Comment on"Glauert's optimum rotor disk revisited – a calculus of variations solution and exact integrals for thrust and bending moment coefficients" by Tyagi and Schmitz (2025)

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The paper by Tyagi and Schmitz (2025a) presents a reformulation of the classical momentum theory optimum rotor problem using the calculus of variations and closed-form integrations for thrust and bending moment coefficients. This comment examines these derivations within the physical and mathematical limits of the one-dimensional momentum model.

Several of the mathematical developments consist of algebraic manipulations of Glauert's induction relations. These include polynomial expansions, rational simplifications, and repeated applications of L'Hôpital's rule. These manipulations change the algebraic form of the standard relations but do not modify the structure of the underlying momentum equations.

The paper begins by examining the behavior of the model equations in the limit $\lambda \to \infty$ and evaluates the resulting expressions for C_P and C_{Be} under that limiting assumption. In this limit, the Glauert relations give $a' \to 0$. Because torque is proportional to a', the torque also approaches zero. The mechanical power coefficient C_P is proportional to torque multiplied by the rotational speed, so C_P approaches zero when a' approaches zero within the axial plus swirl momentum model. Any expression predicting nonzero power in this limit is inconsistent with the angular momentum balance on which the model is based. This inconsistency arises from evaluating the model outside the conditions for which its assumptions are valid, rather than from the algebraic manipulations themselves.

The paper next derives limiting expressions for C_P, C_T, and C_{Be} in the limit $\lambda \to 0$ by repeated differentiation of the numerator and denominator terms. These limits follow from the mathematical continuation of the steady one-dimensional momentum equations. When λ is small, the flow around the rotor is typically separated, unsteady, and non-axisymmetric, and the assumptions of the actuator disk model, namely steady one-dimensional uniform flow with a constant pressure jump, are not satisfied. The limiting values obtained from the continued equations, therefore, describe the algebraic behavior of the continued model but do not represent the behavior of a rotor operating under such conditions.

The calculus of variations derivation in the paper reproduces Glauert's optimum loading condition. The resulting third-order relation is identical to that obtained by extremizing the power coefficient subject to the one-dimensional momentum constraints. This equivalence follows directly from the structure of the classical actuator disk formulation. Because this formulation assumes an infinite number of blades, no tip losses, no drag, and steady uniform inflow, the resulting expressions apply only within those idealized assumptions.

The numerical constants appearing in several equations, such as 2.5457 and -13.3272 in Eqs. 35, 48, and 50 arise from evaluating the closed-form antiderivatives at the lower limit $x = 1-3a$ with $a = 1/4$. Substituting $x = 1/4$ into the polynomial and logarithmic terms yields the reported constants. Providing intermediate symbolic steps would have allowed readers to reproduce these values directly.

Several sections of the paper contain symbolic patterns, such as multi-step rational simplifications, repeated differential reductions, and large composite expressions. These patterns match those typically produced by language model-based symbolic tools. The paper does not indicate whether such tools were used. Clarification of any computational or automated methods would assist readers in reproducing the intermediate steps and verifying the closed-form expressions. This statement concerns only the form of the expressions, not the authors' methods or intent.

The high and low λ regimes considered in the paper correspond to conditions where at least one assumption of the one-dimensional momentum model does not hold. At high λ, the swirl component of the momentum model gives zero torque, so the model predicts zero power. At low λ, the flow is unsteady and separated and does not satisfy the assumptions of a uniform steady actuator disk. In these regimes, expressions obtained from algebraic continuation of the model equations should be interpreted strictly as mathematical consequences of the continued equations and not as predictions of rotor performance under physical conditions outside the validity of the model.

There is substantial overlap between the derivations, polynomial expressions, and integration procedures in this paper and those in a previously published and publicly accessible conference paper by the same authors (Tyagi and Schmitz, 2025b). The earlier paper contains many of the same mathematical developments. Citing this prior work would clarify the relationship between the two publications and help readers follow the development of the results.

References

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