

Under-resolved gradients: slow wake recovery and ~~fast~~ low turbulence ~~decay with~~ behind wind farms parameterized in mesoscale ~~Wind Farm Parameterizations~~ simulations

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1 **Abstract.** Numerical Weather Prediction (NWP) and climate models equipped with Wind Farm Parameterizations (WFPs) can
2 simulate cluster wake effects affecting downstream wind farms in both onshore and offshore environments. This study evaluates
3 the ~~strengths and limitations of~~ wake recovery behind a wind farm represented by the NWP-WFP approach ~~using in~~ the Weather
4 Research and Forecasting (WRF) model ~~with the Fitch WFP, using either the Fitch et al. (2012) or Ma et al. (2022b, a) WFPs.~~
5 Results are benchmarked against large-eddy simulations (LES) of an idealized offshore wind farm with aligned and staggered
6 layouts under neutral atmospheric stability. ~~Wake~~ The near-farm wake recovery is underestimated in NWP-WFP simulations
7 because of two interconnected issues. First, the spatial gradients in the wind velocity field within the near-farm wake are
8 necessarily under-resolved at mesoscale grid resolutions compared to the LES. Second, the ~~faster decay of farm-added low~~
9 turbulence kinetic energy (TKE) in the near-farm wake in the mesoscale simulations is ~~likely~~ not due to excessive dissipation,
10 but rather ~~due to the underestimation of spatial gradients needed to sustain elevated TKE levels via shear production. A key~~
11 ~~insight is that the slow recovery to insufficient shear production of TKE caused by these under-resolved gradients. As a result, a~~
12 wind speed bias of approximately $0.15\text{--}0.60\text{ m s}^{-1}$ develops in the near-farm wake, ~~although depending on the simulation setup~~
13 and wind-farm layout. Although this behavior is confined to a short downstream distance, it has lasting consequences for the
14 far wake region. ~~This fact underscores the~~ Furthermore, the slow near-farm wake recovery is not caused by a limitation of the
15 WFP itself, but by the representation of inherently fine-scale processes on a coarse mesoscale grid. These results underscore the
16 need to address under-resolved spatial gradients to improve wake recovery and reduce ~~far wake far wake~~ biases in NWP-WFP
17 simulations.

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26 1 Introduction

27 The sheer scale of offshore wind farms is attracting increasing attention from the scientific community (Barthelmie et al.,
28 2007, 2009; Platis et al., 2018; Pryor et al., 2020; Cañadillas et al., 2020; Rosencrans et al., 2024; Ouro et al., 2025) largely
29 due to cluster wake effects and associated power losses. The combination of massive wind farms (~ 1 GW), large turbines
30 (10–20+ MW), and the relatively low turbulence offshore (Bodini et al., 2019) leads to strong, persistent wakes that can extend
31 tens of kilometers downstream of the wind farms (Platis et al., 2018). As a result, inter-farm wake effects pose challenges not
32 only to operating wind farms but also to those in planning or development stages, thus mirroring concerns already observed in
33 onshore settings (Lundquist et al., 2019). Understanding and accurately predicting the wakes that arise from atmosphere–wind
34 farm interactions is therefore of scientific and economic relevance (Veers et al., 2019, 2022). In this context, Numerical Weather
35 Prediction (NWP) models equipped with Wind Farm Parameterizations (WFPs) are proving to be a valuable tool (Fischereit
36 et al., 2022a).

37 The representation of wind farms in NWP and climate models has evolved significantly over the past two decades, mov-
38 ing from surface-based approximations to more physically realistic parameterizations. In the early 2000s, wind farms were
39 incorporated into NWP and climate models through enhanced surface roughness (z_0) or drag (Ivanova and Nadyozhina, 2000;
40 Malyshev et al., 2003; Keith et al., 2004; Wang and Prinn, 2010). However, this approach led to exaggerated surface fluxes, tur-
41 bulence kinetic energy (TKE), and wind speed deficits (Fitch et al., 2013b). A key conceptual shift came with Baidya Roy et al.
42 (2004), who proposed that wind farms act as an elevated momentum sink and TKE source within the rotor layer rather than at
43 the surface. The elevated momentum sink and TKE source framework remains the conceptual foundation for most WFPs in use
44 today, and for several subsequent advances (Fitch et al., 2012; Adams and Keith, 2013; Boettcher et al., 2015; Abkar and Porté-Agel, 2015;
45 Fitch et al., 2012; Adams and Keith, 2013; Boettcher et al., 2015; Abkar and Porté-Agel, 2015; Volker et al., 2015; Pan and Archer, 2018;
46 . For a comprehensive overview of WFP developments, see the review by Fischereit et al. (2022a).

47 One of the key advances in WFPs was the modification of the TKE source term, initially treated as a constant (Baidya
48 Roy et al., 2004). Blahak et al. (2010) proposed linking the added TKE to the energy extracted by the turbines via the power
49 coefficient (C_P), and Fitch et al. (2012) introduced the formulation $C_{\text{TKE}} = C_T - C_P$, where C_T is the thrust coefficient.
50 Later, Archer et al. (2020) suggested scaling C_{TKE} with a TKE factor (α) of 0.25 to avoid exaggerated TKE values. Even
51 though some studies find better performance using $\alpha = 1.00$ instead (Larsén and Fischereit, 2021), the impact of changing α
52 varies spatially (Rosencrans et al., 2024; Ali et al., 2023; García-Santiago et al., 2024). Most recently, large-eddy simulation
53 (LES)-based formulations have been proposed to further improve the TKE source term (Khanjari et al., 2025).

54 Regarding the WFPs and the representation of atmosphere–wind farm interactions, it is useful to distinguish between grid-
55 unresolved and grid-resolved processes. Unresolved processes include the momentum sink term, intra-grid-cell interactions be-

tween turbines (~~Abkar and Porté-Agel, 2015; Pan and Archer, 2018; ?~~)([Abkar and Porté-Agel, 2015; Pan and Archer, 2018; Ma et al., 202](#)
, local wake expansion (Volker et al., 2015), and wake recovery occurring within the same grid cell. The momentum sink term
creates a wind speed deficit (wake) as a grid-unresolved process. However, momentum recovery into the generated wake
is a spatial process that occurs over several grid cells and depends on spatial gradients of wind speed, direction and TKE,
[TKE, in addition to planetary boundary layer \(PBL\) schemes](#). Wake recovery is therefore [also](#) a grid-resolved process. This
grid-resolved wake recovery depends on multiple factors. Several studies have shown sensitivity to horizontal grid resolution
(Mangara et al., 2019; Siedersleben et al., 2020; Tomaszewski and Lundquist, 2020; Peña et al., 2022; Sanchez Gomez et al.,
2024) and vertical resolution (Vanderwende et al., 2016; Mangara et al., 2019; Tomaszewski and Lundquist, 2020; Siedersleben
et al., 2020). The ~~planetary boundary layer (PBL)~~ [PBL](#) scheme is also influential (Rybchuk et al., 2022; Agarwal et al., 2025),
as is the tuning of the TKE addition factor α (Archer et al., 2020; Siedersleben et al., 2020; Tomaszewski and Lundquist, 2020;
Larsén and Fischereit, 2021; Sanchez Gomez et al., 2024). In addition, atmospheric stability plays a key role in modulating
wake recovery and has been highlighted in several recent works (Vanderwende et al., 2016; Lundquist et al., 2019; Rosencrans
et al., 2024; García-Santiago et al., 2024; Quint et al., 2025). Performance also varies between different WFPs. For instance,
the Explicit Wake Parameterization (EWP) generally produces shorter wakes than the Fitch scheme (Shepherd et al., 2020;
Pryor et al., 2020; Larsén and Fischereit, 2021; Fischereit et al., 2022b; García-Santiago et al., 2024; Pryor and Barthelmie,
2024).

The underestimation of wake recovery in NWP-WFP simulations is related to grid-resolved processes. A conceptual descrip-
tion of the generation and recovery of the wake in NWP-WFP, in comparison with LES, is provided in Fig. 1. Two downstream
cells are used because the added TKE in the LES usually reaches its maximum in the first downstream cell (Fig. 1e), whereas
the added TKE maximum occurs at the turbine grid cell for the NWP-WFP (Fig. 1d). Thus, wake recovery and TKE ~~decay~~
[decrease](#) are assessed here as streamwise changes between two consecutive downstream cells (Figs. 1b and c; e and f). The
NWP-WFP $\Delta W S$ barely changes between panels (Figs. 1b and c), whereas the LES displays recovery. On the other hand, the
 ΔTKE ~~decays~~ [decreases](#) too fast for the NWP-WFP compared with the LES between panels (Figs. 1e and f). Because the
slow wake recovery and the ~~fast TKE decay~~ [abrupt TKE decrease](#) in the NWP-WFP occur ~~over~~ [in](#) downstream cells without
turbines, they ~~are not~~ [may not be](#) caused by the WFP.

Multiple NWP-WFP studies report good agreement of the wind speed deficit with LES within turbine or farm grid cells
(Abkar and Porté-Agel, 2015; Vanderwende et al., 2016; Peña et al., 2022; García-Santiago et al., 2024), suggesting that the
momentum sink term (i.e., the grid-unresolved component) creates a wind speed deficit consistent with the LES (Fig. 1a).
However, after the generation of the wind speed deficit, the downstream wind speed profiles often remain unchanged in the
NWP compared to the LES (Figs. 1b and c). This discrepancy in wake recovery between NWP-WFP and LES persists across
neutral, convective, and stable atmospheric stability regimes (García-Santiago et al., 2024). Ultimately, this slow recovery in
NWP-WFP simulations likely contributes to the overestimation of power losses often reported when using WFPs (Lee and
Lundquist, 2017; Montavon et al., 2024). [In Montavon et al. \(2024\), additional factors affecting turbine power estimates are](#)
[identified, including the absence of a turbine induction correction in the standard Fitch WFP, which was subsequently addressed](#)

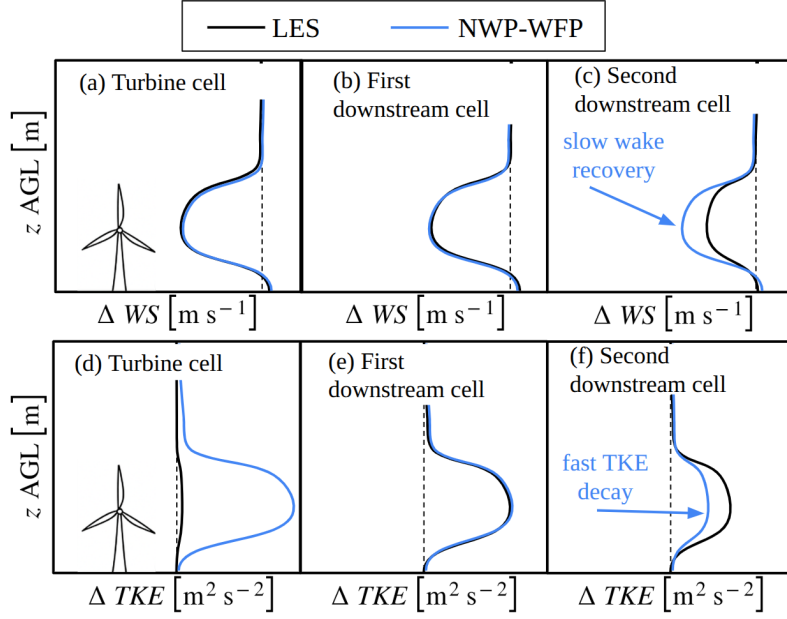


Figure 1. Conceptual description of wind turbine wake generation and recovery in a NWP-WFP simulation provided as a summary of the literature (Abkar and Porté-Agel, 2015; Vanderwende et al., 2016; Peña et al., 2022; García-Santiago et al., 2024). Time-averaged vertical profiles of wind speed deficit (ΔWS , a-c) and turbine-added TKE (ΔTKE , d-f) within the turbine grid cell (a, d), for the first (b, e) and second (c, f) downstream cells in the NWP without turbines. The wind speed deficit is defined as the difference between simulations with and without turbines ($\Delta WS = WS_T - WS_{NT}$), respectively, yielding negative values in most of the wake. The turbine-added TKE ($\Delta TKE = TKE_T - TKE_{NT}$) is similarly defined but typically yields positive values.

by Vollmer et al. (2024). Thus, the evidence of a well-functioning momentum sink term combined with the insufficient wake recovery downstream of turbine grid cells suggests the problem lies in the grid-resolved wake recovery process.

Conceptual description of wind turbine wake generation and recovery in a NWP-WFP simulation provided as a summary of the literature (Abkar and Porté-Agel, 2015; Vanderwende et al., 2016; Peña et al., 2022; García-Santiago et al., 2024). Time-averaged vertical profiles of wind speed deficit (ΔWS , a-c) and turbine-added TKE (ΔTKE , d-f) within the turbine grid cell (a, d), for the first (b, e) and second (c, f) downstream cells in the NWP without turbines. The wind speed deficit is defined as the difference between simulations with and without turbines ($\Delta WS = WS_T - WS_{NT}$), respectively, yielding negative values in most of the wake. The turbine-added TKE ($\Delta TKE = TKE_T - TKE_{NT}$) is similarly defined but typically yields positive values. However, several studies using NWP-WFP simulations driven by realistic synoptic conditions have reported reasonable agreement between simulated and observed wind speed deficits in wind farm wakes. Such agreement has been demonstrated using aircraft measurements (Siedersleben et al., 2018a, b, 2020; Larsén and Fischereit, 2021; Ali et al., 2023; van Stratum et al., 2022) as well as SCADA data (Sanchez Gomez et al., 2024) in offshore wind farms. The contrast between idealized NWP-WFP simulations evaluated against LES, which can exhibit slower wake recovery, and realistic NWP-WFP simulations validated

103 against observations motivates further investigation. It remains unclear whether the slower wake recovery in idealized configurations
104 arises from limitations of the WFP itself or from deficiencies in the representation of wake recovery on a mesoscale grid.
105 Clarifying this distinction is essential for assessing when NWP-WFP simulations can reliably represent wake evolution and
106 associated power losses, and constitutes the central motivation of this study.

107 Another issue, less frequently discussed, is the rapid ~~decay~~ decrease of farm-induced TKE in NWP-WFP simulations. While
108 less obvious, this problem is evident when closely examining the spatial evolution of TKE profiles downstream of turbine grid
109 cells. In NWP-WFP simulations, TKE ~~decays much~~ decreases more rapidly than in LES, as conceptually illustrated in Figs. 1e
110 and f, and supported by evidence from the literature (Figs. 5a–d in Vanderwende et al. (2016); Figs. 4 and 9 in García-Santiago
111 et al. (2024); Figs. 11–13 in Peña et al. (2022)). As more studies focus on wake recovery in large farms, this issue is becoming
112 more visible. For example, Rosencrans et al. (2024) found that the amount of TKE added by the farm influences near-farm wake
113 deficits but not the overall wake length. Similarly, Sanchez Gomez et al. (2024) noted that wake losses at an offshore wind farm
114 located approximately 15 km downstream of another farm were largely unaffected by the TKE factor. However, omitting the
115 TKE factor ($\alpha = 0$) resulted in the largest biases when compared with SCADA data. Furthermore, aircraft observations have
116 shown that TKE is overestimated in the first half of the farm by NWP-WFP, while in reality, TKE peaks further downstream
117 (Siedersleben et al., 2020).

118 These two interrelated issues—the underestimated wake recovery and the fast ~~decay~~ decrease of the farm-added TKE—
119 need a closer examination. While introduced here as two separate problems, turbulent mixing is a key driver for wake recovery
120 (~~Vermeer et al., 2003; Abkar and Porté-Agel, 2015; van der Laan et al., 2023~~). ~~Unrealistic decay~~ (Vermeer et al., 2003; Abkar and Porté-A
121 . Unrealistic decrease of the TKE can slow down wake recovery in NWP-WFP simulations. Therefore, these two issues raise a
122 few important questions. For instance, why does the farm-added TKE ~~decay~~ decrease more quickly in NWP-WFP simulations
123 than in the LES? How much does this rapid ~~decay~~ decrease contribute to the underestimated wake recovery? What other physi-
124 cal or numerical factors are involved? To address these questions, we evaluate the representation of wind farm wake recovery in
125 the NWP-WFP approach. Specifically, we aim to quantify the magnitude and spatial variability of the recovery process behind
126 a wind farm and identify the mechanisms behind the underestimation. This effort requires a large-domain LES to evaluate wake
127 recovery within, immediately downstream and in the far wake of the wind farm. To our knowledge, there are no NWP-WFP
128 vs. LES comparisons over downstream distances of ~ 40 km.

129 The remainder of this article is structured as follows. Section 2 describes the numerical setups used in this study, including
130 the WRF simulations with the ~~Fitch et al. (2012)~~ Fitch (Fitch et al., 2012) and MAV (Ma et al., 2022b, a) wind farm parame-
131 terization (NWP-WFP) and the reference LES with actuator disks (Kasper et al., 2024). The idealized simulations focus on a
132 600 MW offshore wind farm with ~~an aligned layout~~ aligned and staggered layouts, subjected to westerly flow under near-neutral
133 atmospheric conditions. In Section 3, we compare the undisturbed inflow conditions across models to ensure consistency. We
134 then assess wind farm performance and analyze wake recovery in the streamwise direction. Section 4 discusses in depth the
135 two main limitations of wake recovery in NWP-WFP mesoscale simulations using WFPs: the fast ~~decay~~ decrease of farm-added
136 TKE and the under-resolved gradients in the wind farm wake. Finally, Section 5 summarizes the key findings, with particular
137 emphasis on how these limitations impact the simulation of wind farm cluster wakes with NWP-WFP models.

139 To benchmark the NWP simulations with the WFP, we compare the results against LES by Kasper et al. (2024), who studied
 140 atmosphere–wind farm interactions under idealized conditions. Specifically, we consider the Barotropic (BT) case of their
 141 study, which here serves as the reference case that the mesoscale NWP simulations are designed to replicate. The simulation
 142 setup for this LES is briefly covered in Section 2.1, while a thorough discussion on the numerical framework can be found in
 143 Kasper et al. (2024). The subsequent Section 2.2 details the NWP-WFP framework, and the adaptations required to represent
 144 the LES conditions within a mesoscale model.

145 **2.1 Setup for the LES**

146 The reference simulation uses a modified version of the LES code developed by Albertson and Parlange (1999), later validated
 147 in Gadde et al. (2021). The model solves the incompressible filtered mass conservation, Navier–Stokes, and potential temper-
 148 ature transport equations. The subgrid-scale stresses and heat fluxes are modeled using the anisotropic minimum dissipation
 149 (AMD) scheme (Rozema et al., 2015; Abkar et al., 2016a), suitable for stratified boundary layers and wind farm wakes.

150 In the horizontal directions, the code employs pseudo-spectral differentiation and periodic boundary conditions, while
 151 second-order finite differencing is used in the vertical direction. A free-slip boundary condition is imposed at the top, with
 152 a Rayleigh damping layer to minimize gravity wave reflections. At the surface, a zero heat flux condition enforces neutral
 153 stratification, and shear stresses are parameterized using Monin–Obukhov similarity theory. Time integration uses a third-
 154 order Adams–Bashforth scheme. The simulation domain spans $102.4 \times 10.24 \times 10 \text{ km}^3$ in the streamwise, spanwise, and
 155 vertical directions, respectively. It is discretized using a rectilinear grid that consists of $2048 \times 512 \times 384$ points, with
 156 horizontal resolutions of $\Delta x = 50 \text{ m}$ and $\Delta y = 20 \text{ m}$. In the vertical, the resolution is uniform with $\Delta z = 10 \text{ m}$ up to
 157 $z_u = 1.5 \text{ km}$ above ground level (AGL), and stretched above using a hyperbolic tangent profile up to a maximum spacing
 158 of 62 m.

159 The simulated atmosphere represents an idealized offshore environment based on North Sea conditions. The geostrophic
 160 wind vector is prescribed with a magnitude $|\mathbf{U}_g| \approx 10 \text{ m s}^{-1}$, and the Coriolis frequency equals $f_c = 1.159 \times 10^{-4} \text{ s}^{-1}$.
 161 The surface roughness is set to $z_0 = 0.002 \text{ m}$, typical for open-sea conditions. The background stratification is neutral up
 162 to 1 km AGL, with a potential temperature of $\theta = 286 \text{ K}$. The boundary layer is capped by a 3 K inversion over 200 m,
 163 followed by a free-atmosphere lapse rate of 5 K km^{-1} .

164 Two sets of LES are considered, representing aligned and staggered wind-farm layouts. Wind turbines are represented
 165 using the actuator disk model (Jimenez et al., 2008; Calaf et al., 2010). The simulated wind farm consists of ten rows and
 166 six columns of turbines arranged in an aligned layout configuration, spaced by $s_x = 7D$ and $s_y = 5D$ in the streamwise and
 167 spanwise ~~direction~~directions, respectively. A staggered layout configuration is also considered, with an additional spanwise
 168 displacement of $2.5D$ between successive rows. The turbine diameter equals $D = 178 \text{ m}$ and the hub-height $z_h = 119 \text{ m}$ AGL,
 169 corresponding to the DTU 10-MW reference turbine (Bak et al., 2013). A uniform thrust coefficient $C_T = 0.75$ is used, and
 170 turbines yaw to face the local incoming wind.

171 ~~The~~ Each LES is run for a total of 11 hours and comprises two stages. First, a 7-hour spin-up simulation is run on a
 172 coarser grid with a resolution of $2\Delta_x \times 2\Delta_y \times \Delta_z$. Second, once the boundary layer reaches quasi-equilibrium (the mean
 173 wind and turbulence statistics display small variations over time), it is interpolated to the full resolution and the LES proceeds
 174 as a precursor-successor simulation (Stevens et al., 2014). The precursor provides realistic turbulent inflow to the successor
 175 domain containing the wind farm, preventing contamination of the inflow by remnants of the wakes via the periodic boundary
 176 conditions. Statistics are then collected over the final 3 hours of the simulation.

177 2.2 Setup for the NWP-WFP simulations

178 The NWP simulations use the Advanced-Research WRF model version 4.4 (Skamarock et al., 2019), which solves the com-
 179 pressible Euler equations in three spatial dimensions and time. The solver uses a time-split integration scheme. The low-
 180 frequency modes are integrated with a third-order Runge–Kutta scheme, whereas higher-frequency acoustic modes are inte-
 181 grated over smaller time steps. Advective terms are discretized using a fifth-order scheme in the horizontal and a third-order
 182 scheme in the vertical directions. The model applies Arakawa C-grid staggering in the horizontal direction, with a hydrostatic
 183 pressure-based coordinate in the vertical direction.

184 Idealized simulations are employed, omitting cloud microphysics, radiation, moisture, and surface heterogeneity, which are
 185 standard simplifications in studies targeting canonical boundary layers over flat terrain (Fitch et al., 2012; Vanderwende et al.,
 186 2016; Volker et al., 2015; Peña et al., 2022; García-Santiago et al., 2024). In the multiscale framework of the WRF model,
 187 turbulence is entirely parameterized by the PBL scheme for mesoscale grid spacings ($\Delta X \sim 1$ km). Vertical turbulent mixing
 188 is represented by the MYNN PBL scheme (Nakanishi and Niino, 2009; Olson et al., 2026), while horizontal mixing is treated
 189 using a two-dimensional first-order Smagorinsky closure with constant eddy diffusivity (Skamarock et al., 2019). In MYNN,
 190 TKE is prognosed from a budget equation that includes shear production, buoyancy production or destruction, vertical turbulent
 191 transport, and dissipation (Nakanishi and Niino, 2009; Olson et al., 2026). The diagnosed TKE is then used to compute eddy
 192 diffusivities through stability-dependent mixing-length formulations, which directly control the vertical transport of momentum
 193 and scalars in the PBL. Since vertical turbulent transport dominates near-farm wake recovery (Lanzilao and Meyers, 2025; Kasper and Stev
 194 , the discussion here primarily reflects the role of the PBL scheme and grid-resolved dynamics in governing vertical mixing
 195 and shear-driven entrainment.

196 A two-domain nesting configuration is adopted (Fig. 2), with one-way coupling from a parent domain to an inner nest.
 197 The outer domain generates nearly steady boundary-layer inflow characteristics, which are passed to the nested domain. Both
 198 domains use a constant horizontal resolution ($\Delta X = \Delta Y$), hereafter referred to simply as ΔX , as specified in Table 1, ranging
 199 from 346 m to 1246 m for the sets of simulations considered here. Simulations with the finest horizontal grid resolutions
 200 ($\Delta X = 2D$, or 346 m, DX2D and DX2DTKE100) use a coarser resolution ($\Delta X = 5D$, 890 m) for the outer domain, with a
 201 parent grid aspect ratio of 3. Vertically, a fine 10-m resolution is used below 400 m AGL for all domains, resolving the turbine
 202 rotor layer with multiple grid points. The computational domain is larger than in the LES to further minimize the influence of
 203 lateral boundaries, as the added computational cost is relatively small for the NWP-WFP simulations. For most cases (except
 204 DX2D and DX2DTKE100) the innermost domain spans approximately 188 km streamwise and 63 km spanwise. In the finest-

205 resolution cases (DX2D and DX2DTKE100), it spans about 100 km and 40 km in the streamwise and spanwise directions,
 206 respectively. All domains extend 5 km vertically.

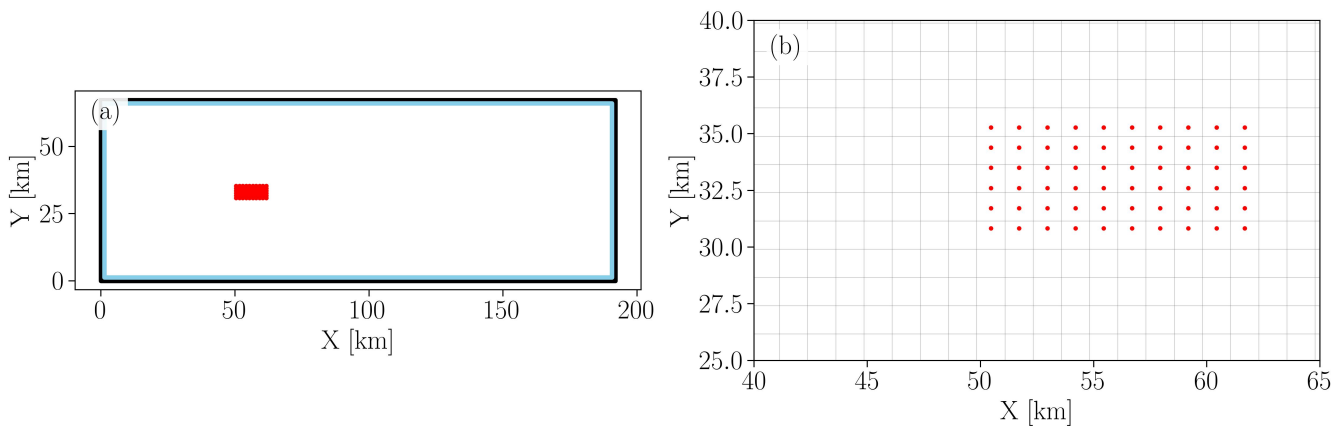


Figure 2. Two computational domains are used in the WRF-WFP simulations, illustrated here for the baseline (BASE) case (a). The outer parent domain (D1, black rectangle), which uses periodic lateral boundary conditions and does not include a wind farm, provides inflow to the inner nested domain (D2, blue rectangle) via one-way nesting. The inner domain includes the wind farm, with turbines represented as red dots. In the BASE setup shown in panel (b), each grid cell contains one turbine, except for the cells between $Y = 32\text{--}34$ km, which contain two.

Table 1. Summary of the NWP-WFP simulations, their subsets and key parameters: horizontal grid resolution (ΔX), TKE addition coefficient (α), [WFP](#) and turbine thrust coefficient (C_T).

Case	Subset	ΔX [m]	α	C_T
BASE	Baseline	1246 (7D)	0.25	0.75
TKE000	TKE	1246 (7D)	0.00	0.75
TKE050	TKE	1246 (7D)	0.50	0.75
TKE075	TKE	1246 (7D)	0.75	0.75
TKE100	TKE	1246 (7D)	1.00	0.75
DX5D	Grid	890 (5D)	0.25	0.75
DX2D	Grid	346 (2D)	0.25	0.75
DX2DTKE100	Grid	346 (2D)	1.00	0.75
MAV	WFP	1246 (7D)	0.25	0.75
MAVDX12D	WFP	2076 (11.6D)	0.25	0.75
CT050	Thrust	1246 (7D)	0.25	0.50
CT081	Thrust	1246 (7D)	0.25	0.81
CTTC	Thrust	1246 (7D)	0.25	Thrust Curve (TC)

207 The wind farm is represented using the Fitch ~~WFP (Fitch et al., 2012)~~ [\(Fitch et al., 2012\)](#) and [MAV \(Ma et al., 2022b, a\)](#)
 208 [WFPs](#), with TKE advection enabled (Archer et al., 2020) and axial induction modified following Vollmer et al. (2024). The

209 wind farm consists of 60 DTU 10-MW turbines (Bak et al., 2013), configured identically to Kasper et al. (2024). Each turbine
 210 has a rotor diameter $D = 178$ m and a hub height $z_h = 119$ m AGL. A constant thrust coefficient of $C_T = 0.75$ is used
 211 in all cases, except for those included in the C_T sensitivity study. Details on the turbine model and the sensitivity analysis
 212 are provided in Appendix A. The ~~wind farm~~ NWP-WFP simulations consider only the aligned wind farm layout. Because
 213 the coarser-resolution Fitch cases (BASE, TKE100) spatially over-distribute the wind speed deficit, the aligned configuration
 214 represents a worst-case scenario in terms of wake effects; accordingly, the staggered LES is also used as a reference for
 215 comparison with these coarser Fitch simulations.

216 The wind farm occupies a region starting around $X = 50$ km and $Y = 30$ km from the western and southern boundaries.
 217 The wind farm spans 11 km streamwise and 4.4 km spanwise, with turbine spacing of $7D$ (1246 m) in the streamwise and $5D$
 218 (890 m) in the spanwise directions. Uniform turbine spacing in the coarse NWP-WFP grid is only achieved with Fitch when
 219 grid spacing matches the physical turbine spacing. For instance, the BASE case has a uniform horizontal spacing which ensures
 220 a uniform representation of turbine spacing in the streamwise direction ($\Delta X = S_x = 7D$), but not in the spanwise direction
 221 where turbines are more closely spaced ($\Delta X = 7D$ but $S_y = 5D$).

222 To investigate the role of subgrid wake effects on wake recovery, we additionally implemented the “MAV” wind farm
 223 parameterizations (Ma et al., 2022b, a), ported from the standard release of WRF v4.6. The MAV WFP is based on the
 224 analytical wake model of Xie and Archer (2015) and represents wake overlap through a superposition of hub-height wind speed
 225 deficits (Ma et al., 2022a). In contrast to the Fitch scheme, which relies on grid-cell-averaged momentum extraction, MAV
 226 explicitly accounts for subgrid wake interactions and has been shown to improve turbine power predictions when compared
 227 against offshore SCADA data (Ma et al., 2022a).

228 Surface boundary conditions assume flat, homogeneous terrain with roughness length $z_0 = 0.002$ m and zero surface heat
 229 flux (neutral stability). The surface-layer scheme applies ~~Monin-Okukhov~~ Monin-Obukhov Similarity Theory (MOST)-based
 230 drag using near-surface wind speeds. The Coriolis parameter corresponds to a latitude of 52.65° . The upper boundary enforces
 231 zero vertical velocity and free-slip horizontal flow. A Rayleigh damping layer (coefficient 0.2 s^{-1}) occupies the top 2 km of
 232 the domain to absorb gravity waves.

233 Initial conditions prescribe a uniform, westerly flow from 282° at 10.93 m s^{-1} . The initial potential temperature is uniform
 234 at 286 K below 1000 m AGL, then increases with lapse rates of 15 K km^{-1} (1000–1200 m AGL) and 5 K km^{-1} (above 1200 m
 235 to the 5-km AGL domain top) to match the LES. Simulations run for 27 hours, with the final hour used for analysis after a
 236 26-hour spin-up. The initial forcing is fine-tuned to ensure post-spin-up conditions match target values, a standard approach
 237 in idealized WRF setups (Mirocha et al., 2018; Peña et al., 2021; Hsieh et al., 2025). Inertial oscillations driven by Coriolis
 238 effects also modulate boundary-layer winds during spin-up. The chosen spin-up time ensures minimal residual oscillations in
 239 the analysis period.

240 Three simulation sets and a baseline case are run (Table 1). The baseline (BASE) case uses a horizontal resolution equal to the
 241 turbine streamwise spacing ($7D$) to avoid subgrid wake effects from multiple turbines in one cell. It applies a thrust coefficient
 242 of $C_T = 0.75$ (such as in (Kasper et al., 2024)) and a TKE addition coefficient of $\alpha = 0.25$ (Archer et al., 2020). The TKE
 243 subset includes $\alpha = 0.00, 0.50, 0.75$ and 1.00 . The grid subset varies ΔX between 346 m ($2D$) and 890 m ($5D$). The thrust

subset applies constant C_T values of 0.50 and 0.81, and also includes a wind-speed-dependent thrust case (see Appendix A). This subset serves to assess the sensitivity of the wake generation and recovery relative to the choice of $C_T = 0.75$ in the LES. The high-resolution cases DX2D and DX2DTKE100 are used to assess the impact of sharper wake gradients on power and recovery, acknowledging limitations of the application of traditional PBL schemes at sub-kilometer resolutions due to the *terra incognita* (Wyngaard, 2004; Rai et al., 2019; Haupt et al., 2019, 2023).

3 Results

3.1 Undisturbed inflow profiles

Before delving into modeling differences and similarities between NWP-WFP and LES in terms of power production and wake recovery, it is necessary to evaluate inflow variability to ensure inflow profiles are sufficiently similar so that downstream differences are not attributed to inflow variability (Peña et al., 2022; Hsieh et al., 2025). There is excellent agreement between NWP-WFP and LES inflow profiles for all variables (Fig. 3). The differences in hub-height (WS_{119}) and rotor-averaged (WS_r) wind speed compared to the LES are approximately 0.03 and -0.01 m s^{-1} , respectively, as shown in Table 2.

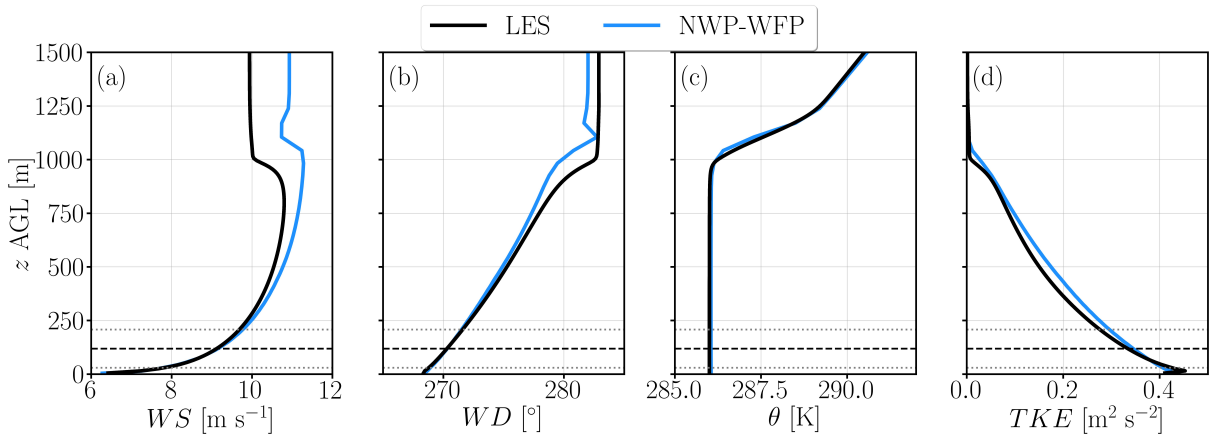


Figure 3. Time- and horizontally-averaged profiles of wind speed (a), wind direction (b), potential temperature (c), and TKE (d) during the analysis window for LES (black line) and NWP-WFP (blue line) in the simulation without turbines. The horizontal dashed and dotted gray lines denote rotor hub height and bottom/top tips, respectively.

Not only do the hub-height and rotor-averaged values match well, but so do the wind shear (α_r) and veer (β_r) across the rotor (Figs. 3a, b). This is important because under near-neutral conditions, turbulence production is governed primarily by mechanical shear, both in wind speed and direction (Stull, 1988). The fact that similar wind speed and direction profiles result in similar TKE profiles (Fig. 3d) reinforces the physical consistency between the models. The NWP-WFP wind speed profile exhibits slightly greater shear between 300 and 800 m AGL, which leads to marginally higher TKE values in that layer. Surface boundary conditions are also consistent, as indicated by the good agreement in friction velocity (u_* , Table 2).

Table 2. Time-averaged inflow properties from the precursor simulations and their differences. Subscripts 119 and r denote hub-height (in m AGL) and rotor-averaged values, respectively. For wind shear (ΔWS_r) and veer (ΔWD_r), values represent the difference between the top and bottom rotor tips.

Source	WS_{119} [m s ⁻¹]	WD_{119} [°]	TKE_{119} [m ² s ⁻²]	WS_r [m s ⁻¹]	WD_r [°]	TKE_r [m ² s ⁻²]	u_* [m s ⁻¹]	ΔWS_r [m s ⁻¹]	ΔWD_r [°]
NWP-WFP	9.15	270.3	0.35	9.02	270.3	0.35	0.32	1.98	2.58
LES	9.12	270.3	0.33	9.03	270.3	0.34	0.33	1.87	2.81
Difference	0.03	0.0	0.01	-0.01	0.0	0.01	-0.01	0.12	-0.23

3.2 Row-averaged streamwise power patterns

This section evaluates streamwise changes in row-averaged power (i.e., averaged across turbines within the same row) for the TKE (Fig. 4a) and grid resolution (Fig. 4b) simulation subsets. These results reflect both the magnitude of wake effects ~~on~~ downstream-owing to momentum extraction by the turbines and the ability of ~~the~~ this waked flow to recover momentum within the wind farm.

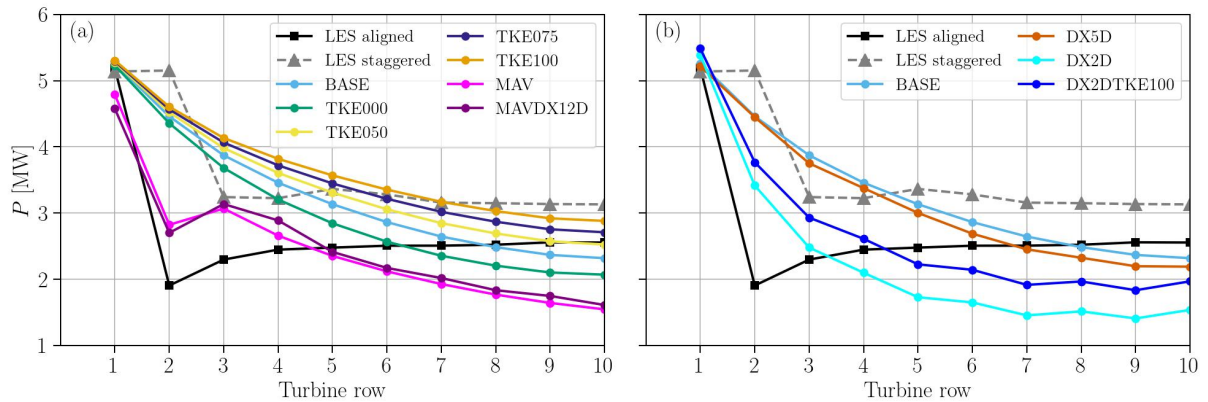


Figure 4. Row-averaged power in the NWP-WFP set of simulations with different wind farm added TKE and WFP (a) and grid resolutions (b) compared with the LES.

Compared to ~~the~~ both the aligned and staggered LES, there is excellent agreement in the first-row averaged power output (~ 5 MW; Fig. 4a), which stems from the matched inflow profiles (Fig. 3) and the implementation of the Fitch WFP correction (Vollmer et al., 2024). This agreement indicates that turbine power is consistently modeled across both simulation frameworks, enabling a meaningful evaluation of model-specific biases. The MAV and MAVDX12D cases exhibit lower power due to the absence of an induction correction, while the DX2D and DX2DTKE100 cases slightly overestimate first-row power (Fig. 4b) as a result of marginally stronger inflow wind. Additionally, increasing the farm-added TKE enhances row-averaged power output by promoting more efficient wake recovery via momentum transport into the farm.

274 In the aligned LES, the power drops sharply in the second row (to ~ 2 MW) and is followed by a gradual power recovery
 275 downstream (Figs. 4a,b), as is often observed in LES studies of dense offshore wind farms with an aligned layout (Allaerts and
 276 Meyers, 2017; Stevens and Meneveau, 2017; Stieren and Stevens, 2022; Stipa et al., 2024). For ~~staggered layouts~~the staggered
 277 layout, the power decrease is smaller because the effective streamwise distance between turbine rows doubles compared to the
 278 aligned layout (Stieren and Stevens, 2022). None of the NWP-WFP simulations using Fitch capture the sharp drop in power,
 279 instead displaying a more gradual pattern of power decrease. ~~Only the DX2D and DX2DTKE100 cases (Fig. 4b) show some agreement with the LES owing to aligned LES due to a more accurate representation of~~
 280 ~~subgrid wake effects, while only the DX2D and DX2DTKE100 cases (Fig. 4b) achieve similar agreement through~~ their finer
 281 spatial resolution ($\Delta X = 2D$). Coarser-resolution Fitch cases, regardless of the added TKE (Figs. 4a), tend to overestimate
 282 power in the upstream half of the farm when considering the aligned LES the reference. This power overestimation results
 283 from weaker wake losses, as the coarse NWP-WFP grid ($\Delta X = 1$ km) dilutes wake structures spatially. This limitation has
 284 been previously documented (Archer et al., 2020; Sanchez Gomez et al., 2024). The agreement improves considerably if the
 285 staggered LES case is considered the reference.

287 At finer resolution (cases DX2D and DX2DTKE100), wakes become sharper and induce more realistic power deficits in
 288 turbine rows 2–4 (Fig. 4b) compared with the aligned LES. The absence of power recovery beyond the second row in the
 289 NWP-WFP simulations, compared to the LES (Figs. 4a,b), likely stems from insufficient wake recovery, an aspect discussed
 290 further in Section 3.4. ~~Consequently, power performance patterns produced by-~~

291 In summary, the coarser NWP-WFP simulations may differ significantly from those in the LES. This discrepancy should
 292 ~~be considered when employing NWP-WFP for intra-farm power performance assessments. configurations, the Fitch WFP~~
 293 spatially averages the wind speed deficit over each grid cell, leading to an underestimation of wake losses at downstream
 294 turbines and a corresponding overestimation of power. This excess power implies enhanced momentum extraction within the
 295 wind farm, which modulates the wind speed at the farm exit. The MAV scheme mitigates this behavior by explicitly accounting
 296 for subgrid turbine-turbine wake interactions, resulting in more realistic wake losses and power levels. As a result, the wind
 297 speed at the wind farm exit, which is critical for downstream wake recovery, is more accurately represented when subgrid wake
 298 effects are included.

299 3.3 Wind farm wake flow field and spatial average

300 In this section, we compare the representations of hub-height wind speed and TKE by the LES and NWP-WFP simulations. The
 301 goal is to quantify the differences in wind farm wake structure and recovery between the aligned and staggered LES, spatially
 302 averaged to the grid of the BASE case (~~coarsened LES~~Fig. 5), and selected NWP-WFP cases (Fig. ~~??6~~). The coarsened LES
 303 ~~result is results for both aligned and staggered cases are~~ obtained by spatially averaging the ~~full-resolution native-resolution~~
 304 LES data located within individual grid cells of the BASE case, enabling a direct comparison between the two (Figs. ~~??k,15k-n~~),
 305 as in previous studies (Vanderwende et al., 2016; Peña et al., 2022; García-Santiago et al., 2024). The origin of the coordinate
 306 system is shifted to the southwest corner of the wind farm. Throughout the text, we divide the wind farm wake into three
 307 distinct regions: the intra-farm wake ($0 \text{ km} < X < \text{11.2 km}$), the near-farm wake ($\text{11.2 km} < X < 15 \text{ km}$), and the far

wake of the farm ($X > 15$ km). The wind farm exit separates the intra-farm and near-farm wake regions. The thick black rectangle shows the wind farm perimeter as defined by the WFP. In the case DX2D (Fig. 6e,f), the finer resolution results in a smaller represented perimeter compared to the BASE case.

The full-resolution LES (Figs. 5a,b) exhibits sharp streaks of alternating low and high wind speed and TKE due to the aligned turbine layout (Stieren and Stevens, 2022; Stipa et al., 2024). These streaks extend approximately 3–5 km downstream before merging into a single and broader structure (Fig. 5a). For the staggered layout (Figs. 5e), the streaks are more broadly distributed in the spanwise direction. In contrast, the coarsened LES aggregates and smooths out these microscale variabilities (Fig. 5c,g), producing more homogeneous flow and turbulence fields within the farm. In the far wake region ($X > 15$ km), the LES and coarsened LES fields become similar, as turbulent mixing has reduced the spatial gradients in wind speed and TKE.

A persistent feature in the coarsened aligned LES, BASE and TKE100 cases (Figs. e-e,g) cases-5c,i and 6c) is a narrow band of reduced wind speed around $Y = 2.5$ km. This more intense wake results from the Y -direction turbine spacing ($s_y = 5D$) being finer than the grid spacing ($\Delta X = 7D$), such that two turbine columns fall within a single grid cell. This aggregation produces a locally stronger momentum sink and TKE source (Fitch et al., 2012).

Although the total momentum sink in DX2D is comparable to BASE and TKE100, the local wind speed deficits are larger due to the finer resolution, which produces more concentrated wakes (Figs. 6e). This localization of the wind speed deficits explains the improved agreement with the aligned LES regarding the second-row power losses for cases DX2D and DX2DTKE100 (Fig. 4b).

The wind speed (ΔWS_{119}) and TKE (ΔTKE_{119}) differences, calculated as the BASE case minus the coarsened LES (Figs. k,5k-n), are small upstream and beside the wind farm for both aligned and staggered layouts. Faint blue bands of negative ΔWS_{119} appear outside the spanwise averaging region, caused by stronger acceleration around the wind farm in the LES. Within the farm, ΔWS_{119} transitions from slightly positive in the first few rows, to near-zero at row 4, and then to negative further downstream. The strongest negative wind speed differences occur in the near-farm wake (11.2 km $< X < 15$ km), followed by a modest recovery, but remain between -0.5 and -1 m s $^{-1}$ in the far wake of the farm ($X > 20$ km). For the aligned layout (Fig. 5k). For the staggered layout (Fig. 5m), wind speed differences are reduced, indicating improved agreement between the BASE case and the LES. For ΔTKE_{119} , the BASE case overestimates TKE compared to the both the aligned and staggered LES in the first turbine row and underestimates it in rows 3 and further downstream. In the near-wake near-farm wake (11.2 km $< X < 15$ km), the TKE remains underestimated but recovers further downstream ($X > 20$ km) where the agreement with the LES is excellent.

3.4 Intra-farm, near-farm and far wake recovery

Here, we assess how the streamwise evolution of the wind farm wake is affected by changing the TKE-coefficient-added TKE coefficient and WFP (Fig. 7) and the grid resolution (Fig. 8). The time-averaged wind speed and TKE are evaluated at hub height and averaged in the spanwise direction within the bounds ($Y = -0.923$ and 5.307 km) of the horizontal dashed lines represented in Fig. 5, the lateral extent of the wind farm in the reference BASE case. Furthermore, to mitigate averaging

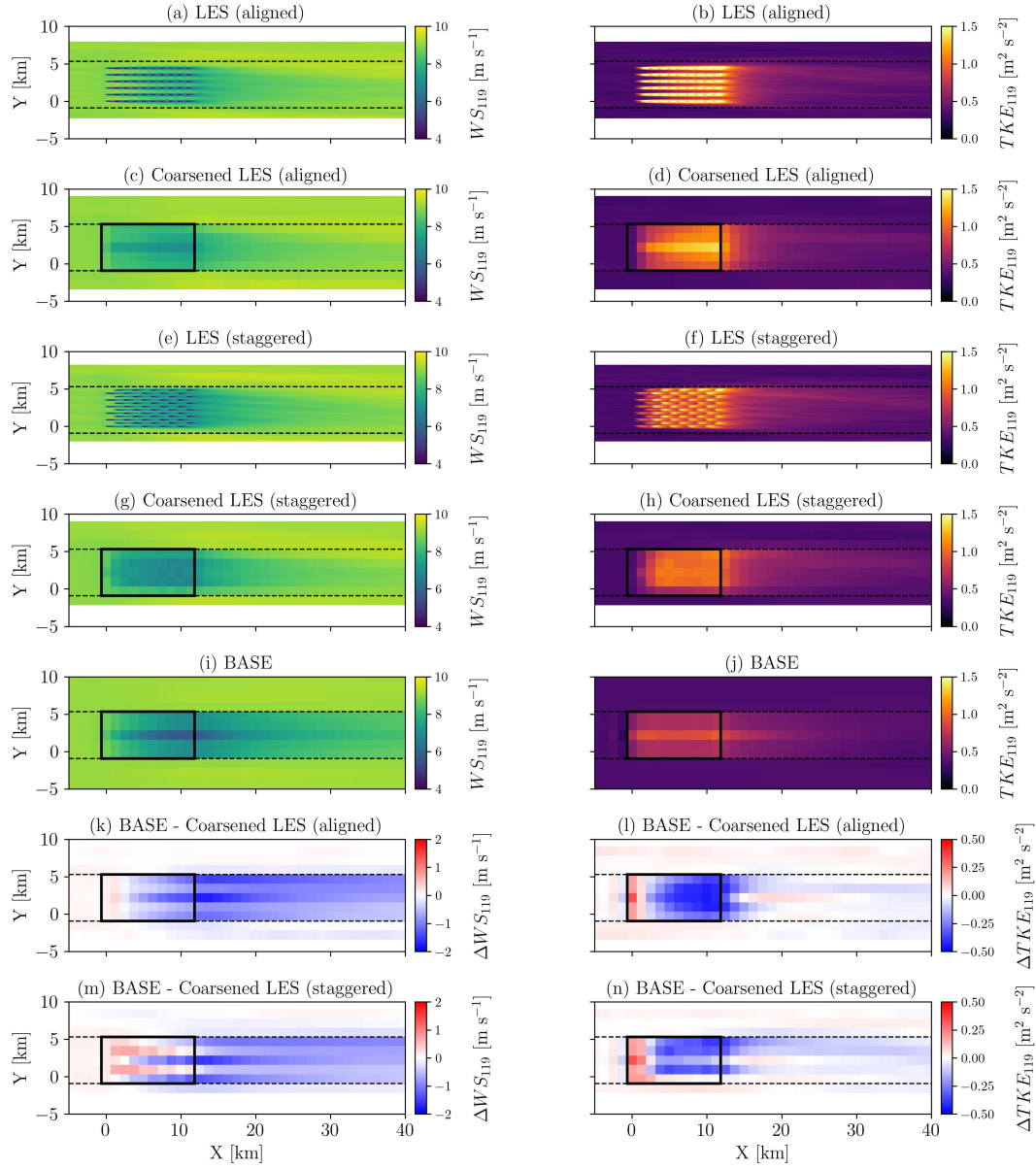


Figure 5. Time-averaged wind speed (WS_{119}) and TKE (TKE_{119}) at hub height for the aligned LES (a, b), coarsened aligned LES (c, d), staggered LES (e, f), coarsened staggered LES (g, h), NWP-WFP case BASE (i, j). The last two rows show the difference between the BASE case and the coarsened aligned (k, l) and staggered LES (m, n). The black rectangles indicate the wind farm perimeter as represented in the NWP-WFP simulation. Horizontal dashed lines mark the spanwise extent of the region used for averaging.

errors from the coarse mesoscale resolution near the spanwise boundaries, all results are first interpolated to a higher-resolution grid ($\Delta X = 50$ m).

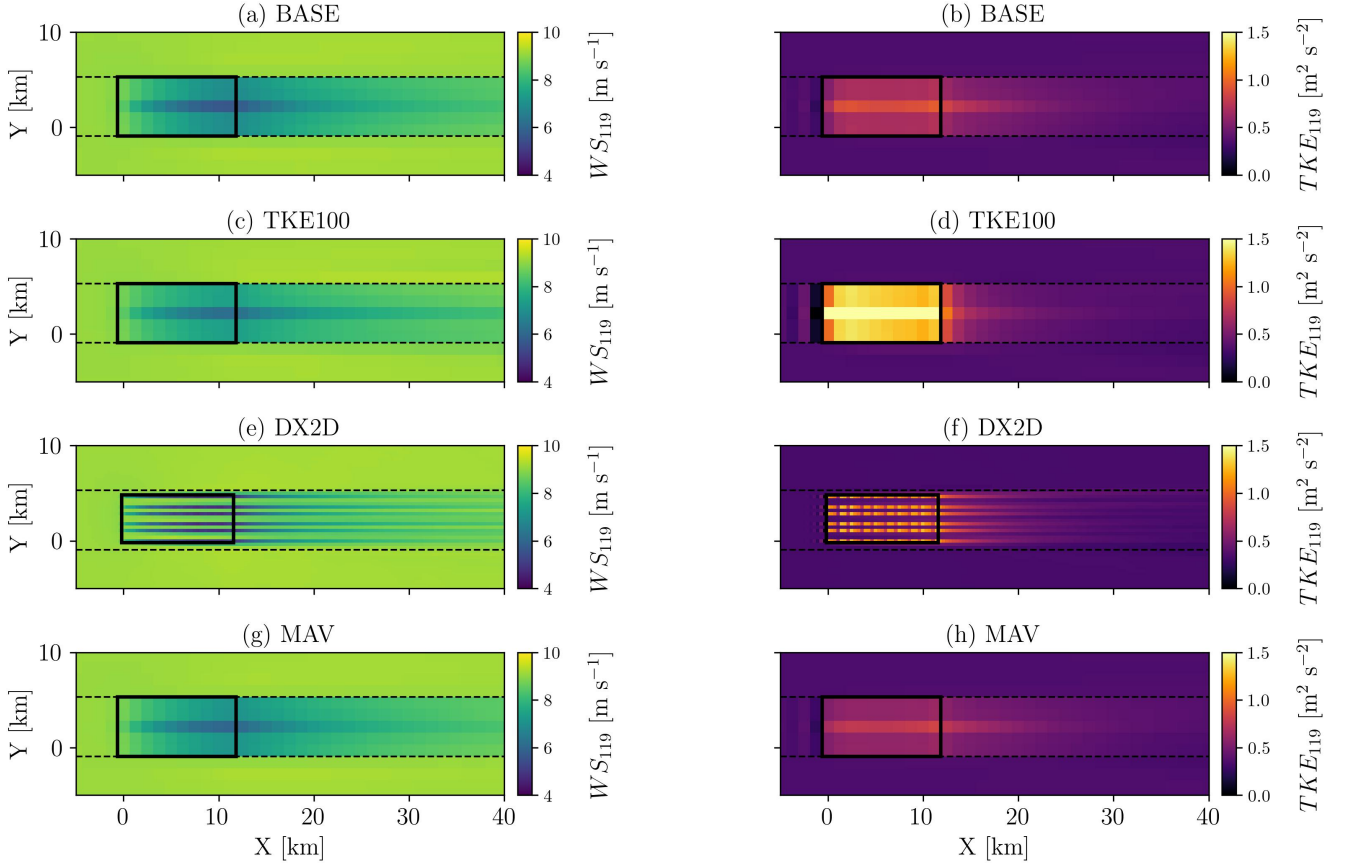


Figure 6. Time-averaged wind speed (WS_{119}) and TKE (TKE_{119}) at hub height for the LES-NWP-WFP cases BASE (a, b), coarsened-LES TKE100 (c, d), NWP-WFP cases BASE and DX2D (e, f), TKE100 and MAV (g, h), and DX2D (i, j). The last row shows the difference between the BASE case and the coarsened LES (k, l). The black rectangles indicate the wind farm perimeter as represented in the NWP-WFP simulation. Horizontal dashed lines mark the spanwise extent of the region used for averaging.

343 The NWP-WFP
 344 In the intra-farm wake region, the momentum extraction by the turbines acts simultaneously with the wake recovery. The
 345 coarse Fitch simulations slightly underestimate the wind speed deficit in the first three turbine rows of the wind farm (leading to
 346 overestimated power production, Fig. 4) but overestimate the deficit further downstream (Figs. 7a and 8a). Increasing the added
 347 TKE has little impact on the first few turbine rows, because momentum entrainment builds up progressively row by row, with its
 348 cumulative effects most evident at) relative to the aligned LES. However, using the staggered LES as reference produces much
 349 better agreement in the second half of the wind farm exit, especially for the TKE050–100. Notably, the cases with α values of
 350 75% and 100% show clear improvement at the wind farm exit and in the near-wake region ($X < 15$ km). Differences in wind
 351 speed between the NWP-WFP cases diminish in the far wake (Figs. 7a and 8a). Overall, regardless of the TKE coefficient, all

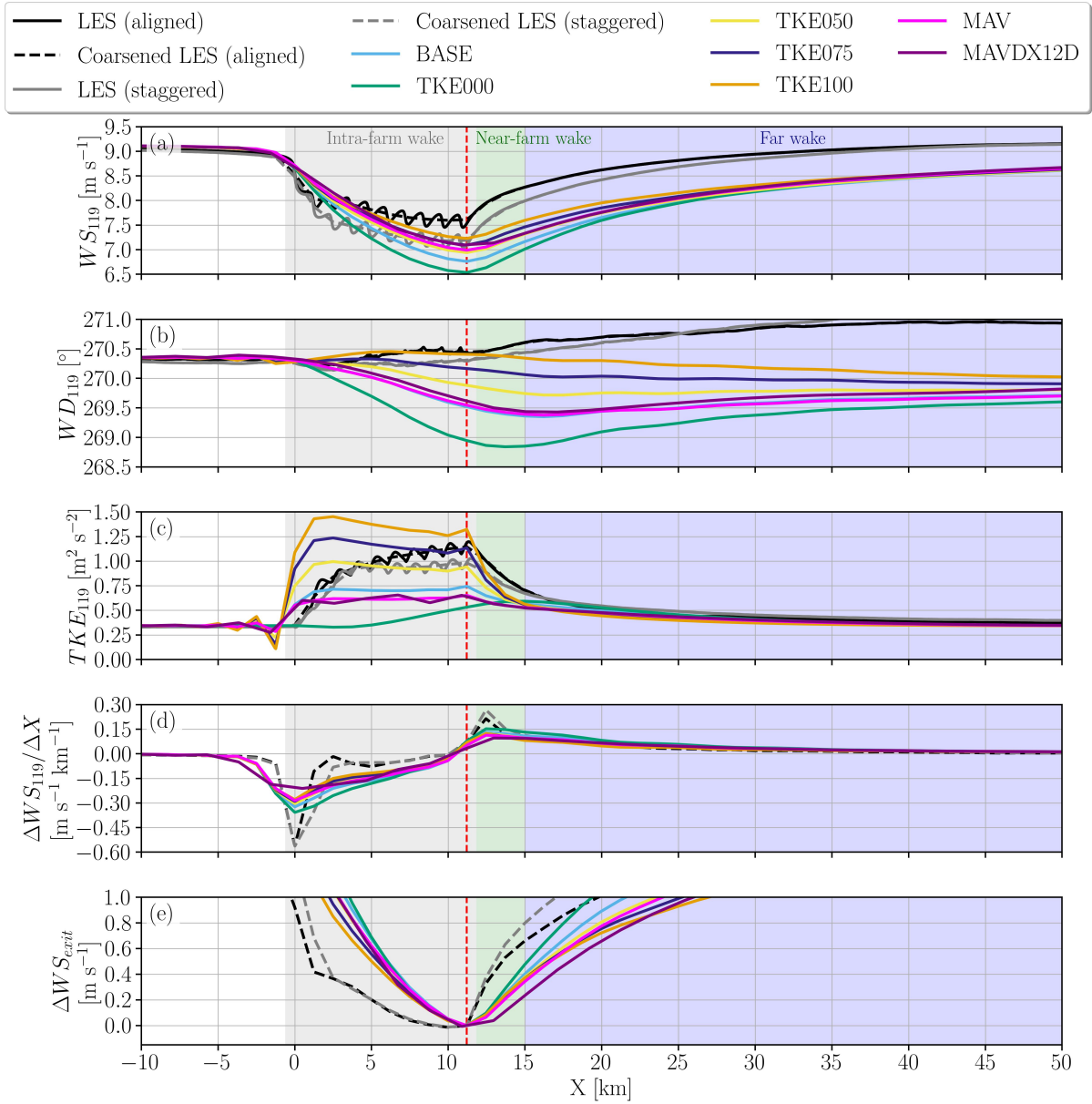


Figure 7. Streamwise variation of spanwise averages over the wind farm area of hub-height wind speed (a), wind direction (b), TKE (c), and streamwise gradient of wind speed (d) and wind speed change relative to the wind farm exit (e) for the aligned and staggered LES at full resolution, coarsened LES, and NWP-WFP cases with different α . The colored background areas indicate the streamwise extent of the intra-farm wake (gray), near-farm wake (green), and far wake of the farm (blue). The red vertical dashed line marks the wind farm exit.

the mesoscale simulations display a consistent negative wind speed bias ranging from approximately -0.7 m s^{-1} (TKE000) to -1.3 m s^{-1} (TKE100) in the near-farm wake at $X = 15 \text{ km}$. The bias decreases to approximately -0.6 m s^{-1} in the far

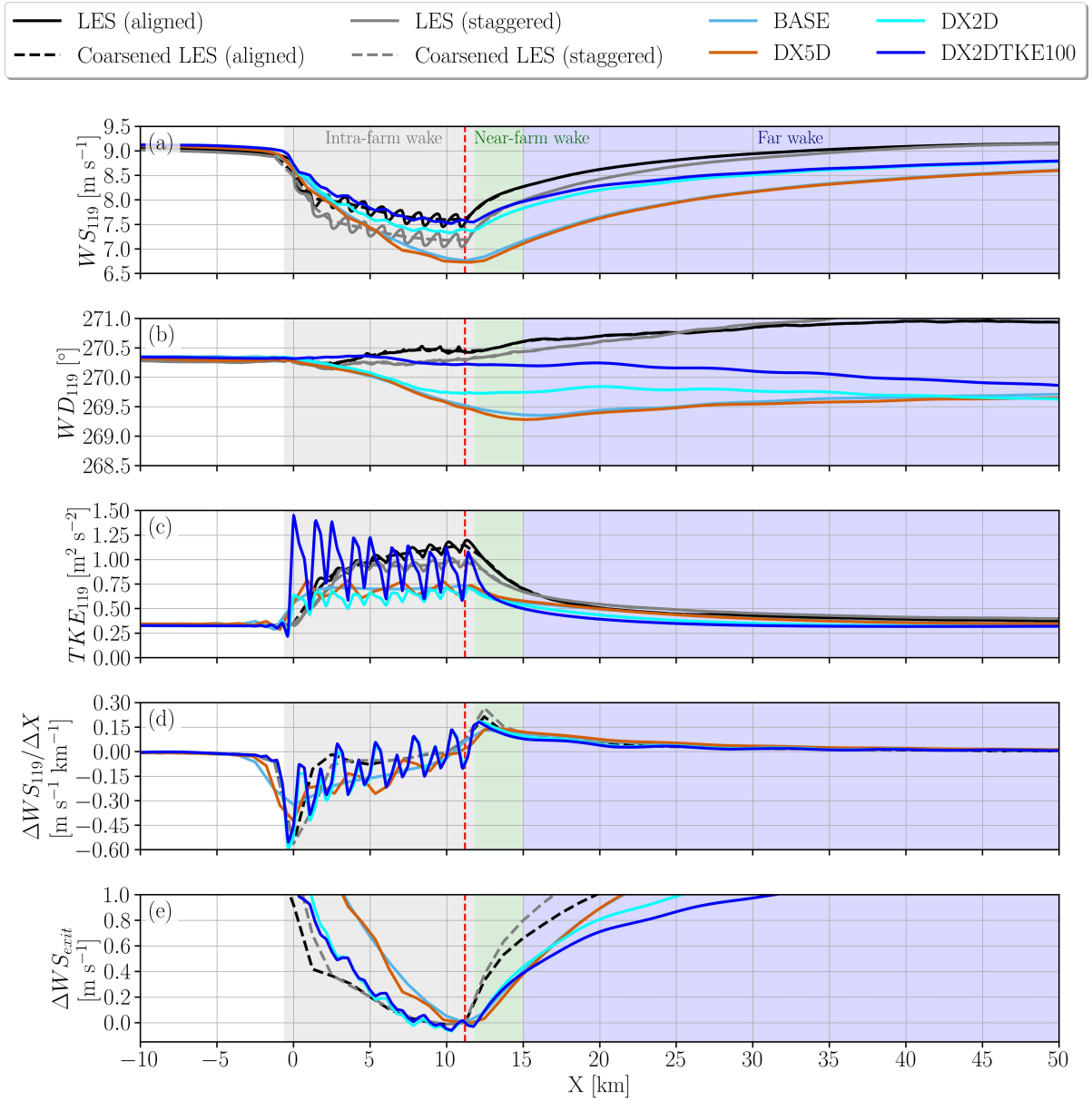


Figure 8. Streamwise variation of spanwise averages over the wind farm area of hub-height wind speed (a) Same as Fig. 7, wind direction (b), TKE (c), and streamwise gradient of wind speed (d) but for the LES at full-resolution, coarsened LES, and NWP-WFP-Fitch cases with different grid resolutions. The colored background areas indicate the streamwise extent of the intra-farm wake (gray), near-farm wake (green), and far wake of the farm (blue).

354 wake ($X = 50$ km) for all cases (Fig. due to the enhanced momentum entrainment into the wake associated with the larger
 355 TKE.

356 The MAV cases are superior to Fitch's BASE case because the improved representation of subgrid wake effects leads to
 357 better turbine power and momentum extraction predictions (Ma et al., 2022a). Because of the smaller momentum extraction
 358 relative to the BASE case, the added TKE is also smaller. The similar trends in most variables (Figs. 7a) compared to the
 359 LESa-c) between the coarser MAVDX12D and the finer MAV demonstrate the consistency of this WFP across different spatial
 360 resolutions.

361 The grid resolution exerts a stronger impact on improving the bias. The bias improves considerably for the two finest
 362 resolution cases. Simulations with the finest grid resolution (DX2D and DX2DTKE100 (horizontal resolution of $2D$), with
 363 wind speed deficits of -0.3 m s^{-1} (DX2DTKE100) and -0.5 m s^{-1} (DX2D) in the) improve the representation of wind
 364 speed in the intra-farm and near-farm wake at $X = 15 \text{ km}$ (Fig. 8a). This improvement is first attributed to the
 365 more realistic predictions of turbine power in these cases (Fig. 4b), which imply a more accurate extraction of momentum by
 366 the wind farm. As a result, the generated wake exhibits a wind speed deficit that more closely matches the aligned LES near
 367 the wind farm exit. In the far wake at $X = 50 \text{ km}$, the bias of approximately -0.4 m s^{-1} for the DX2D and DX2DTKE100
 368 remains relatively similar to the values in the near-farm wake (from -0.3 to -0.5 m s^{-1}). However, the BASE case ($7D$ or
 369 1246 m resolution) and the DX5D case ($5D$ or 890 m resolution) yield very similar results, suggesting that the modest increase
 370 in mesoscale grid resolution does not noticeably affect the wake.

371 The streamwise gradient of wind speed ($\Delta WS_{11g}/\Delta X$) quantifies wake recovery (

372 The combination of momentum extraction and wake recovery inside the wind farm creates the wind speed and TKE
 373 conditions at the farm exit (the red vertical dashed line in Fig. 7d). This condition at the farm exit is relevant for the
 374 subsequent recovery of the near-farm wake. Among the cases varying the TKE coefficient (Fig. 7a), TKE100 most closely
 375 approximates the LES within the farm area. In the far wake ($X > 20 \text{ km}$), streamwise derivatives across all cases converge
 376 and agree well with the LES, despite the bias in absolute wind speed aligned LES at the farm exit. The agreement improves
 377 with the staggered LES as the reference. The TKE000 case is the worst performing because the momentum extraction is not
 378 counterbalanced by the wake recovery within the farm. The MAV cases perform better than Fitch's BASE case and would
 379 possibly perform even better with more added TKE considering the aligned LES. However, the greatest divergence

380 The momentum extraction by the turbines ceases in the near-farm wake region so that the wake recovery rates can be
 381 evaluated in isolation. The streamwise gradient of wind speed ($\Delta WS_{11g}/\Delta X$) and the wind speed change relative to the
 382 wind farm exit (ΔWS_{exit}) quantify the near-farm wake recovery (Fig. 7d,e). The greatest divergence between the NWP-WFP
 383 simulations and the LES occurs in the near-farm wake ($11.2 < X < 15 \text{ km}$), where the NWP-WFP simulations all fail to
 384 capture a peak in recovery rate (Fig. 7d). Thus, that the wake recovery in the LES is faster immediately after the wind farm
 385 exit, which is also noticeable in the shape of the streamwise wind speed curvature (Fig. 7a). Even case-cases TKE100 and
 386 MAV, which most closely approximates the LES wind speed in the near-farm wake, underestimates the wake recovery rate
 387 downstream. This discrepancy suggests that a key mechanism for wake recovery is not adequately captured in the NWP-WFP
 388 simulations in the near-farm wake.

389 Simulations with the finest grid resolution (DX2D and DX2DTKE100) improve the representation of wind speed in the
 390 intra-farm and The near-farm wake regions (Fig. 8a). The wake recovers slightly faster in finer-resolution cases, as evident in both the

391 wind speed (Fig. 8a,d). This improvement is first attributed to the more realistic predictions of turbine power in these cases
392) and the streamwise gradients in wind speed (Fig. 4b8d), which ~~imply a more accurate extraction of momentum by the wind~~
393 ~~farm~~. As a result, the generated wake exhibits a now reproduce the peak displayed by the LES. Finally, adding more TKE
394 ($\alpha = 100\%$) in the high-resolution simulation mostly influences the momentum extraction within the farm but has a weak
395 influence on wake recovery rates.

396 Even though the difference in near-farm wake recovery rates between the NWP-WFP simulations and the LES occurs over a
397 relatively short distance ($\sim 1-2$ km), it produces measurable bias in wind speeds. Notice that even if some cases match the wind
398 speed (TKE100 and aligned LES) at the farm exit (Fig. 7a), a departure between the two curves occurs downstream. Between
399 ~~the wind speed deficit that more closely matches the LES near the wind farm exit~~. Secondly, ~~the~~ at 11.2 km and 15 km, the gain
400 in wind speed is of about 0.65 m s^{-1} and 0.8 m s^{-1} for the aligned and staggered LES (Fig. 7e), respectively. The change in
401 wind speed is much smaller for the coarser resolution NWP-WFP cases, in the range between 0.2 and 0.5 m s^{-1} (Fig. 7e). On
402 the other hand, the higher resolution cases gain about 0.4 m s^{-1} (Fig. 8e). Amongst the NWP-WFP simulations, case TKE000
403 displays the fastest near-farm wake ~~recovers more quickly than in the coarser-resolution cases, as evident in both the wind~~
404 ~~speed (Fig. recovery rate because of the largest wind speed deficit~~. Subtracting the wind speed change of the two LES with the
405 NWP-WFP cases, a difference of $0.15-0.60 \text{ m s}^{-1}$ is found. These values represent the bias in wind speed associated with the
406 slower near-farm wake recovery in the NWP-WFP simulations.

407 None of the NWP-WFP simulations matches the wind speed of the LES in the far wake (Figs. 7a and 8a) ~~and the streamwise~~
408 ~~gradients in wind speed (Fig.~~, but the wake recovery rates agree very well (Figs. 7d and 8d). The bias in wind speed decreases
409 in the far wake for cases with strong deficit, such as BASE and TKE000. However, the bias remains mostly unchanged for cases
410 with weaker deficit at the farm exit, such as TKE100, ~~which now reproduce the peak displayed by the LES~~. Finally, ~~adding~~
411 ~~more TKE DX2D and DX2DTKE100~~. Overall, regardless of the TKE coefficient, all the mesoscale simulations display a
412 consistent negative wind speed bias ranging from approximately -0.7 m s^{-1} (TKE000) to -1.3 m s^{-1} ($\alpha = 100\%$ TKE100)
413 ~~in the high-resolution simulation further improves wake generation and recovery, yielding the best agreement with near-farm~~
414 wake at $X = 15$ km. The bias decreases to approximately -0.6 m s^{-1} in the far wake ($X = 50$ km) for all cases (Fig. 7a)
415 compared to the LES.

416 In the LES, TKE builds up gradually, row by row, whereas in the NWP-WFP cases with a TKE source ($\alpha > 0$), the TKE
417 peaks near the first few turbine rows and then decreases monotonically downstream (Fig. 7c). The TKE remains nearly constant
418 within the farm in case BASE, and is small throughout in case TKE000, which lacks an explicit TKE source. Interestingly,
419 cases with α of 25% and 50% better match the TKE levels near the first turbine rows, consistent with results from Archer
420 et al. (2020), while those with higher α (75%, 100%) better match the TKE in the latter half of the farm, in line with other
421 findings (Larsén and Fischereit, 2021; Ali et al., 2023). This variability in the literature seems to stem in part from where the
422 comparison is made: within, near or further downstream of the wind farm, as shown here.

423 A key insight is that turbine-added TKE ~~cannot accumulate properly does not evolve properly within the wind farm~~ in the
424 NWP-WFP simulations, even if when its magnitude matches or exceeds that of the LES in the first few ~~rows of turbines~~ turbine
425 rows. The root problem therefore lies not only in the amount of turbine-added TKE, ~~but in its rapid decay~~. A large TKE

dissipation rate in the NWP simulations appears to inhibit the streamwise accumulation of turbine-added TKE that is evident in the LES. Supporting this interpretation, the much faster decay of turbine-added TKE as a gradual reduction of intra-farm TKE persists across several cases (TKE050–TKE100). Moreover, TKE decreases more rapidly than in the LES in the NWP-WFP simulations in the near-farm wake (Fig. 7c), compared to the LES, provides a clear signal of what initially appears to be exaggerated TKE dissipation. However, in. While this behavior in the NWP-WFP simulations could in principle be attributed to excessive dissipation, Section 4.1.2 this interpretation is revisited in light of additional evidence suggesting other mechanisms may play a provides additional evidence that insufficient shear production of TKE, rather than dissipation, plays the dominant role.

Lastly, the underestimation of the subtle anti-clockwise turning of the wake depends on turbulent mixing (Fig. 7b). For the wake turning, this behavior results from downward turbulent momentum entrainment, which transports more veered wind from aloft into the wake (van der Laan and Sørensen, 2017; Gadde and Stevens, 2019; Englberger et al., 2020; Stieren et al., 2022; Kasper et al., 2024). Accordingly, cases with weaker entrainment, such as TKE000 and BASE, show a stronger directional bias. Although the absolute differences in wind direction are small (about 1° between TKE000 and TKE100), over long distances these differences may accumulate into downstream power losses for adjacent wind farms.

3.5 Under-resolved spatial gradients in the NWP-WFP simulation wake

In this section, we examine spatial gradients in the wind farm wake as represented by the aligned LES at full resolution and when spatially averaged to match the grid resolution of the BASE case. We also compare the LES results with the NWP-WFP cases BASE and TKE100. The goal is to evaluate how the realistic spatial gradients of the LES influence wake recovery, and how the horizontal and vertical gradients of the latter compare with the NWP-WFP simulations. Figures 9 and 10 intentionally focus on localized profiles at specific turbine-aligned grid cells to highlight differences in resolved gradients between the NWP-WFP simulations and the LES. While spanwise averaging would yield different absolute TKE levels, such averaging would obscure the local shear and turbulence structures that directly control wake recovery in the near-farm region. These figures are therefore not intended to represent farm-averaged behavior, but rather to diagnose the structural deficiencies of mesoscale simulations at the grid-cell scale.

The difference-discrepancy between the coarsened aligned LES and the BASE and TKE100 profiles of wind speed grows in the streamwise distance wind speed profiles increases with downstream distance. The stronger momentum extraction in the staggered LES, relative to the aligned LES, results in improved agreement with the BASE and TKE100 cases. Figure 9 shows hub-height profiles of wind speed (Figs. 9a–e) and TKE (Figs. 9f–j) along the spanwise (Y) direction at selected streamwise distances: the wind farm entrance ($X = 0$ km), middle ($X = 5$ km), near-exit ($X = 10$ – 11.2 km), and two downstream locations ($X = 15$ and 20 km). At the entrance ($X = 0$ km), the spatially averaged LES gradients in wind speed (both coarsened LES) agree reasonably well with both NWP-WFP cases (Figs. 9a). However, deviations become noticeable at $X = 5$ km (Figs. 9b), especially for the between the coarsened aligned LES and the BASE case, and grow progressively larger through $X = 10$ – 11.2 and 15 km (Figs. 9c and d). At $X = 20$ km (Figs. 9e), the discrepancy remains large. The narrow band of reduced wind speed

459 and increased TKE near the center of the wind farm in the Y direction is created by the existence of two turbines within that
 460 grid cell (Fig. 2b), as discussed in Section 3.3.

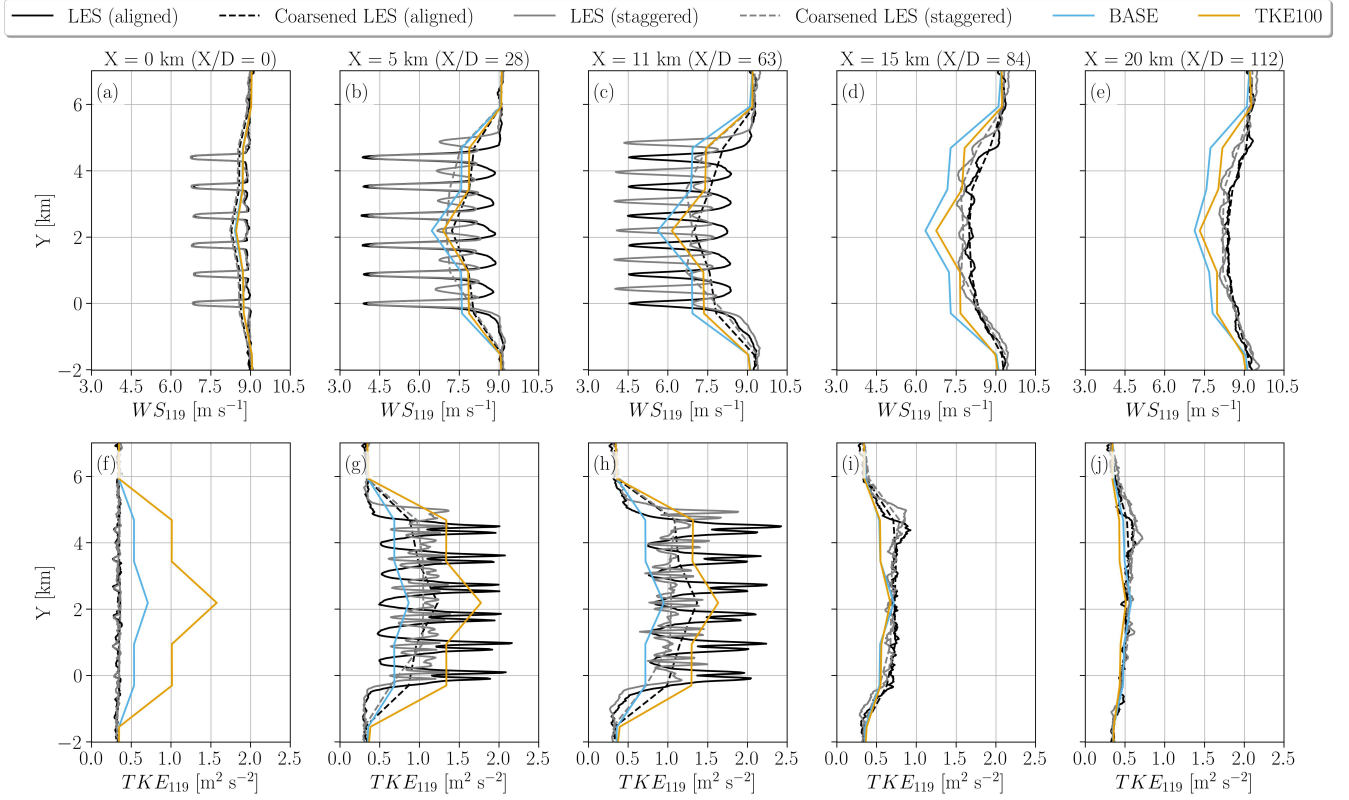


Figure 9. Time-averaged wind speed (a–e) and TKE (f–j) at hub height (119 m AGL) along spanwise Y lines at specific streamwise distances X (expressed as X/D in parentheses) for the aligned and staggered layout LES, coarsened LES, and NWP-WFP BASE and TKE100 cases.

461 From the standpoint of spatial wind speed gradients, differences between ~~the both the aligned and staggered layout~~ LES and
 462 the NWP-WFP cases are striking. While the coarsened LES profile appears similar to those of the NWP-WFP cases within the
 463 wind farm ($0 \leq X \leq 10.112$ km, $0 \leq X/D \leq 5663$), this ~~resemblance is misleading and fails to represent important physical~~
 464 ~~processes. The full-resolution LES wind speed profiles feature sharp gradients that resemble spikes~~ similarity hides strong
 465 localized gradients in the wakes that only appear in the non-averaged LES (Figs. 9a–c). These strong ~~local gradients~~ localized
 466 gradients are expected with a fine-resolution grid and facilitate faster wake recovery in the LES. Notably, model discrepancies in
 467 wind speed profiles grow with streamwise distance while these ~~spiky strong localized~~ gradients persist ($0 \leq X \leq 10.112$ km,
 468 $0 \leq X/D \leq 5663$), but no longer increase between $X = 15$ and 20 km ($X/D = 84$ and 112 , respectively), where the LES
 469 gradients become smoother and more comparable to those in the NWP-WFP cases.

470 This behavior suggests that the fundamental problem lies upstream, within the intra-farm and near-farm wake regions. Once
 471 the ~~spikiness disappears in the strong localized gradients in the wakes~~ disappear in the LES, the differences between models

472 stabilize. Therefore, the persistent lower wind speeds in NWP-WFP simulations in the far wake of the farm (Figs. 9d,e) are
 473 not caused by conditions there, but rather reflect limitations in representing spatial gradients and turbulent mixing within the
 474 intra-farm and near-farm wake regions. As conceptually illustrated in the Introduction, the slow wake recovery (Figs. 1b,c) and
 475 ~~rapid-TKE-decay~~ TKE decrease (Figs. 1e,f) are evident in the results shown in Figs. 9c,d and h,i, respectively.

476 Vertical profiles reveal how wind farm effects modify wind speed (Figs. 10a–f) and TKE (Figs. 10g–l) gradients in each
 477 simulation. Vertical profiles are sampled along the southernmost turbine column (near $Y = 0$ km) at selected streamwise
 478 locations to examine how each simulation resolves local vertical gradients. The data are not spatially averaged, allowing direct
 479 assessment of the gradients resolved by each grid. Upstream of the farm, wind speed (Fig. 10a) and TKE (Fig. 10g) profiles
 480 are nearly identical across simulations. Within and downstream of the farm, momentum extraction (Figs. 10b–d) and TKE
 481 production (Figs. 10h–j) alter these profiles. In the LES, the stronger wind speed deficit enhances vertical shear, especially near
 482 the rotor top tip, by $X/D = 28$ (Figs. 10b–d), leading to intense TKE generation in the same region (Figs. 10i–j). Combined,
 483 the stronger vertical wind speed gradient and enhanced TKE in the LES contribute to a faster intra-farm and near-farm wake
 484 recovery.

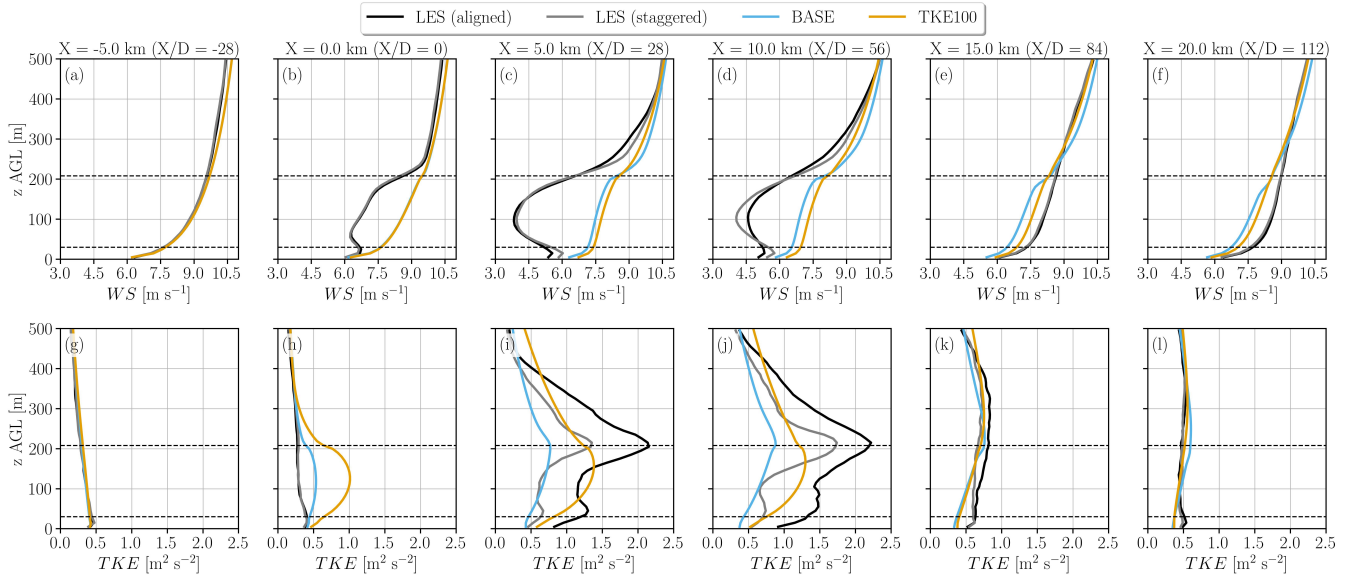


Figure 10. Vertical profiles of time-averaged wind speed (a–f) and TKE (g–l) at specific streamwise distances X (expressed as X/D in parentheses) probed over the southernmost column of turbines near $Y = 0$ km. The aligned and staggered layout LES at full-resolution without spatial averaging and NWP-WFP cases BASE and TKE100 are shown. The dashed horizontal lines represent the rotor top and bottom tips.

485 Despite the fine vertical resolution, NWP-WFP simulations fail to capture strong vertical gradients due to coarse horizontal
 486 resolution. Although the NWP-WFP simulations use the same vertical resolution as the LES ($\Delta z \sim 10$ m), they locally under-
 487 resolve vertical wind speed gradients (Figs. 10b–d). ~~The LES shows~~ Both the LES show a much sharper local wind speed deficit

(Figs. 10b–d), while in the NWP-WFP simulations the deficit is diluted due to spatial averaging over the coarser horizontal grid ($\Delta X \sim 1$ km). This horizontal averaging dilutes the momentum sink effect, weakening both horizontal and vertical gradients. As a result, even with sufficient vertical resolution, the vertical structure of the wake is poorly captured in the NWP-WFP simulations due to the coupling between horizontal and vertical gradients.

Further evidence of the critical role of under-resolved gradients in intra-farm and near-farm wake recovery emerges when evaluating the effect of TKE. From a turbulent mixing perspective, increased TKE accelerates wake recovery: for instance, the TKE100 case displays faster recovery than the BASE case, as also shown by Rosencrans et al. (2024). However, despite exhibiting more TKE than both the coarsened LES throughout much of the wind farm ($0 \leq X \leq 11.2$ km), including earlier onset of added TKE (Fig. 9f), the TKE100 wake still recovers slower than that of the LES. These findings highlight that enhanced farm-added TKE alone is insufficient to compensate for the under-resolved gradients.

4 Discussion

4.1 What are the fundamental problems?

The preceding results identify two interconnected sources of modeling bias: (i) under-resolved spatial gradients in turbine wakes and (ii) ~~rapid-decay-of-farm-added-TKE-low TKE behind wind farms~~ in NWP-WFP simulations. *Under-resolved*, ~~not~~ rather than unresolved, is ~~the appropriate term~~, appropriate since the mesoscale grid partially captures the turbine-induced wind speed gradients, but lacks sufficient fidelity. These two issues affect the physics of wake recovery, which is governed by two interrelated mechanisms:

- (a) the magnitude of turbulent mixing, and
- (b) the strength of spatial gradients in the mean wind velocity field.

The recovery of momentum in wind turbine and near-farm wakes occurs through lateral and vertical turbulent entrainment of momentum, expressed as divergences of $\overline{u'v'}$ and $\overline{u'w'}$, respectively (Vermeer et al., 2003; Cal et al., 2010; Calaf et al., 2010; Abkar and Porté-Agel, 2015; Porté-Agel et al., 2020; Stieren and Stevens, 2022; van der Laan et al., 2023). Here, u' , v' , and w' denote fluctuations relative to the time-averaged wind velocity components U , V , and W in the streamwise, spanwise, and vertical directions, respectively. These momentum fluxes are commonly approximated using the Boussinesq hypothesis (Boussinesq, 1897; van der Laan et al., 2023) or equivalently the K-theory (Stull, 1988):

$$\overline{u'v'} = K_m \frac{\partial U}{\partial y} \quad (1)$$

$$\overline{u'w'} = K_m \frac{\partial U}{\partial z}. \quad (2)$$

Here, K_m is the eddy viscosity, which depends on turbulence and atmospheric stability (Stull, 1988), and $\frac{\partial U}{\partial y}$ and $\frac{\partial U}{\partial z}$ are the spanwise and vertical gradients of wind speed (for convenience, we assume the mean flow aligns with the x -direction). The eddy viscosity K_m increases with TKE, and therefore wakes tend to recover more rapidly under convective conditions compared to neutral or stable conditions (Magnusson and Smedman, 1994; Jungo et al., 2013; Fitch et al., 2013a; Mirocha et al., 2015; Abkar and Porté-Agel, 2015; Stevens and Meneveau, 2017; Bodini et al., 2017; Lundquist et al., 2019; Rosencrans et al., 2024; García-Santiago et al., 2024). The two modeling biases identified above directly impact these physical mechanisms of wake recovery:

- (i) Under-resolved spatial gradients: weaken the mean shear in the wake, thereby reducing the turbulent fluxes [affecting factor (b)]. Even if TKE is present, the lack of strong horizontal and vertical gradients limits momentum transport into the wake.
- (ii) ~~Rapid-decay-of-farm-added-Low~~ TKE: reduces the eddy viscosity K_m , which diminishes the efficiency of turbulent mixing [affecting factor (a)]. As a result, the momentum recovery by turbulence is suppressed, even in regions where spatial gradients are better resolved.

In the following subsections, we examine each of these two problems in more detail. We begin with the role of under-resolved wind speed gradients and their consequences for wake recovery, followed by the impact of ~~rapid-TKE-decay-artificially low~~ TKE in the farm region.

4.1.1 Under-resolved wind speed gradients

The first and perhaps most critical problem is that NWP-WFP simulations cannot accurately represent the spatial wind speed gradients that drive intra-farm and near-farm wake recovery. Many studies have shown that WFPs can reproduce wind speed deficits at turbine grid cells that generally resemble those from LES (Vanderwende et al., 2016; Abkar and Porté-Agel, 2015; Archer et al., 2020; Peña et al., 2022; García-Santiago et al., 2024). However, a closer look at the downstream regions reveals a slower wake recovery in NWP-WFP simulations compared to LES (e.g., Figs. 4a,c in Vanderwende et al. (2016); Fig. 7 in Archer et al. (2020); Figs. 11–13 in Peña et al. (2022); Figs. 4 and 7 in García-Santiago et al. (2024)). Here, we demonstrate that this discrepancy arises because the momentum sink term in WFPs is not resolved by the grid, and thus is not severely affected by its coarseness, whereas the wake recovery is fundamentally resolved by the grid. Specifically, the NWP-WFP simulations exhibit inherently weaker horizontal (Figs. 9a–c) and vertical (Figs. 10b–d) gradients in the wind velocity field within the intra-farm and near-farm wake regions, i.e. $\frac{\partial U}{\partial y}|_{\text{NWP-WFP}} < \frac{\partial U}{\partial y}|_{\text{LES}}$ and $\frac{\partial U}{\partial z}|_{\text{NWP-WFP}} < \frac{\partial U}{\partial z}|_{\text{LES}}$, respectively. While discrete velocity differences evaluated at WRF grid resolution can locally yield gradients comparable to or even exceeding those in a coarsened LES (Fig. 9d), they do not organize into shear structures comparable to those present in the native-resolution LES. In contrast, the LES at native resolution exhibits spatially coherent and persistent shear layers that extend downstream and continuously drive turbulence production and wake recovery, a structural feature that is not maintained in the mesoscale representation.

547 As a result, even when farm-added TKE levels are comparable to or exceed those in the LES, the intra-farm and near-farm
548 wake recovery (driven by the weaker gradients) remains underestimated in the NWP-WFP simulations (Sections 3.4 and 3.5).
549 The fact that simulations with the finest grid resolution (DX2D and DX2DTKE100), which better resolve spatial gradients,
550 improve the representation of the near-farm wake recovery (Figs. 8a,d) supports this argument. Under-resolved gradients have
551 also been noticed by others (Fischereit et al., 2022b). Related, in another study using WRF and the Fitch WFP (Pryor et al.,
552 2020), shorter wind farm wakes result from finer grid resolutions, which could in part be explained by the impact of the
553 under-resolved gradients on wake recovery.

554 4.1.2 ~~Rapid decay of farm-added~~ Insufficient shear production causes low TKE

555 The second problem is the relatively fast ~~decay~~ decrease of farm-added TKE in the NWP-WFP simulations compared to the
556 LES. This ~~rapid decay~~ comparatively low TKE in the near-farm wake reduces turbulent mixing, effectively lowering the eddy
557 viscosity K_m , and further slowing wake recovery. Even when large amounts of turbine-added TKE are injected (e.g., $\alpha = 75\%$
558 or 100%), the TKE fails to accumulate row-by-row as it does in the LES (Fig. 7c). Across all tested TKE enhancement levels
559 ($\alpha = 25\%–100\%$), the NWP-WFP TKE ~~decays~~ returns to near-ambient levels within 5 km downstream, almost twice as fast
560 as in the LES.

561 A compelling hypothesis is that ~~this rapid decay~~ the rapid reduction of TKE is not merely a dissipation artifact ~~but rather~~, but
562 instead a consequence of ~~the first problem—the~~ under-resolved gradients. ~~The first evidence for this hypothesis is the excellent~~
563 This interpretation is supported by the close agreement between NWP-WFP and LES TKE levels in the inflow ~~profiles~~ (Fig. 3d)
564 and in the far wake (Fig. 7c), indicating that the mesoscale model does not inherently over-dissipate TKE. ~~Instead, the issue~~
565 ~~may lie~~ Rather, the limitation emerges in the intra- and near-farm wake ~~regions~~, where TKE ~~fails to persist because the shear~~
566 ~~production of TKE is insufficiently generated because shear production~~ depends on spatial gradients (Mellor and Yamada,
567 1982; Nakanishi and Niino, 2009) ~~, which that~~ are under-resolved ~~. For instance, the TKE levels are enhanced in regions of~~
568 ~~strong wind shear due to shear production of TKE. If the wind speed and direction became homogeneous (zero wind shear),~~
569 ~~the TKE profile as in Fig. 3d would decay. Therefore, an explicit source of TKE without sufficient gradients to maintain it~~
570 ~~becomes unsustainable and decays (Fig. ??). This distinction highlights a key limitation: while the NWP-WFP approach~~
571 ~~can represent background ABL turbulence reasonably well, it fails to represent the strong turbulence generated at mesoscale~~
572 resolution. The coupling between TKE, shear production, and dissipation is illustrated in Appendix B. While this limitation
573 can be partially offset within the wind farm ~~itself. The mechanism for the rapid decay of TKE is relevant for any studies that~~
574 ~~employ the~~ through turbine-added TKE, it becomes evident downstream, where the WFP is inactive and TKE levels fall below
575 those of the LES. This mechanism is therefore intrinsic to NWP-WFP ~~approach, especially those that propose modifications to~~
576 ~~the frameworks and has implications for studies that focus on modifying~~ turbine-added TKE ~~source formulations~~ (Fitch et al.,
577 2012; Archer et al., 2020; Khanjari et al., 2025).

578 4.2 Implications

579 Because both problems – slow wake recovery and ~~fast TKE decay~~ insufficient shear production of TKE – are fundamentally
580 linked to grid resolution, they are likely to affect wake recovery not only in WRF with the Fitch ~~WFP~~ or MAV WFPs but also
581 in other NWP and climate models that use WFPs. As such, these findings underscore the need for improved representation
582 of both spatial gradients and turbulent mixing if WFPs are to accurately simulate wind farm wakes and their downstream
583 impacts. Building on this, we present implications of our work for studies of real wind farm wake effects, where environmental
584 and observational aspects increase the complexity of the analysis. We highlight the importance of separating wake generation
585 (momentum extraction) from its recovery when evaluating model performance.

586 Some NWP-WFP simulations driven by realistic synoptic conditions have demonstrated reasonable agreement with observed
587 wind speed deficits in wind farm wakes, based on aircraft measurements (~~Siedersleben et al., 2018a, b, 2020; Larsén and Fischereit, 2021; A~~
588 Siedersleben et al., 2018a, b, 2020; Larsén and Fischereit, 2021; Ali et al., 2023; van Stratum et al., 2022) and SCADA data (Sanchez
589 Gomez et al., 2024) from offshore sites. However, discrepancies in inflow conditions between simulations and observations
590 remain a major challenge, as they can obscure the evaluation of wake recovery. Despite this, several case studies have achieved
591 good correspondence with observed wind speed profiles along wind farm transects. Given the inherent spatio-temporal vari-
592 ability and limited control over inflow in realistic configurations, such results are promising. In contrast, our idealized setup
593 ensures excellent agreement in the inflow, allowing a more direct assessment of WFP performance and limitations. These
594 controlled conditions provide valuable guidance for improving their representation in more complex, operational scenarios.

595 Another important issue is the separation between wake generation and recovery for modeling evaluation. The wind speed
596 bias between the NWP-WFP simulation and the LES within the wind farm is not exclusively caused by a difference in wake
597 recovery, but also by a difference in momentum extraction. For instance, in Fig. 4b, the coarser-resolution cases BASE and
598 DX5D have larger row-averaged power (extract more momentum) than the finer-resolution cases DX2D and DX2DTKE100.
599 As a result, in combination with differences in wake recovery between the simulations, cases BASE and DX5D have stronger
600 wind speed deficits (Fig. 8a). Matching the wind speed deficit predicted by LES or observations does not necessarily mean the
601 dynamics of wake recovery are well represented in NWP-WFP simulations. For instance, a seemingly faster wake recovery
602 was attributed to the NWP-WFP simulation in comparison with the LES, when in fact the NWP-WFP simulation generated a
603 much weaker wake in the first place (Eriksson et al., 2015). As the stronger wake of the LES recovers momentum, it eventually
604 matches the wind speed deficit of the weaker wake of the NWP-WFP simulation downstream. Thus, wake generation and
605 recovery are two important aspects of wind farm flows that need to be considered simultaneously.

606 The degree of wake recovery underestimation is likely sensitive to inflow wind speed, direction and atmospheric stability.
607 For instance, the weaker ambient turbulence in stable conditions promotes longer individual turbine wakes (and thus stronger
608 spatial gradients in wind speed) in comparison with neutral or convective conditions (Abkar and Porté-Agel, 2015; Abkar et al.,
609 2016b). Hypothetically, these unmixed wind speed gradients could further slow wake recovery in NWP-WFP simulations,
610 which requires more research. Evaluating wake recovery in stable conditions is important because it is exactly when wakes are

most pronounced (Magnusson and Smedman, 1994; Iungo et al., 2013; Fitch et al., 2013a; Mirocha et al., 2015; Abkar and Porté-Agel, 2015; Bodini et al., 2017; Lundquist et al., 2019; Rosencrans et al., 2024; García-Santiago et al., 2024).

5 Conclusions

Numerical Weather Prediction (NWP) and climate models equipped with Wind Farm Parameterizations (WFPs) provide a powerful framework for simulating wind farm cluster wakes, both onshore and offshore. Their ability to capture physical processes across a wide range of spatiotemporal scales enables studies of atmosphere–wind farm interactions under realistic conditions and over large computational domains. In this paper, we assess the strengths and limitations of the NWP-WFP approach using the Weather Research and Forecasting (WRF) model with the ~~Fitch-WFP~~ Fitch et al. (2012) and MAV (Ma et al., 2022b, a) WFPs, in comparison to the neutrally-stratified large-eddy simulation (LES) of Kasper et al. (2024). We find that near-farm wake recovery is slower in the NWP-WFP simulations relative to the LES for two interconnected reasons: (i) under-resolved spatial gradients in the wind velocity field and (ii) ~~overly-rapid-decay-of-wind-turbine-added-insufficient~~ shear production of turbulence kinetic energy (TKE).

The first issue stems from the fact that in the LES, near-farm wake recovery is driven by sharp local velocity gradients and enhanced turbulent mixing that replenishes momentum in the wake. In contrast, while the NWP-WFP momentum deficit at the turbine grid cell is *unresolved* by the grid, its downstream recovery depends on grid-resolved gradients. However, these horizontal and vertical gradients in wind speed in the intra- and near-farm wake are *under-resolved* at the mesoscale grid spacing used in NWP-WFP, leading to underestimated wake recovery. ~~In coarser-resolution simulations,~~

~~In the spanwise-averaged wind speed bias in the near-farm wake reaches approximately 1.0~~ wake, differences in wind speed recovery between the NWP-WFP simulations and the LES emerge over a short downstream distance ($\sim 1\text{--}2\text{km}$) but lead to measurable wind speed biases. Between the wind-farm exit at 11.2 km and 15 km downstream, the LES recovers approximately $0.65\text{--}0.8\text{ m s}^{-1}$, and about 0.6 m whereas the coarser-resolution NWP-WFP simulations recovers only $0.2\text{--}0.5\text{ s}^{-1}$ in the far wake, relative to the LES. Finer-resolution cases reduce these biases to around 0.3 to 0.5 , yielding a wind speed bias of about $0.15\text{--}0.60\text{ m s}^{-1}$ in the near-farm wake and approximately 0.4 m in the far wake, but differences relative to the LES remain. Despite similarly fine vertical grid spacing ~~between the NWP-WFP and LES~~, horizontal smearing of the momentum deficit in the NWP-WFP ~~also results in underestimated vertical wind speed simulations~~ leads to under-represented horizontal and vertical gradients. Even simulations with increased turbine-added TKE ~~could not~~ cannot fully compensate for these limitations, indicating that under-resolved gradients. Thus, under-resolved gradients in both horizontal and vertical directions limit wake recovery constrain wake recovery behind the wind farm.

The second issue involves the ~~decay of wind turbine-added~~ insufficient shear production of TKE. In the LES, TKE ~~accumulates~~ increases progressively along the wind farm rows, peaking near the wind farm exit. In the NWP-WFP simulations, however, the maximum occurs within the first few rows and then decreases monotonically along the streamwise direction ~~because the TKE cannot be maintained. This rapid TKE decay continues in the~~. Most importantly, the TKE decreases faster than in the LES

644 in the near-farm wake region (within 54 km downstream), likely due to the same ~~under-resolved gradients~~insufficient shear
645 production. The inflow profiles have similar shear and veer characteristics across simulations, which initially produce compa-
646 rable TKE levels. However, the insufficient magnitude of spatial gradients in the intra- and near-farm wake in the NWP-WFP
647 ~~renders the turbine-added TKE unsustainable~~undermines the local shear production of TKE. As a result, the TKE ~~decays~~returns
648 to ambient levels much faster than in the LES and further undermines wake recovery in these neutrally-stratified simulations.

649 A key insight is that the slow recovery in the near-farm wake, although confined to a short downstream distance, has lasting
650 consequences for the far wake region. In coarse-resolution simulations, the far wake wind speed bias remains substantial even
651 when large amounts of turbine-added TKE are introduced. However, when near-farm wake recovery improves through finer
652 grid resolution and better-resolved gradients, the far wake bias is also reduced. ~~This highlights the importance of accurately~~
653 ~~representing wake recovery not only near the farm, but also as a prerequisite for improving conditions further~~ Thus, accurately
654 representing near-farm wake recovery is also essential for reducing modeling biases in the far wake downstream.

655 Because these two findings stem from the relatively coarse mesoscale grid, they are relevant to other NWP and climate
656 modeling frameworks that employ any form of WFP. ~~Beyond~~ We note that the slower wake recovery compared with the
657 LES arises from the coarse representation of wake recovery processes at the mesoscale, rather than from deficiencies in the
658 WFPs themselves. This slower wake recovery occurs predominantly in the near-farm wake, a region that lies outside the direct
659 influence of the WFPs and is therefore governed by grid-resolved dynamics and planetary boundary layer (PBL) schemes.
660 Naturally, the WFPs exert influence on wake recovery since they affect wind speed and TKE at the wind farm exit. Therefore,
661 beyond improving the subgrid parameterizations of momentum sinks and TKE sources, it is equally important to develop new
662 strategies that account for the effects of under-resolved gradients~~in NWP-WFP frameworks~~, especially in the near-farm wake.
663 These efforts should produce spatial variations of TKE and wake recovery rates more consistent with LES. A potential pathway
664 forward is the development of a subgrid model that accounts for the missing spatial gradients driving wake recovery. Such a
665 model would act over grid cells downstream of the wind farm in the near-farm wake and be evaluated against LES, potentially
666 using empirical tuning. Otherwise, the underestimation of wake recovery may lead to overestimated wake losses.

667 Future work could: (i) propose methods to address the problem of under-resolved gradients ~~, and~~ (ii) ~~investigate the differences~~
668 ~~between NWP-WFP and LES under aligned and staggered turbine layouts, and (iii)~~ assess wake recovery under varying atmo-
669 spheric stability regimes. Another possible direction is to (iv) ~~investigate~~ whether different planetary boundary layer (PBL)
670 schemes can improve turbulent mixing and thus wake recovery, such as the 3DPBL scheme (Kosović et al., 2020; Juliano et al.,
671 2022). Regarding (iii), we note that the velocity gradients in the LES become smoother and more mesoscale-resolvable be-
672 yond approximately 5 km downstream. Under such conditions, NWP-WFP simulations may better reproduce the reference LES
673 recovery. Following this rationale, convective boundary layers, by mixing sharp gradients more efficiently, may allow NWP-
674 WFP to more accurately capture wake recovery than is possible under neutral or stable conditions. Therefore, understanding
675 the role of atmospheric stability on wake recovery is also necessary for improving the accuracy of NWP-WFP approaches.

676 *Code and data availability.* The WRF model version 4.4 with the axial induction correction (Vollmer et al., 2024) and the MAV WFP (Ma
677 et al., 2022b, a) is available at https://github.com/wradunz/WRFv4.4-DRM_GAD.git. The WRF setup files for the NWP-WFP simulations
678 can be accessed at Radünz (2025).

679 Appendix A: DTU 10-MW turbine power and thrust curves

680 This section evaluates the sensitivity of wake recovery to the thrust coefficient (C_T), as outlined in Table 1. The power and
681 thrust coefficient curves for the DTU 10-MW wind turbine are shown in Figs. A1a,b, respectively. For an inflow wind speed of
682 approximately 9 m s^{-1} , the turbine produces slightly over 5 MW of power, and the corresponding C_T is approximately 0.81.

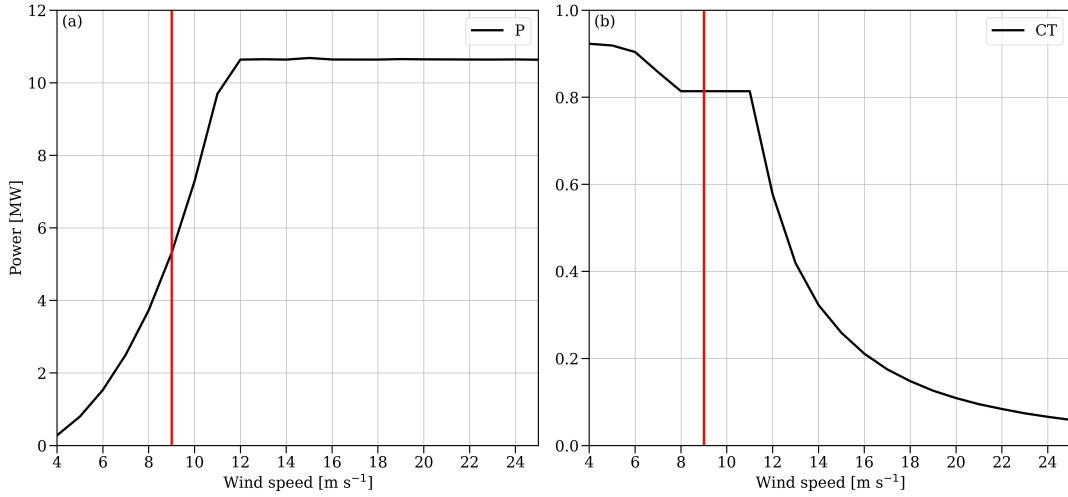


Figure A1. Power (a) and thrust coefficient (b) curves as function of wind speed for the wind turbine of the DTU 10-MW model. The red vertical line denotes the point of operation based on the hub height wind speed of approximately 9 m s^{-1} considered in this study.

683 The value of $C_T = 0.75$ adopted in the LES (Section 2.1) yields wind speed deficits similar to those obtained with a fixed
684 C_T of 0.81 or with a wind-speed-dependent C_T (Fig. A2a). In contrast, using a lower C_T value of 0.50 results in a weaker
685 wake and reduced TKE generation (Fig. A2c), since the TKE source term is proportional to the difference $C_T - C_P$. Therefore,
686 whether C_T is set to 0.81, 0.75, or dynamically determined based on wind speed, the main conclusions of our investigation
687 remain unchanged.

688 Appendix B: Streamwise TKE budget in NWP-WFP simulations

689 To support the interpretation presented in Section 4.1, we examine the streamwise evolution of selected MYNN TKE budget
690 terms at hub height for the mesoscale NWP-WFP simulations (BASE, TKE100, and MAV), shown in Fig. B1. The budget
691 terms are computed using the same spanwise averaging applied in Figs. 7 and 8, ensuring consistency with the bulk wake

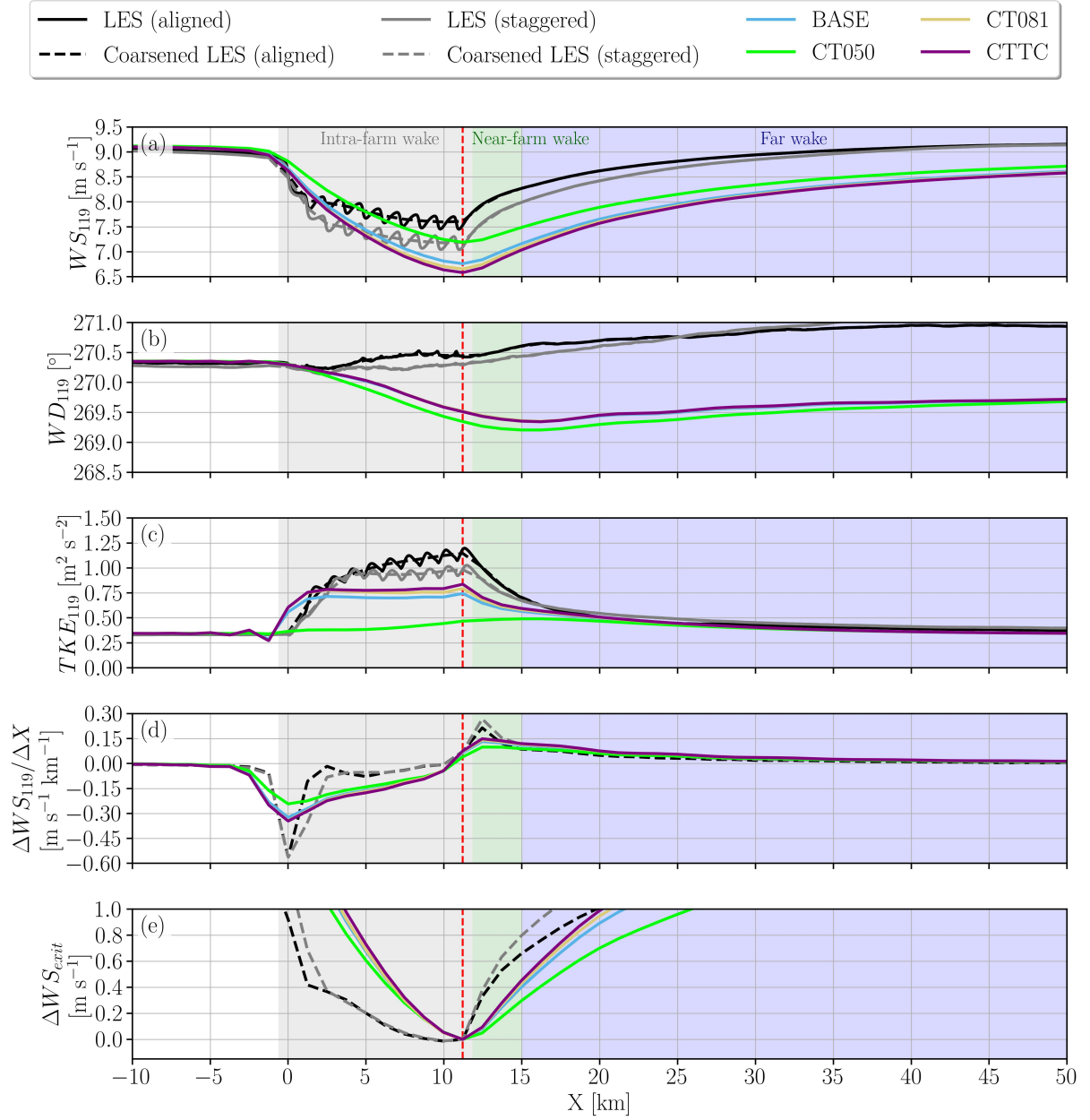


Figure A2. Streamwise variation of spanwise averages over the wind farm area of hub-height wind speed (a), [wind](#) direction (b), TKE (c), [and](#) streamwise gradient of wind speed (d) [and wind speed change relative to the wind farm exit \(e\)](#) for the [aligned and staggered](#) LES at full resolution, coarsened LES, and NWP-WFP cases with different C_T . In the CTTC case, the thrust coefficient C_T varies with wind speed according to the turbine's thrust curve. The colored background areas indicate the streamwise extent of the intra-farm wake (gray), near-farm wake (green), and far wake of the farm (blue). [The red vertical dashed line marks the wind farm exit.](#)

692 diagnostics used to characterize intra-farm, near-farm, and far-wake behavior. Buoyancy production and vertical transport are
693 omitted, as their contributions are small relative to the dominant terms and do not influence the conclusions discussed below.

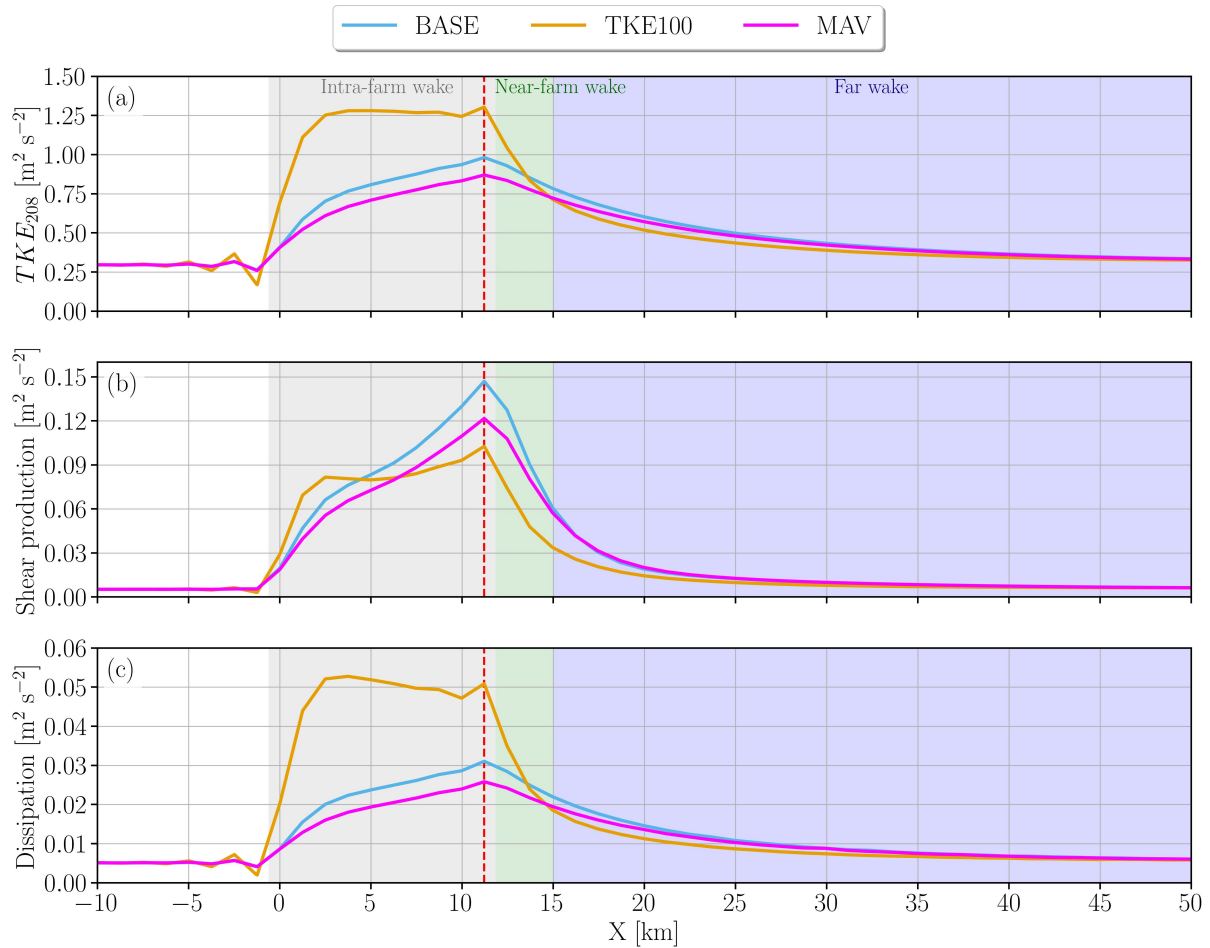


Figure B1. Streamwise variation of spanwise averages over the wind farm area of rotor top tip TKE (a), shear production (b), and dissipation (c) for the BASE, TKE100 and MAV cases. The colored background areas indicate the streamwise extent of the intra-farm wake (gray), near-farm wake (green), and far wake of the farm (blue). The red vertical dashed line marks the wind farm exit.

694 Figure B1a shows that the TKE is highest within the wind farm due to direct addition by the WFPs, with dissipation
695 (Fig. B1c) closely following the TKE magnitude. Shear production (Fig. B1b) increases through the intra-farm region as the
696 wind speed deficit builds across successive turbine rows (Fig. 7a). In the near-farm wake, where the WFPs are inactive, shear
697 production in the BASE and MAV cases exceeds that of the TKE100 case, despite similar TKE and dissipation levels at the
698 wind-farm exit. This difference is critical: the reduced shear production in TKE100 leads to a reduced TKE in the near-farm
699 wake compared to BASE and MAV. Consistently, cases with larger wind speed deficits exhibit stronger shear production,
700 with the ordering at the farm exit being BASE, followed by MAV and TKE100. These results reinforce the conclusion

701 from Section 4.1 that insufficiently sustained shear production limits TKE levels and eddy viscosity in the near-farm wake
702 of mesoscale NWP-WFP simulations.

703 *Author contributions.* Conceptualization: WCR and JKL. Methodology: WCR. Data curation: WCR and JHK. Formal analysis: WCR. In-
704 vestigation: WCR and JKL. Writing (original draft): WCR and JKL. Writing (review and editing): all authors. All authors contributed to the
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