics of long constant wind speed periods are an intrinsic feature of the atmospheric boundary layer ~~and show the challenging power law behaviour of extreme events, which depends.~~ We strictly confirm that the probability distribution of such periods of constant wind speeds follows a Pareto-like distribution admitting power law behavior for periods exceeding the large eddy turnover time. The power law characteristics depend on the local conditions and the precise definition of wind speed thresholds. A comparison to wind time series generated with standard synthetic wind models and to time series from ideal stationary turbulence suggests that these structures are not characteristics of small-scale turbulence but seem to be consequences of larger-scale structures of the atmospheric boundary layer ~~,~~ and thus are a typical multi-scale effect. Given the conclusive results, we show that the Continuous Time Random Walk model, as a non-standard wind model, can be adapted to generate the statistics of those periods of constant wind speed measured from the atmospheric turbulent wind.

1 Introduction

The estimation of the loads experienced by a wind turbine (WT) is fundamental for decision-making processes during the design phase of the various components of the machine, as well as for control strategies during its operation. Such estimation is performed through numerical modelling of the interaction between the WT and the incoming wind. Therefore, an accurate description of the wind within the atmospheric boundary layer (ABL) is essential for correctly calculating the loads acting on the WT. The International Electrotechnical Commission (IEC, 2019) has defined both the widely-used standard parameters ~~and models~~ for the characterization of the atmospheric wind .These standard wind field models and the models for generating synthetic wind fields used for numerical estimation of loads on the WT. These IEC standard guidelines extensively consider the spectral properties and coherence of the velocity components of the wind. Nevertheless, such standards are designed to

25 mimic the atmospheric wind in a computationally efficient way. As a result, ~~some features of the flow for the characterization as well as for the wind fields, some flow features~~ in the ABL are neglected. ~~During or simplified.~~ Furthermore, during the past decades, new challenges in the design process of wind turbines have emerged (Veers et al., 2019). On the one hand, trends in the design of modern WT account for bigger rotor areas and less rigid structures (i.e. blades) to capture more energy from the available wind resources. On the other hand, the weight and material requirements of each component are being pushed to
30 minimal levels. As a result, new WTs are becoming, in general, larger and less rigid. Therefore, some of the characteristics of the atmospheric wind that ~~have been neglected~~ need to be addressed in the IEC standard wind models might become relevant for extra loads not previously considered. ~~Together with the WT manufacturer involved in our research~~ within the design of smaller and stiffer WTs.

Based on cooperative research with a WT manufacturer, we concluded that one of these features, disregarded by the IEC
35 guidelines, is the periods of constant wind speed (CWS) in atmospheric flows. Such periods are defined as the intervals of time over which the magnitude of the wind speed remains almost constant within a certain range, defined by a threshold value. ~~Such events are important for the functionality of a WT and can lead to beneficial, less noisy working conditions, but also to undesirable increasing dynamics, especially if weakly undamped vibrations are present under such operating conditions. As discussed below, such events are also of general interest for turbulent flows~~ In the following, we first contextualize the periods
40 of CWS within the general characterization of turbulent features. Afterwards, we discuss in which way such CWS periods may be relevant for a WT.

~~The concept of persistence is closely related to~~ Concerning the periods of CWS as a general feature of wind it should be mentioned that there are relevant and well-investigated turbulent quantities closely associated with our definition of periods of CWS. The persistence phenomenon is straightforwardly recalled. Persistence characterizes how long ~~a system~~ the flow remains
45 in a particular state before switching to another one. ~~As a general concept, this feature has been investigated in various research fields (Saleedo-Sanz et al., 2022; Grebenkov et al., 2020), such as in economy (Fletcher and Forbes, 2002; Caporale et al., 2022; Nikitopoulos, 2019), biology (Arachchige et al., 2021), epidemiology (Kane and T., 2010), and meteorology (Saleedo-Sanz et al., 2021; Lee et al., 2021; Voyer et al., 2021).~~ One prominent concept that uses persistence Persistence times can be inversely correlated with extreme wind speeds or gusts. In this context, the exceedance statistics proposed by Rice's theorem (Rice, 1944) have been applied for describing gusts as
50 excursions at which certain thresholds of wind speed are exceeded (Kristensen et al., 1991; Young and Kristensen, 1992; Manshour et al., 2019). Another interpretation of persistence within turbulent flows is the so-called zero-crossing ~~method.~~ For a random process $x(t)$ with analysis. In this case, for a zero-mean signal, the waiting times between two successive crossings of its zero level are evaluated. Statistical properties of zero-crossings have been used to characterize ~~quantities like~~ intrinsic turbulent quantities such as the Taylor micro-scale (Narayanan et al., 1977; Sreenivasan et al., 1983; Kailasnath and Sreenivasan, 1993; Poggi and Katul, 2010) or the integral length scale (Mora and Obligado, 2020; Mazellier and Vassilicos, 2008). Analysis of zero-crossings of
55 velocity and temperature fluctuations in atmospheric turbulent data ~~inside canopies, focused on thermal stratification, has been reported (Cava and Katul, 2009; Cava et al., 2012).~~ The scheme of have been discussed (Cava and Katul, 2009; Cava et al., 2012; Chameck

To summarize, the above-mentioned investigations showed that the statistical characteristics of the persistence for experimental and atmospheric data exhibit a power law behavior up to a certain threshold, followed by log-normal or exponential cutoffs.

60 It is worth noting that even though the inter-arrival times of both, excursions and zero-crossings ~~does not investigate the structure of the signal between the crossing, such as possible~~, refer to structures between particular turbulent states, they do not correspond to the periods of reduced turbulent amplitudes, in which we are interested. ~~In fact, we introduce a new approach for measuring the events of our study~~ Further details of the differences between CWS periods and inter-arrival times between excursions and zero-crossings are shown in Appendix A. Nevertheless, the method and statistics of such persistent
65 ~~zero-crossing~~ events are relevant to the discussion. Of special interest are self-similar, critical, or fractal features of turbulence that propose a power law behavior for the probability distribution of the time intervals with duration T , which can be formulated as $p(T) \propto T^{-\alpha}$ (in particular for the limit of large T). ~~Such power-law statistics may lead to the demanding phenomenon of divergence of mean value or variance, depending on the value of α , and can be taken as proof for scale invariance and extreme events.~~ A characteristic feature of a power law distribution is the absence of an intrinsic scale, i.e., the probability of
70 observing a realization larger than T is $T^{-\alpha+1}$ times the probability of observing a realization larger than T ; independently of the value of T . The far-tail regime of many distributions occurring in complex systems is assumed to exhibit power law behavior (Laherrere and Sornette, 1998). In the context of wind energy, for instance, a Pareto distribution has been tested to extrapolate the response of a multi-megawatt wind turbine generator (Dimitrov, 2016).

Next, we discuss the potential relevance of an accurate description of the CWS periods for WT applications which is directly
75 linked with the increasing size and flexibility of the WTs. In the simplest case, such periods of CWS should imply relatively quiescent operating conditions for a wind turbine when the CWS structure occurs homogeneously in the rotor area. A more entangled case might occur when resonant or near-resonant dynamics appear for specific periods of CWS, over which the resonance can be strongly excited. In particular for the larger WTs, the CWS periods may be restricted to a sub-area of the rotor plane. In this case, resonant dynamics exhibiting 3P oscillations may be amplified. Within this context, recent studies
80 are devoted to interfaces between turbulent and non-turbulent states in atmospheric wind measured at typical WT heights (Neuhaus et al., 2024). Meanwhile, numerical and experimental investigations on the laminar-turbulent transition mechanisms on rotating wind turbine blades have shown changes in the transition characteristics over a single revolution, which affect the aerodynamic response of the WT (Lobo et al., 2023; Özçakmak et al., 2020).

As a last possible application for WTs, we want to mention that the statistical features of CWS may become of interest for
85 probabilistic design methods. Although the methods proposed by the IEC for estimating WT loads are mostly deterministic, in recent years, probabilistic design methods have been introduced (Koçak, 2008; Leahy and McKeogh, 2013; Patlakas et al., 2017). However, the available studies using such techniques are mainly focused on characterizing the so-called low-wind-speed events over which very low or no energy is produced. Therefore, the low-wind-speed periods are normally defined for wind speed values below the cut-in thresholds of the WTs. Results on the statistics of low-wind-speed periods have been reported for
90 local data (Ohlendorf and Schill, 2020; Kruyt et al., 2017; Leahy and McKeogh, 2013; Patlakas et al., 2017; Sinden, 2007). In common, these studies investigated modeled time series based on extrapolated or reanalyzed local records (Brune et al., 2021)

95 ~~as surrogates for the design and load assessment of WTs (Abhinav et al., 2024; Kelma, 2024). Such probabilistic approaches account for more reliable estimations by considering the explicit calculation of the uncertainties from the operational conditions, aerodynamic models, materials, etc (Sørensen and Toft, 2010). Characteristics of the wind are then defined as stochastic variables within the probabilistic model parametrization. Accordingly, broader and more accurate statistical descriptions of the intrinsic features of the wind inside the ABL account for a reduction in the uncertainty of the estimated loads and responses of the WTs.~~

100 ~~We~~ In this paper we focus on the periods of CWS as general features of turbulence, the discussion of possible impacts on a WT will be done only as side remarks. In particular, we characterize the statistics of periods of CWS (with a low level of turbulent fluctuations) from wind measurements in the ABL. In a preliminary investigation (Moreno et al., 2022), the method for the assessment of such events from wind speed time series was presented, and first results on the characterization of the periods of CWS in terms of their duration and probability distributions were also reported. Special attention within the characterization was given to the tails of the distributions, which describe extremely long periods. ~~Such strong periods are expected to have a stronger influence on a WT.~~ Interestingly, we found that the probability distribution for very long periods shows a power law decay $p(T) \propto T^{-\alpha}$. Furthermore, a comparison with wind data generated by an IEC standard model (IEC, 2019) revealed that the model underestimates the frequency of occurrence of the extremely long periods measured in the ABL. ~~Along with the mentioned findings, some points remained inconclusive in our initial investigation. These points concern whether these periods~~ In this study, we aim to address whether the periods of CWS are induced by specific orographic perturbations, whether they are laminar or low turbulent structures, and whether they are intrinsic features of a turbulent flow or, respectively, rather result from large-scale interactions within the ABL. ~~As an extension of the work presented in (Moreno et al., 2022), in this study we aim to address such open questions. Firstly, by characterizing the periods of constant wind speed from a different measurement site; and secondly, by comparing the results with experimental~~ To characterize the CWS periods we use data from offshore wind, as we expect to have less special orographic effects, compared to onshore data, and thus get more general insights of the CWS structure. This is also the motivation to compare the results with ideal turbulent data from a free jet experiment. Furthermore, a stochastic wind field model for WT simulations is presented as a surrogate approach to incorporate the statistics of long periods of CWS from turbulence in the ABL.

The paper is structured as follows: Sec. 2 retakes the method for measuring the periods and describes the atmospheric wind data to be analyzed. In Sec. 3, the results of the statistical characterization of the periods from the atmospheric data are shown. In Sec. 4, we compare the results from ABL data to those from two different data sets, i.e., IEC standard wind model and experimental ideal turbulence. In Sec. 5, we present our conclusions and potential future work.

2 Methodology and Data

2.1 Definition of a period of CWS

A period of constant wind speed Following (Moreno et al., 2022), a period of CWS (T_c) is defined as the time over which the magnitude of the wind speed $u(t)$ exhibits low-amplitude fluctuations enclosed within certain thresholds (Moreno et al., 2022). A period T_c is depicted in Fig. 1. Over the length of T_c , the wind speed remains inside the *constant speed interval*, u_t " , where u_t is a the reference speed value at $t = t$ and " is the maximum acceptable magnitude of the fluctuations around u_t . In the figure, the horizontal red bars illustrate the thresholds that delineate the constant speed interval. It should be noted that these periods are not strictly laminar but periods with a smaller amplitude of turbulence; see also Sec. 3.

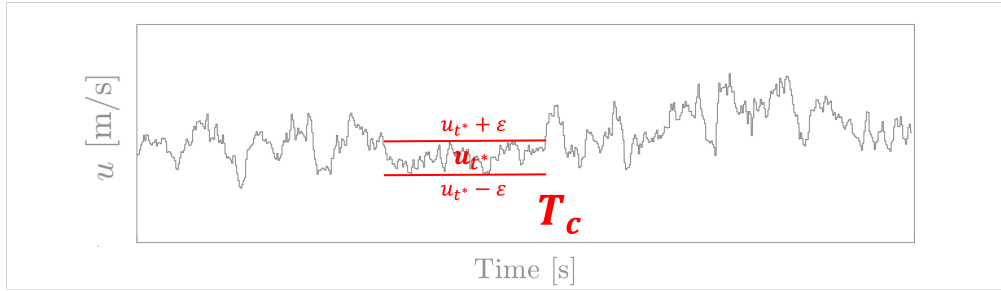


Figure 1. Schematic representation of a period of CWS T_c measured from an exemplary wind speed time series $u(t)$. The *constant speed interval* u_t " (horizontal red bars) specifies the limits for the accepted level of turbulence within a period T_c .

In the following, the method for measuring the length of a period T_c at a given time step t is described. Here we present a more rigorous formulation of the method, compared to the one provided in (Moreno et al., 2022). Essentially, the in detail. The goal is to count the number N of consecutive time steps, including t , for which their wind velocity $u(t)$ is contained inside the constant speed interval. For that, the reference speed $u_t = u(t)$ and the corresponding constant speed interval u_t " are defined. Next, the velocities at the time steps $t + i$ for $i = (1; 2; 3; \dots; 1)$ are evaluated and counted. The counter \tilde{N}^+ for the evaluation of $u(t + i) - u_{t+1} = u(t + i)$ is then defined as :

$$\tilde{N}^+ = \begin{cases} \tilde{N}^+ = +1 & \text{if } (u_t \text{ "}) \quad u_{t+1} \quad (u_t \text{ "}) \\ \tilde{N}^+ = ; \text{end} & \text{otherwise:} \end{cases} \quad (1)$$

Note that only consecutive points are counted in \tilde{N}^+ . The count is concluded once the value of $u(t + i)$ exceeds either the bottom or the top limits of the constant speed interval. So far, only points in the forward direction (+) from t are evaluated. The same algorithm is subsequently applied to counting the number of points \tilde{N} in the backward direction from t . In this case, values of $i = (1; 2; 3; \dots; 1)$ are considered for evaluating $u(t + i) - u_{t+1}$ in Eq. (1). Finally, the total number of consecutive points N measured at t results from the sum of \tilde{N}^+ and \tilde{N} , which are independently measured in their corresponding direction. The length of the period T_c at t is then obtained by multiplying the total N by the size of the time step t .

A period T_c is estimated for every time step in the time series $u(t)$. In the case of overlapping periods, only the longest-measured period is recorded. By doing so, a recounting of events is avoided.

145 In (Moreno et al., 2022), the threshold "for fixing the constant speed interval u_t " was randomly selected (e.g. 0.2 - 0.4 m/s).
~~Now, in order to, and the method described in Eq. (1) was applied over the actual measurements $u(t)$. However, limitations on~~
~~the method appear when analyzing large data sets with very different mean wind speed \bar{u} and standard deviation σ_u calculated~~
~~over shorter time windows (i.e. 10 minutes) with respect to the length of the sample. To~~ introduce a systematic approach, ~~in~~
~~this paper~~ " is defined to be proportional to the standard deviation of the wind speed σ_u . ~~Given a wind speed time series $u(t)$,~~
150 ~~the standard deviation σ_u measures the size of the fluctuations around the mean value \bar{u} .~~ Then, "for fixing the constant speed
~~interval u_t "~~ is calculated as,

$$" = A \sigma_u \quad (2)$$

where A is a factor, typically $A < 1$. The value of A can be chosen depending on the particular application. In the case of a
WT, A might be related to the thresholds for the control system to operate within different turbulent regimes. In practice, such
155 thresholds in the operating protocols are commonly defined as a function of the 10-min turbulence intensity $TI = \sigma_u / \bar{u}$. In
Eq. (2) and through this document, we refer to \bar{u} and σ_u as the values calculated over 10-minute periods unless a distinction is
clearly stated.

2.2 Atmospheric wind data

~~In (Moreno et al., 2022) data from two different onshore sites were investigated. The onshore wind is strongly influenced~~
160 ~~by orographic conditions. Therefore, it remained unclear to what extent the the periods T_c were originated by such external~~
~~conditions. To address this issue, we selected offshore data to be analyzed in this study~~ Data from the offshore research platform
FINO1 (FINO) are investigated. We expect ~~such data offshore wind~~ to provide a better representation of undisturbed, or less
disturbed conditions within the ABL compared to onshore data. Therefore, the possible effects of onshore orographic conditions
on the CWS structures are diminished.

165 The FINO1 platform is located in the North Sea. Records of the wind speed were taken by vertically aligned cup anemometers
mounted at different heights. The data correspond to ~~a continuous period of approximately five days (4×10^5 s), measured in~~
~~January 2006 measurements from January to December 2007~~ with a sampling frequency of 1Hz. Measurements at heights
 $H = [30, 40, 50, 60, 70, 80, 90]$ m above the mean sea level are considered. Wind speed records have been limited to those
between 3 and 25 m/s due to their relevance for WT operation. Values of $u(t)$ outside this range have been neglected. Moreover,
170 to avoid disturbances from the met mast, data for wind directions between 275 and 350° are not considered. As an overview
of the complete data set, Fig. 2 shows the mean \bar{u} and standard deviation σ_u calculated over individual 10-minute periods at
 $H = 90$ m.

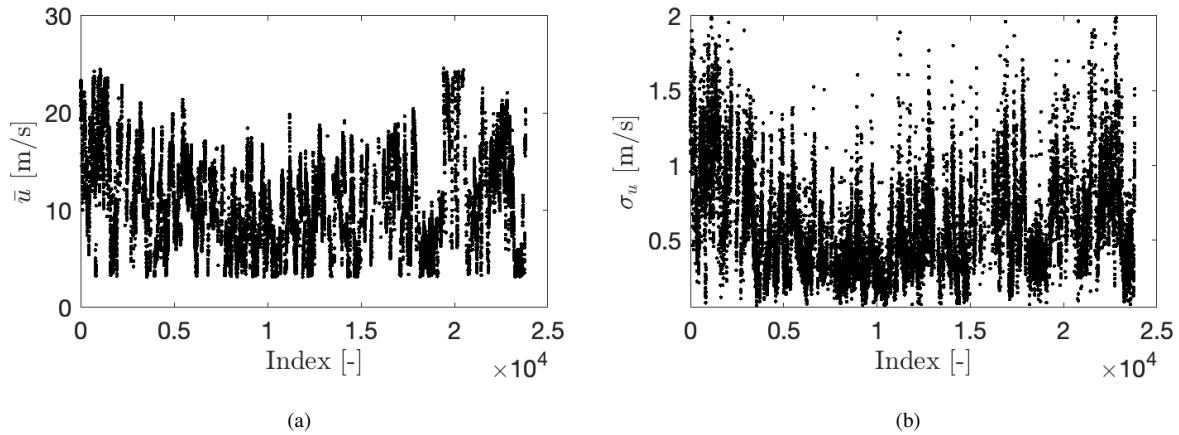


Figure 2. Wind velocity statistics of atmospheric FINO data at $H=90\text{m}$. (a) Mean wind speed \bar{u} . (b) Standard deviation σ_u . Each dot in the plots corresponds to a calculated value over a single 10-minute period. The dots are chronologically ordered.

Complementary, Table 1 summarizes the mean and standard deviation of $u(t)$ for all heights H . In the table and through the rest of the document, the angular brackets $\langle \cdot \rangle$ denote averaging over all the available 10-min periods. Then, $\langle \bar{u} \rangle$ and $\langle \sigma_u \rangle$ correspond to the average of \bar{u} and σ_u over the 666 at each H over all the 10-minute intervals. Accordingly, for $H=90\text{m}$, the values of $\langle \bar{u} \rangle$ vary from 9.7 to 10.0 m/s, and the standard deviations and $\langle \sigma_u \rangle$ are edged between 0.65 and 0.76 m/s the averages of the dots in Fig. 2(a) and (b) respectively.

$H[\text{m}]$	30	50	70	90
$\langle \bar{u} \rangle$ [m/s]	9.90	10.26	10.61	11.16
$\langle \sigma_u \rangle$ [m/s]	0.69	0.63	0.63	0.66

Table 1. Mean $\langle \bar{u} \rangle$ and standard deviation $\langle \sigma_u \rangle$ of the FINO data at different heights H . Angular brackets $\langle \cdot \rangle$ indicate averaging over the 666 subsets of 10 minutes in length all 10-min periods.

3 Statistics of T_C for atmospheric turbulent data

3.1 Mean, standard deviation and maximum value of T_C

180 As a starting point on the statistical characterization of the measured periods T_C , we discuss their mean duration ($\overline{T_C}$), standard deviation (σ_{T_C}) and maximum value ($T_{C,max}$). We define $T_{C,max}$ as a representative value from a set of the longest measured periods rather than the absolute and unique longest event. More details follow in Sec. 3.2. We compare the mentioned statistics of T_C at different heights H . A factor $A=0.3$ is exemplarily chosen for defining the threshold $\bar{u} = A \langle \bar{u} \rangle$ for the

constant speed interval U_t ". ~~With the definitions above, periods with less than 2% turbulence are selected.~~ The results are summarized in Table 2. ~~The values of "~~ are also provided.

H [m]	30	50	70	90
$\overline{T_c}$ [s]	3.6	3.6	3.7	3.6
τ_c [s]	3.0	3.2	3.3	3.3
$T_{c,max}$ [s]	106	147	151	123

Table 2. Mean ($\overline{T_c}$), standard deviation (τ_c), and maximum length ($T_{c,max}$) of the calculated periods T_c at different heights H . A factor $A=0.3$ is assumed for the estimation of T_c : ~~The values of "~~ are calculated by considering the value of the standard deviation \hat{h}/U_t at the corresponding H (see Table 1).

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As a remark, special attention has to be devoted to the meaning of the statistical moments $\overline{T_c}$ and τ_c calculated from the data. In certain cases, as those presented in (Moreno et al., 2022), the probability distribution $\rho(T_c)$ may lead to non-converging moments, e.g., mean and variance. Further details are discussed in Appendices B and C.

3.2 Probability density function of T_c

190 Next, in the statistical characterization of T_c , the probability density functions (PDFs) $\rho(T_c)$ are discussed. Fig. 3 shows $\rho(T_c)$ for the data shown in Table 2 for different H . As mentioned before, we focus our attention on characterizing very long periods ~~T_c as potential sources of special responses of the WTs.~~ Therefore we concentrate on the tails of $\rho(T_c)$. For comparability, the values of T_c are normalized by the longest measured period at each H ; more precisely, we use a representative value $T_{c,max}$ of at least five-ten of the longest periods to become statistically more robust. The obtained values for $T_{c,max}$ are those summarized
195 in Table 2.

The normalized PDFs $\rho(T_c)$ in Fig. 3 are presented in a log-log scale. In such a representation, a straight line reveals a power law behavior of the form $\rho(T_c) \propto T_c^{-\alpha}$ with α as the characteristic exponent. In the figure, such power laws are depicted by solid lines with the same color used for the dots at each H . We emphasize that the power laws extend over more than one decade. The corresponding exponents are calculated following the procedure proposed by (Clauset et al., 2009) and described in Appendix D. The values of α are given in the legends of the figure. Since the variation of the exponent α for all H is enclosed within 6%, then we conclude that the decay $\rho(T_c) \propto T_c^{-\alpha}$ is height independent. Moreover, since $\alpha \approx 3$ for all H , ~~all the moments of the power-law distribution $\rho(T_c)$ are defined (see Eq. (C1)). Since this is the case for all values of α in Fig. ??, the moments $\overline{T_c}$ and τ_c converge. In this way, the~~ the second-order statistical moments of T_c converge and the results presented in Table 2 provide meaningful information about the characteristics of the periods T_c (see Appendices B and C), regardless of the length of the data. ~~Moreover, since the results for the measurements at all H are enclosed within 8% of the estimated power-law fitting $\rho(T_c) \propto T_c^{-\alpha}$, then we conclude that $\rho(T_c) \propto T_c^{-\alpha}$ is height independent. In addition, the power-law decay is proved to hold for different widths of the constant speed interval. They will be discussed in Sec. 3.3.~~
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The power law behavior observed in the distributions $\rho(T_c)$ for the offshore data shown in Fig. 3 agree with the obtained for the two onshore sites investigated in (Moreno et al., 2022). This indicates that the CWS structures T_c are not due to the specific orographic conditions, but rather represent general characteristics of the boundary layer. However, as the actual values of the statistics of CWS periods (i.e. \bar{T}_c , T_c , $T_{c,max}$,) vary significantly between data sets, they should be exclusively considered for each location.

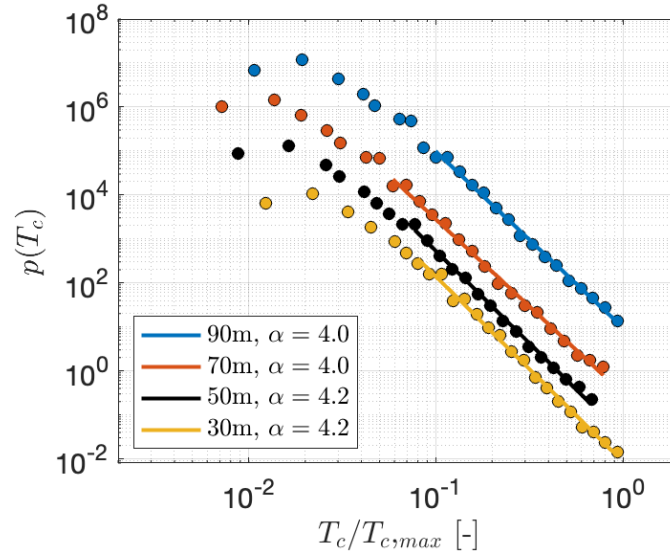


Figure 3. Normalized probability density functions $\rho(T_c=T_{c,max})$ for FINO data at different heights H . The dots illustrate the results from the FINO data. The solid lines show the power law decay fitting $\rho(T_c) \propto T_c^{-\alpha}$. The value $T_{c,max}$ for each height is defined as the bin centre containing at least five-ten of the largest measured periods after a binning process. The individual distributions are vertically shifted for better visualization.

3.3 Validity of the power law $\rho(T_c) \propto T_c^{-\alpha}$

To validate the universality of the power law distribution $\rho(T_c) \propto T_c^{-\alpha}$, we investigate the effect of the threshold θ by varying the factor A , as $\theta = A \cdot u$. The results of \bar{T}_c , T_c , $T_{c,max}$, and α , for values of $A=[0.2, 0.3, 0.5, 0.8]$ are summarized in Table 3. Respectively, Fig. 4 shows the normalized PDFs $\rho(T_c)$ in an analogue representation as shown previously in Fig. 3.

A [-]	0.2	0.3	0.5	0.8
$\overline{T_c}$ [s]	3.0	3.6	5.3	9.4
τ_c [s]	2.2	3.3	6.2	13.4
$T_{c,max}$ [s]	89	123	294	463
[s]	4.1	4.0	3.7	3.6

Table 3. Mean ($\overline{T_c}$), standard deviation (τ_c), maximum length ($T_{c,max}$), and exponent of the calculated periods T_c for different values of the factor A . FINO measurements at $H=90\text{m}$ are analyzed. The result of τ_c for $A=0.5$ is particularly discussed.

Fig. 4 shows a clear power law decay $\rho(T_c) \propto T_c^{-\alpha}$ for all values of A . Interesting to note, is that the exponent α decreases with increasing A . We conclude that the PDFs of CWS that $\rho(T_c)$ follow a Pareto-like distribution for large T_c (Laherrere and Sornette, 1998). Secondly, we now focus on the case $A=0.5$, for which results are marked by (*) in Table 3. As shown in Fig. ??, for this case, a characteristic exponent $\alpha = 3$ is obtained. Thus, the second moment of $\rho(T_c) \propto T_c^{-3}$ diverges or is not defined (see Eq. (C1)). In other words, the estimation of the mean of T_c leads to $\overline{T_c} = \infty$. As a consequence, the estimated value of τ_c for $A=0.5$ in Table 3 depends on the length of the time series $u(t)$. This is a prominent feature of distributions with power law tails for which arbitrarily large (with no upper bound) events are expected.

This feature of unbounded periods T_c is also indicated in Table 3. For $A < 0.5$ we see a nearly linear increase of $T_{c,max}$ by about 45s for $A + 0.1$. But for the increase of A from 0.4 to 0.5, the length of $T_{c,max}$ increases more than 200s. For longer time series this value would increase further.

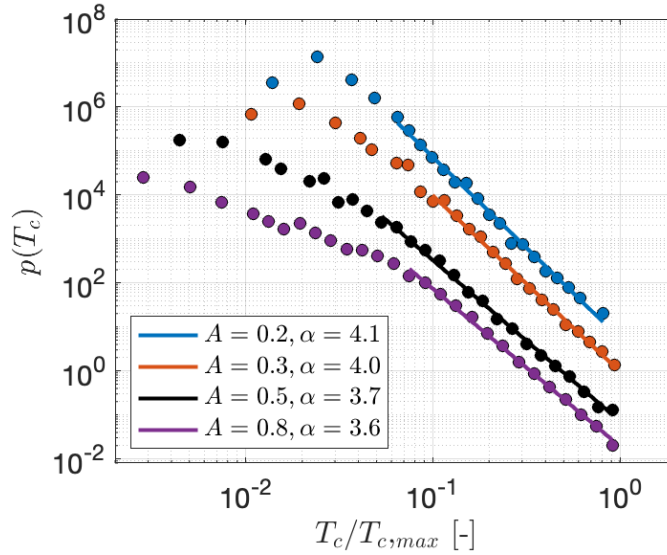


Figure 4. Normalized probability density functions $p(T_c=T_{c,max})$ for FINO data for different values of A . The power law fittings $\propto T_c^{-\alpha}$ are depicted by the solid lines. Measurements at $H=90\text{m}$ are considered. The value $T_{c,max}$ for each value of A is defined as the bin center containing at least ten of the largest measured periods after a binning process.

3.4 Power spectra of $u(t)$ during periods T_c

Further in the characterization of T_c , the spectral features of the wind speed $u(t)$ during the periods T_c address the question of whether the wind speed is strictly laminar, or rather turbulent with a low degree of turbulence. The turbulent nature of $u(t)$ filtered for periods $T_c > 10\text{s}$ is now verified by the power spectra, shown in Fig. 5. It is based on a selected time window of roughly five days. A decay of the form $E(f)/f^{-5=3}$ is obtained for all H . Accordingly, the wind data embedded along the periods T_c are not laminar flow sections but periods of turbulence with smaller amplitudes.

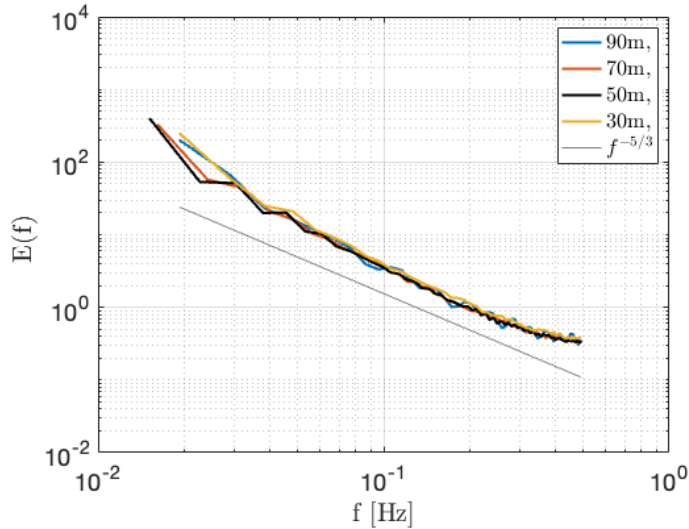


Figure 5. Power spectra $E(f)$ of wind speed $u(t)$ during the measured periods T_c at different heights H . The grey solid line shows a decay $E(f)/f^{-5/3}$. The spectra are calculated for each period T_c and then averaged over all periods within a selected time window of five days.

4 Comparison to pure turbulent and synthetic wind data

4.1 Experimental pure turbulence and Standard-IEC Kaimal

235 In order to investigate whether the CWS periods are typical features of turbulent flow or are special features of the ABL, we investigate the statistics of the periods T_c from experimental ideal turbulent data, as well as from numerical data. The experimental data, ‘Lab’, was measured by (Renner et al., 2001) in the central region of a free jet, which is approximately stationary, homogeneous, and isotropic. The numerical data, ‘Kaimal’, corresponds to IEC-standard wind data based on the well-known Kaimal model Kaimal et al. (1972) and generated by the NREL Turbsim package (Jonkman, 2016). Details about
240 the parameters and characteristics of the two additional data sets, ‘Lab’ and ‘Kaimal’, are given in Appendix E.

The analysis of the CWS periods from FINO and Kaimal could be easily compared as the wind data sets $u(t)$ have comparable IEC-standard characteristics in terms of mean wind speed, standard deviation, sampling frequency, and integral length scale. However, such a match of parameters to atmospheric data is not possible with the experimental Lab data. To work out the intrinsic features of the periods of CWS from these different data, we used ~~three~~two different approaches for normalizing the
245 calculated T_c .

Firstly, the normalization is done by $T_{c,max}$ analogous as in Fig. 3 and Fig. 4. Fig. 6 shows the resulting normalized PDFs $\rho(T_c)$ for the three wind data sets: (a) FINO, (b) Kaimal, and (c) Lab. The results in Fig. 6 clearly show different PDFs for the three data sets. The most prominent power law $\rho(T_c)/T_c$ is found for the FINO data, with a smaller exponent or more heavy-tailed probabilities. ~~FINO data exhibit a slope characterized by smaller values of the characteristic exponent~~

250 ($\alpha_{FINO} = 3.66$, $\alpha_{Kaimal} = 4.21$, $\alpha_{Lab} = 4.36$). As a result, only the FINO data show a tendency to non-convergence of their lower moments, leading to undefined mean or variance, as well as difficulties in the prediction of extremely large events T_c . For the Kaimal and Lab a power law can be put into question. We show nevertheless power laws as a reference for comparison between the three data sets. Interestingly, the range of periods T_c for which the power law holds for the FINO data extends over a decade, at least from $T_c = 0.1 T_{c,max}$ to $T_c = T_{c,max}$. In contrast, the power law range for Kaimal and Lab spreads only from $T_c = 0.3 T_{c,max}$ to $T_c = T_{c,max}$.

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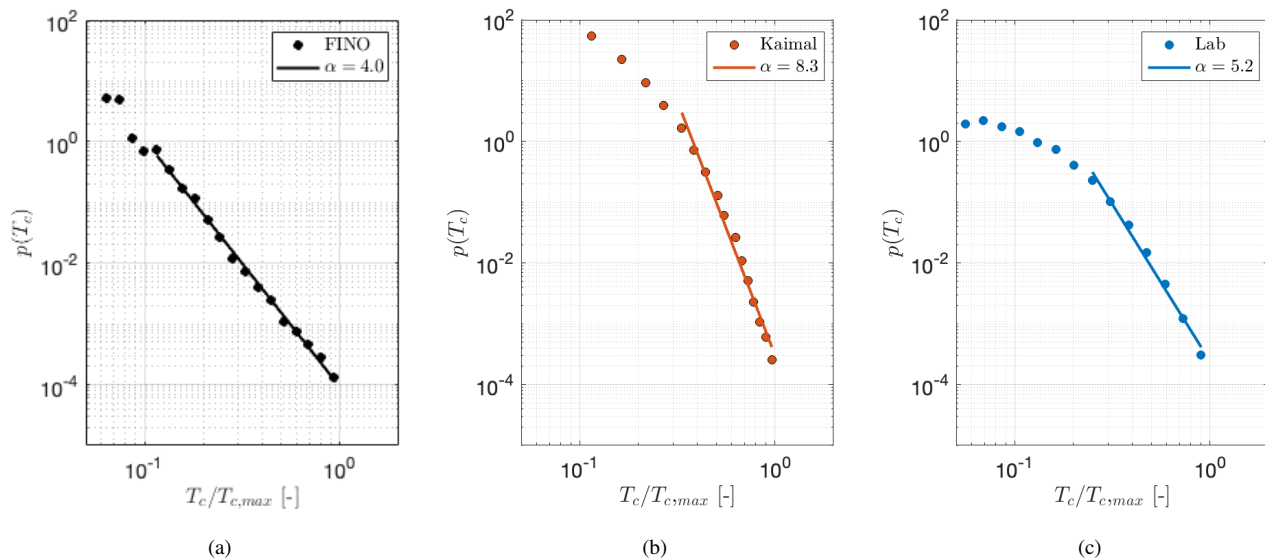


Figure 6. Normalized probability density functions $p(T_c = T_{c,max})$ for (a) FINO, (b) Kaimal and (c) Lab data sets. The power law fittings $p(T_c) \propto T_c^{-\alpha}$ are depicted by the solid lines. The value $T_{c,max}$ for each data set is defined after a binning process as the center of a bin containing at least ten of the largest measured periods. Measurements at $H=90\text{m}$ are considered for FINO. The constant speed interval Δu is calculated with $A = 0.3$. The values of Δu for Kaimal and Lab are 0.58 m/s and 0.38 m/s , respectively. In this particular case, as both data sets are expected to be steady, the standard deviation Δu is calculated over the length of the time series.

As a second way to compare the data, we normalize T_c with respect to the total length of the time series L . By doing so, we get information on the absolute duration of periods T_c within the duration of the sample. The normalization by $T_{c,max}$ shown in Fig. 7 does not provide any information regarding the magnitude of the periods T_c . Therefore, a comparison of absolute values of T_c between the three data sets remains inconclusive. Accordingly, we chose a third approach for normalizing the periods T_c so that their lengths are related to the intrinsic lengths of the flow. The integral length scale L_{int} is a measure of the longest correlations. For ideal turbulence, structures that are significantly larger than L_{int} are not to be expected. For meteorological wind data, the problem arises that at lower frequencies no white noise (i.e. zero correlation) is present so that larger structures than L_{int} are expected, see (Sim et al.; Larsén et al., 2016). Thus we use corresponding

260

PDFs $\rho(T_c)$ normalized by L_{int} , the so-called large eddy turnover time $T_{int} = L_{int}/U$ (Monin and Yaglom, 2007), where U is calculated over the length of the time series for Kaimal and Lab data. The results are shown in Fig. 7.

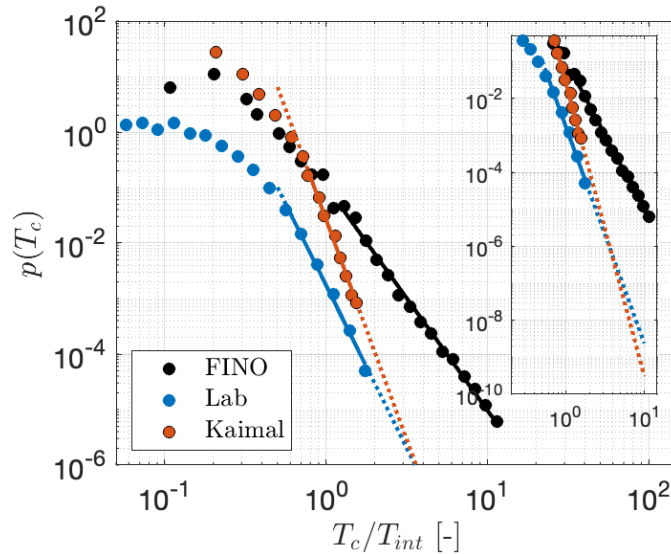


Figure 7. Normalized $\rho(T_c=T_{int})$ probability density functions for FINO, Kaimal and Lab data sets. (a) Normalized $\rho(T_c=L)$. L is the same for FINO and Kaimal $L=4 \times 10^5$ s, and for Lab data $L=1062$ s. (b) Normalized $\rho(T_c=L_{int})$. The values of T_{int} are, respectively, 10 s and 0.029 s for Kaimal and Lab (Fuchs et al., 2022). For FINO, T_{int} is considered to be 10 s as a representative value of the atmospheric data. The power law fittings $\rho(T_c)$ are depicted by the solid lines. The dotted lines show the power law fittings extended over a range of T_c larger than the range used for calculating the fitting parameters.

For the interpretation of Fig. 7 it is important to remark that the number of data points, given by the sampling rate and measured time, determines the lowest probability that can be resolved within the PDF. Accordingly, the minimum value of $\rho(T_c)$ for Kaimal data in Fig. 7 is explained by fewer data in the sample. Oppositely, the high probability $\rho(T_c)$ of shorter periods for Lab data is explained by a much higher sampling of the data. Taking this into account, Fig. 7 shows that the FINO data have significantly longer periods of CWS. It is observed in Fig. 7 that the maximal event of the data from the Kaimal model, $T_c \approx 2T_{int}$, is around 100 times more frequent for the FINO data than for the other two data sets. Assuming the extended power law tails for Kaimal and Lab depicted by the dotted lines, and better visualized in the zoomed plot, a period $T_c = 10T_{int}$ would be around 10^4 times less probable in the Kaimal model and Lab data compared to the measured FINO data. From the 1-year FINO data, we measured 15 events $T_c \approx 10T_{int}$ (with $\rho(T_c) = 5.7 \times 10^{-6}$). Roughly, it means an observation $T_c \approx 10T_{int}$ every 24 days. Under the Kaimal assumptions, this event will appear once every 24×10^4 days or 657 years.

Interestingly, in Fig. 7(b) we note that the three data sets exhibit periods T_c which surpass of the size of L_{int} , or $T_c = L_{int} > 1$. Such structures are large scale structures or may be considered as superstructures (Pandey et al., 2018; Krug et al., 2020). However, for Kaimal and Lab the largest events occur at $T_c \approx 2L_{int}$, while events of length up to $\approx 5L_{int}$ are observed

for Assuming the extended power law tails for Kaimal and Lab depicted by the dotted lines, and better visualized in the zoomed plot, a period $T_c = 10 T_{int}$ would be around 10^4 times less probable in the Kaimal model and Lab data compared to the measured FINO data. From the 1-year FINO data, we measured 15 events $T_c \sim 10 T_{int}$ (with $\rho(T_c) = 5.7 \times 10^{-6}$). Roughly, it means an observation $T_c \sim 10 T_{int}$ every 24 days. Under the Kaimal assumptions, this event will appear once every 24×10^4 days or 657 years.

Furthermore, we calculate the standard deviation of the periods T_c in units of integral lengths L_{int} . The resulting values are $T_{c;Lab} = 0.12 L_{int}$, $T_{c;Kaimal} = 0.15 L_{int}$, and $T_{c;FINO} = 0.47 L_{int}$. $T_{c;FINO} = 0.31 L_{int}$. The estimated values of T_c show in another way that FINO data have the tendency of remarkably longer periods, compared to Kaimal and Lab.

4.2 CTRW wind model

We have shown conclusive results on the distributions $\rho(T_c)$ in the ABL and their underestimation by a standard wind model. Finally, we show how the observed features of the FINO data can be included in a numeric wind field model. As a surrogate for the standard Kaimal model, we investigate non-standard wind velocity time series generated by the Continuous Time Random Walk (CTRW) model (Kleinhans, 2008; Ehrich, 2022; Schwarz et al., 2019; Mücke et al., 2011). The CTRW model generates either Gaussian ‘CTRW-G’ (-G as an abbreviation of Gaussian) or non-Gaussian (-NG as for non-Gaussian wind velocity time series. For the ‘CTRW-G’, the statistics of $u(t)$ are entirely Gaussian. On the contrary, the statistics of $u(t)$ for the ‘CTRW-NG’ deviate from Gaussianity towards distributions with so-called heavy tails or higher probabilities of extreme events.

The CTRW model uses a skewed Levy-distributed stochastic process, parameterized by the characteristic exponent α , as outlined in more detail in Appendix F and Appendix E. The stochastic process defines a time transformation from the intrinsic scale of the model s to the physical time t . Such time-scaling transformation allows the generation of non-Gaussian time series $u(t)$. The characteristic exponent α , with $0 < \alpha < 1$, specifies the asymptotic behaviour of the skewed Levy distribution. For $\alpha=1$ the resulting process $u(t)$ is entirely Gaussian. Values of $\alpha \neq 1$ generate processes with more pronounced non-Gaussian characteristics. In this case, non-Gaussianity is related to extremely long waiting times between two successive time steps s . A very long waiting time in $u(s)$ would then be translated into a period over which the process $u(t)$ remains constant.

Fig. 8 shows an excerpt of $u(t)$ for a Gaussian CTRW-G and a non-Gaussian CTRW-NG realizations. Respectively, values of $\alpha=1$ and $\alpha=0.9$ are considered. Along the interval between $t=875s$ and $t=895s$, a period of almost constant wind speed is observed for the CTRW-NG. For better visualization, a zoomed version of the time series is presented in the sub-figure in the right-bottom corner. Such a structure of the wind, indicated by the horizontal blue line, agrees with our definition of T_c . The observed small fluctuations within the period result from the interpolation process between the intrinsic and the physical times $s \rightarrow t$ (Ehrich, 2022).

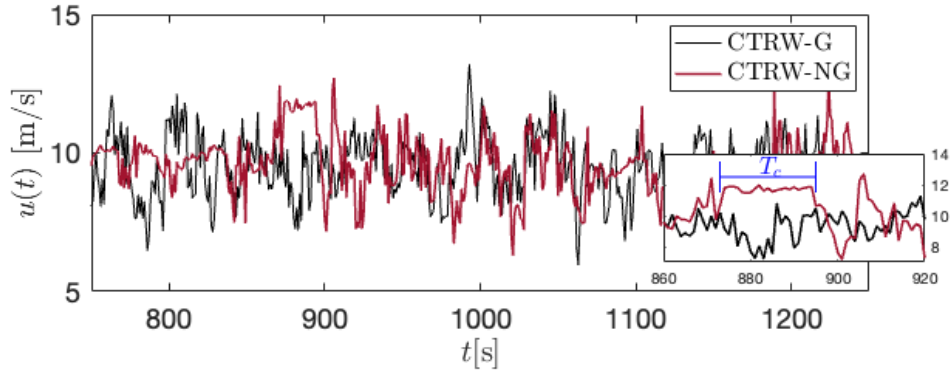


Figure 8. 750-s excerpt of the wind speed time series $u(t)$ for CTRW-G and CTRW-NG. A visible period T_c is visible between 875-895s for the CTRW-NG.

The fundamentals of the CTRW model as well as further details on the method for achieving such non-Gaussian features are given in Appendix F. The parameters for generating the time series are provided in Appendix E.

310 Fig. 9(a) shows the PDFs $\rho(T_c)$ for the CTRW realizations, and the FINO data. ~~For FINO, measurements at $H=90\text{m}$ are considered. The constant speed interval is fixed with a factor $A=0.3$.~~ The individual distributions are vertically shifted for better visualization. The dotted lines show the Gaussian distributions with the mean and standard deviation of the corresponding $\rho(T_c)$. The grey-shaded area illustrates the range of the decays of $\rho(T_c)$ or slopes α , enclosed by CTRW-G ($\alpha=1$) and CTRW-NG ($\alpha=0.9$). The distribution of the CTRW-NG realization shows an overestimation, compared
 315 to the FINO data, of the deviation from Gaussianity towards a higher probability of very long-duration periods T_c . This deviation is visible from $T_c = 0.3T_{c,max}$. On the contrary, the decay of the CTRW-G is much more pronounced and the divergence from the Gaussian distribution is visible only for events higher than $0.706T_{c,max}$. A third realization, 'CTR-NG' with $\alpha=0.99$ is included. The resulting $\rho(T_c)$ distribution for CTRW-NG* ($\alpha=0.995$) shows a better agreement with the
 320 the Gaussian CTRW-G and extremely non-Gaussian CTRW-NG.

Fig. 9(b) shows the resulting exponents α from the decay $\rho(T_c) / T_c^{-\alpha}$, against the exponent α from the Levy distribution of the CTRW model. The dotted horizontal line depicts the value of α for FINO. We conclude, that by tuning the α parameter of the CTRW model, non-Gaussian realizations of $u(t)$ can reproduce the statistics of $\rho(T_c)$ from the atmospheric turbulent wind.

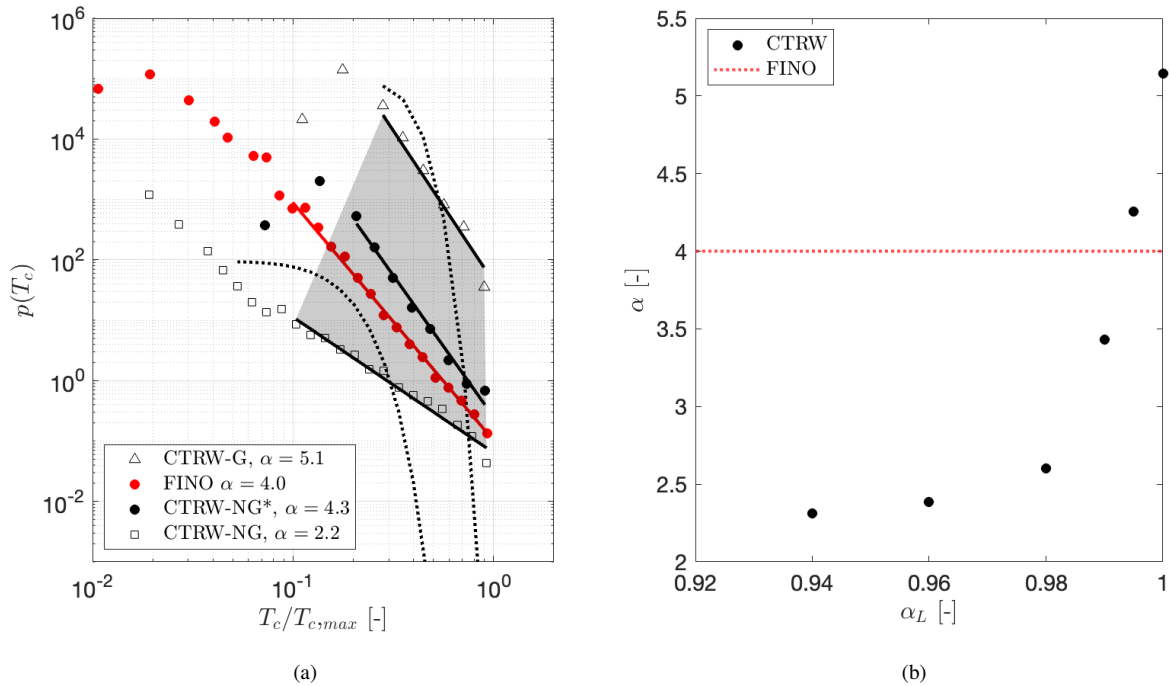


Figure 9. (a) Normalized probability density functions $\rho(T_c=T_{c,max})$ for the CTRW-G, CTRW-NG, CTRW-NG*, and the FINO data. The individual distributions are shifted vertically for better visualization. Dotted lines depict Gaussian distributions. The grey area depicts the range of the slopes covered between CTRW-G and CTRW-NG. Measurements at $H=90\text{m}$ are considered for FINO with $u_i=0.65\text{m/s}$. (b) Power law exponents α from $\rho(T_c) / T_c$ as a function of the characteristic exponent α_L from the Levy distribution driving of the CTRW model. The horizontal red line depicts the value of α for FINO data shown in (a).

325 5 Conclusions and Outlook

The method introduced in (Moreno et al., 2022) was used to measure the constant wind speed periods. We present measurements of the periods of CWS (T_c) (periods with turbulence of a reduced amplitude) from offshore wind data within the ABL. In agreement with (Moreno et al., 2022), we showed It is shown that the probability distributions $\rho(T_c)$ for offshore data exhibit a power law decay $\rho(T_c) / T_c$ for very long events. Given that offshore conditions maintain a more unperturbed ABL, we demonstrated that the periods T_c are intrinsic features of the ABL and are not due to specific external agents (i.e. mountains, obstacles) (i.e. hundreds of seconds). This agrees with (Moreno et al., 2022), where preliminary results from onshore cases were reported. However, significant differences in the values of the critical exponent presented in (Moreno et al., 2022) between offshore and onshore conditions suggest that the lengths of T_c are indeed influenced by interactions with the surroundings. Therefore, the estimated statistics of T_c must be considered locally for the specific location of interest. Given that offshore conditions maintain a more unperturbed ABL compared to onshore, we demonstrated that the periods T_c are intrinsic

features of the ABL rather than resulting structures originated by specific external factors (i.e. mountains, obstacles). Moreover, the exponent α seems to be quite independent of the height but changes significantly with the threshold u . Less pronounced decays of $\rho(T_c)$ are obtained with wider thresholds for considering the wind speed as constant. We found examples of T_c significantly larger than 100s, which correspond to spatially extended structures over sizes larger than 1km, using Taylor's hypothesis of frozen turbulence. Such large structures in a turbulent wind may be related to the so-called and currently very discussed "turbulent superstructures" (Pandey et al., 2018; Krug et al., 2020; Käufer et al., 2023).

~~We~~ Based on the spectral properties, we proved the turbulent nature of the wind speed $u(t)$ during the periods T_c . This relates our results to the case of the turbulent-turbulent interfaces (Kankanwadi and Buxton, 2022). However, the statistics of T_c are significantly different when comparing different turbulent data. Results from experimental homogeneous isotropic turbulence data suggest that the nature of the periods T_c is attributed to special structures developing in the wind inside the ABL. It is still an open question whether they are caused by special effects of the small-scale turbulence such as turbulence with or without shear or whether they are indeed consequences of larger-scale interactions of the atmospheric boundary layer, ~~like effects of such as phenomena related to~~ the spectral gap (Larsén et al., 2016).

The frequency of very events T_c in the ABL is significantly underestimated by the Gaussian assumptions in the IEC model. Therefore, the need for an improved wind model is justified. The Continuous Time Random Walk (CTRW) model with its characteristic time mapping (see Appendix F) is particularly suitable for the incorporation of the periods T_c measured from the atmospheric turbulent wind. This surrogate wind model represents an improvement ~~in wind modelling~~ towards more realistic atmospheric wind fields for numerical simulations. Consequently, responses of the WT interacting with such disregarded structures on the wind might be better predicted, ~~and critical loads due to these events might be avoided~~.

From an engineering perspective, very long periods of CWS might be undesirable for the operation of WTs if phenomena such as resonance or critical loading are induced. On the other hand, they also might be profitable/beneficial if conditions such as constant power production are achieved. ~~In fact, first calculations of the loads induced by periods T_c were investigated by BEM simulations of the 5MW NREL wind turbine (Jonkman et al., 2009). The results suggest that depending on the operational conditions of the WT, certain loads are damped over the period T_c . However, few load sensors, such as the side-to-side bending moment at the base of the tower, are amplified. Therefore, the here-presented detailed statistical description of T_c can be useful for control practices. A control system may be adapted to the u value, as a threshold value when the control dynamics sets in. Our results indicate that such a threshold value would lead to fundamentally different T_c statistics, having predictable longest periods or not. On the other hand, some specific aeroelastic events on the WT might be ignored during load simulations for design and control procedures due to inaccurate modelling of such periods within the standard wind models. In special cases, wind field models with improved or extended capabilities to reproduce this feature observed on the atmospheric turbulent wind might become necessary for accurate simulation of the loads and dynamics of the WTs. Further research is needed on the detailed effects of CWS periods on loads by investigating specific WT models.~~

A very long period of CWS might have an increased impact on a WT depending on its spatial location in the plane of the rotor. The effect of such an event happening in the outer region of the rotor plane might be higher compared to the case when it reaches the turbine at the region near the hub. ~~Within the former scenario, larger moments might be induced on the main shaft or at the root of the blades. Indeed, from the same above-mentioned simulations on the 5MW turbine, the effect on the amplification of the side-to-side moment of the tower increased when considering periods T_c affecting exclusively one quadrant of the rotor plane. Accordingly, in terms of the characterization of such constant wind speeds, future~~ Accordingly, preliminary investigations (detailed in Appendix G) suggest that the periods of CWS show a tendency to be localized at different measurement heights, and therefore, may become of particular interest for turbines with larger diameters. Future work has to be devoted to evaluating the structures in the spatial domain. Spatial correlations of the periods T_c might be highly relevant for the dynamics of the WT. Afterwards assessing the relevance of the empirically observed power law behavior of periods of CWS on turbine loading. For that, the complete statistical parametrization of periods of CWS, in both time and spatial domains, should be assessed and improved for the synthetic wind field models such as the ~~existing here~~ proposed CTRW model (Kleinhans, 2008), the recently introduced Time-mapped Mann model (Yassin et al., 2023) which can generate long waiting times of $u(t)$ as in the CTRW model, or the Superstatistical model (Friedrich et al., 2021, 2022) that follows the K62 model of turbulence.

Code availability. The algorithm described through Sec. 2.1 for measuring the periods T_c was coded in MATLAB for the analysis of wind speed data. The code can be made available upon request.

Data availability. The FINO and Lab measurements, as well as the generated Kaimal and CTRW time series can be obtained upon request.

385 **Appendix A: Periods T_c vs persistence events**

In the Introduction (Sec. 1) we referred to the inter-arrival times of excursions and zero-crossings as two general turbulent characteristics within the context of persistence phenomena. Those inter-arrival times might wrongly be assumed as intrinsically related to our periods of CWS. As shown in Fig. G1, fundamental differences arise when comparing the three events within a turbulent signal. In the upper part of Fig. G1 a zero-mean and normalized-by-standard-deviation signal $(u(t) - \bar{u})/\sigma_u$ is plotted. The thresholds $\pm U$ are fixed for considering the excursions of the signal. The blue area depicts the range contained inside these thresholds. The individual times when excursions occur are depicted by blue crosses. Similarly, the times when the signal crosses the zero line are the zero-crossings and they are depicted by red crosses. The grey rectangles depict the measured CWS periods $T_c > 10\sigma_u$ inside grey rectangles. We assume $\sigma_u = 0.3$ for measuring T_c .

At the bottom part of Fig. G1 the length of the inter-arrival times between the events (excursions and zero-crossings) are plotted. Blue lines depict the times between successive excursions at U (those at $-U$ are not considered). Red lines show the

times between zero crossings, and black lines show the duration of T_c (equivalent to the grey areas marked on the signal). The inter-arrival times for the excursions and zero-crossings in the plot are filtered to be longer than 10s, as are the periods T_c .

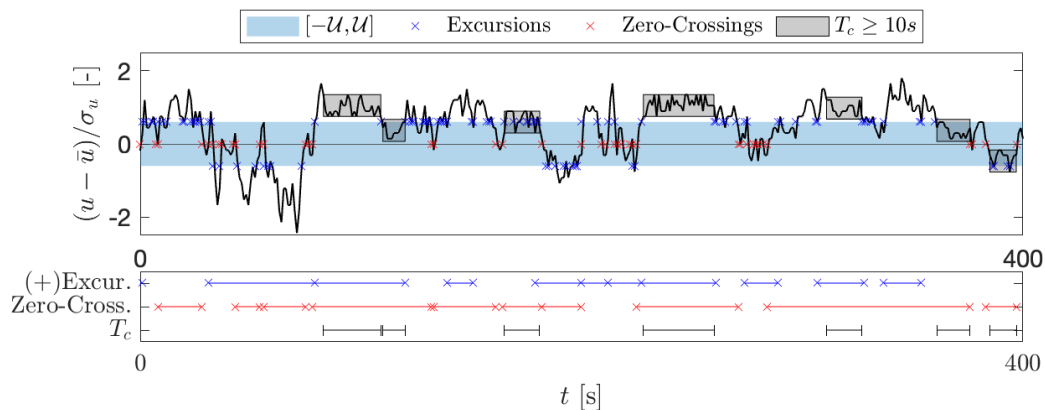


Figure A1. Illustration of excursions, zero-crossings and periods of CWS (T_c). On top, a normalized signal $(u(t) - \bar{u})/\sigma_u$. The blue crosses depict the excursions, considering U as thresholds. The red crosses correspond to the zero-crossings. The grey rectangles mark periods of CWS $T_c > 10s$. The blue and red lines in the bottom plot depict the resulting inter-arrival times for the excursion measured at $+U$, and the zero-crossings, respectively. For comparison, the periods $T_c > 10s$ are replotted as black lines.

As observed, there is no direct correlation between the occurrence or the length of the periods of CWS and the inter-arrival times; neither between excursions nor between zero-crossings. A period of CWS might enclose several inter-arrival times, as well as several periods of CWS might be embedded inside an interval between consecutive zero-crossings or excursions.

Appendix B: Power law distributions

A general quantity x with a probability distribution $\rho(x)$ follows a so-called *power law* if

$$\rho(x) = C x^{-\gamma} \quad (\text{B1})$$

with $\gamma > 1$ as for $x \geq x_{min}$ with the characteristic exponent γ and a constant $C = e^c$. The estimation of the minimum value x_{min} holds for the lowest limit of the power law. The exponent $\gamma > 1$, otherwise $\int_0^\infty x^\gamma \rho(x) dx$ does not converge. The estimation of γ from empirical data has been extensively discussed in the analysis of the distributions of a very wide range of applications (Newman, 2005; Clauset et al., 2009). Since Eq. (B1) is equivalent to $\ln \rho(x) = -\gamma \ln x + c$, the most simple approach for the calculation of γ comes from a linear regression on the log-log plot of the histogram of x . However, this procedure introduces significant errors due to the binning of the data and the resulting distributions. Such distributions are usually dominated by a few bins at lower values of x with very high values of $\rho(x)$, and several bins at the higher range of x with very low probabilities $\rho(x)$ (Newman, 2005; Dorval, 2008).

Instead of such a linear regression, a logarithmic binning process of the data is recommended. Within this approach, the histogram of x is constructed for k number of bins with variable width. More specifically, the bin edges B are proportional to successive powers of a constant a . Then,

$$415 \quad B = (b_1; b_2; \dots; b_{k+1}) = x_{c,min}(a^0; a^1; \dots; a^k) \quad (B2)$$

where $b_1 > 0$, $k > 1$ and x_{min} is the minimum value of x for considering the power law behaviour. Thus, the i_{th} bin encloses the interval $[b_i; b_{i+1})$ and the larger edge of the k_{th} is assumed to be $+1$.

The value of the lower bound x_{min} affects the estimation of the exponent in $p(x) \propto x^{-k}$. Analogously, for binned data, b_{min} is defined as the minimum bin taken into consideration for the calculation of k . We follow the algorithm proposed by
 420 (Clauset et al., 2009; Virkar and Clauset, 2014) for choosing b_{min} from binned empirical data. This method is based on a Kolmogorov-Smirnov (KS) statistic test (Massey, 1951) for minimizing the distance between the distributions of the fitted model $P(b_j; b_{min})$ and the empirical model $S(b)$ above b_{min} . Then, the optimized value of b_{min} minimizes

$$D = \max_b \left| \frac{S(b) - P(b; b_{min})}{j} \right| \quad (B3)$$

Further details about the method for calculating b_{min} and k are provided in Appendix D.

425 ~~A distribution with a power-law behaviour is known as critical and may lead to divergent moments. For a~~

Appendix C: Statistical moments of power laws

A power law distribution of a continuous variable x is defined in Eq. (B1), where $k > 1$ is the power law exponent, C is a normalization constant, and x_{min} is the minimum value at which the power law holds. Then, the k^{th} statistical moment of a power law distribution $p(x) = C x^{-k}$ is given by,

$$430 \quad \int_0^Z x^k p(x) dx = \int_{x_{min}}^Z x^k p(x) dx + \int_0^{x_{min}} x^k p(x) dx = \tilde{A} + \frac{C}{k+1} x^{-k+1} \Big|_{x_{min}}^Z \quad (C1)$$

Then, a quantity x with $p(x) \propto x^{-k}$, may have divergent moments. Extensively, its general k^{th} moment exists only if $k < k+1$. The mean value of $p(x)$, or $\int x^1 p(x) dx$, becomes infinite for $k < 2$. Furthermore, if $k < 3$, $p(x)$ has no finite variance, $\int x^2 p(x) dx$. In such a case, x can take values of $x \geq x_{min}$. Many phenomena, varying from biological to economical, are characterized by such so-called critical distributions. A few examples are the frequency of use of words, the income among individuals, and the magnitude
 435 of earthquakes (Newman, 2005; Marquet et al., 2005; Powers, 1998). ~~The latter represents a challenge to the forecasting of seismic events.~~

Appendix D: Estimation of b_{\min}

Here we describe the method for estimating the minimum b_{\min} , introduced in Appendix B, above which the power law $p(T_c) / T_c$ is valid. The method was proposed by Virkar and Clauset (2014).

440 For each possible $b_{\min} \in (b_1; b_2; \dots; b_{k=2})$,

1. Calculate the cumulative binned empirical distribution $S(b)$ for bins $b \in [b_{\min}, \dots]$.
2. Estimate the characteristic exponent α considering $b \in [b_{\min}, \dots]$.
3. Calculate the cumulative density function (CDF) $F(b; \alpha, b_{\min})$ of the binned power law.
4. Calculate the Kolmogorov-Smirnov(KS) test statistic D defined in Eq. (B3).

445 5. Select the optimal value b_{\min} as the value of b_{\min} with the minimum test statistic D .

The bins b are defined according to Eq. (B2). For the estimation of α (step 2.), a least-squares linear regression method is considered.

Appendix E: Further details of experimental and synthetic wind data

- Kaimal: The data set contains 4×10^5 data points with a frequency of 1Hz. The mean wind speed is 10m/s and the standard deviation is 0.58m/s. The integral length scale is set to 10m. The parameters are chosen to be comparable to the averaged values of FINO data (see Sec. 2.2).
- CTRW: Both realizations, 'CTRW-G' and 'CTRW-NG', have 4×10^5 data points with a frequency of 1Hz. The mean wind speed and standard deviation are 9.5m/s and 1.1m/s for both cases. Extended parameters for the model are $\beta_c = 1.8\text{Hz}$; $\beta_L = [0.9, 1]$, $\epsilon = 350$ and \dots . Details on the definition of the parameters are given in Appendix F and (Ehrich, 2022).
- Lab: The velocity in the direction of the flow was measured by a hot-wire anemometer. The data set consists of 8.48×10^6 points with a sampling frequency of 8kHz. The measured integral length scale is reported as 0.067m (Fuchs et al., 2022). Details of the experiment are found in (Renner et al., 2001).

Appendix F: CTRW model for the generation of wind fields

460 More detailed descriptions of the model are provided in (Kleinhans, 2008; Yassin et al., 2023; Mücke et al., 2011; Schwarz et al., 2019). Time series of the wind speed $v_i(t)$ at each point of a defined grid are based on two coupled Ornstein-Uhlenbeck (OU) stochastic processes $v_i(s)$ and $u_i(s)$. Both processes are first generated in an intrinsic scale. The super index i accounts for the three directions of the wind $\mathbf{v} = [(x); (y); (z)]$. In our case, we generate wind speed time series only

in the longitudinal direction $u^{(x)}$, so that $\mathbf{u} = (u)$. The two processes are defined as,

$$465 \quad \frac{du_r^{(x)}(s)}{ds} = -\gamma_r(u_r^{(x)}(s) - u_0^{(x)}) + \sqrt{D_r} \xi_r^{(x)}(s) \quad (F1)$$

and,

$$\frac{du_i^{(x)}(s)}{ds} = -(\gamma_i^{(x)}(s) - u_i^{(x)}(s)) + \sqrt{D_i^{(x)}(s)} \xi_i^{(x)}(s) \quad (F2)$$

where γ_r and γ_i are damping constants, and D_r and D_i are diffusion constants; $\xi_r(s)$ and $\xi_i(s)$ are Gaussian-distributed white noise. Next, the resulting Gaussian velocity signals $u_i^{(x)}(s)$ are mapped to the physical time scale by means of an additional
470 stochastic process as,

$$\frac{dt(s)}{ds} = \epsilon_{\gamma, L}(s) \quad (F3)$$

where $\epsilon_{\gamma, L}(s)$ is a Lévy-distributed process with characteristic exponent γ and a cutoff value L . In the case of $L=1$, the intrinsic scale s is equivalent to the physical time t so that $u_i^{(x)}(s) = u_i^{(x)}(t)$. The time mapping process described in Eq. (F3) allows the key feature of the model which accounts for the intermittent behaviour of the wind speed time series. The
475 intermittency is introduced by the Lévy-distributed sizes of the waiting times for the transformations from

In Sec. 4 we investigated two CTRW data sets: CTRW-G and CTRW-NG. For the CTRW-G time series shown in Fig. 8 and Fig. 9(a), the exponent $L=1$ so that the waiting times of the intrinsic scale are constant and the statistics $u_i^{(x)}(t)$ are Gaussian. For the CTRW-NG time series, we assumed $L=0.9$. By doing so, we introduce non-Gaussian features on the probability distributions. Further values of the parameters for generating the fields are given in Appendix E.

480 Appendix G: [Spatial coherence of \$T_c\$](#)

[The spatial coherence of the periods of CWS has been preliminary investigated. Fig. G1 shows the results of evaluating the simultaneity of events \$T_c > 30s\$, conditioned on \$H\$, occurring at different heights of the FINO data. Exemplary Fig. G1 shows the case when considering the reference height \$H=90m\$. For each event \$T_c > 30s\$ at \$H\$, the occurrence of simultaneous events \$T_c\$ at the remaining lower heights is evaluated. A black line is drawn when an event \$T_c\$ is measured at the corresponding \$H\$.](#)

Figure G1. Events $T_c > T_{min}$ at different heights conditioned on $H=90m$. First, the reference height H is defined. Next, for each event $T_{c,i} > T_{min}$ at $H=H$, the occurrence of T_c at the remaining heights $H=[70, 50, 30]m$ is evaluated. Black lines depict the occurrence of an event. Note that T_c at all heights are conditioned so that $T_c > T_{min}$. For the example in this figure, $T_{min}=30s$ and $H=90m$.

485 The results show that most of the events are not coherent over the four heights and confirm the appearance of localized structures. In fact, for the example shown, 37% of the events at 90m are happening simultaneously at 70m. This number decreases to 11% when comparing the periods of CWS between 90m and 30m. The same evaluation for coherent events has been performed for different values of T_{min} and reference heights H .

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