

Wind turbine wake dynamics subjected to atmospheric gravity waves: A measurement-driven large-eddy simulation study

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Abstract. Atmospheric gravity waves (AGWs) are large-scale wave-like flow structures commonly generated when atmospheric flows are vertically perturbed by topographical features or meteorological phenomena. These transient phenomena can significantly affect wind turbine outputs and loads; however, their influence on wake dynamics remains poorly understood, posing challenges for accurate wind farm modeling. In this study, we perform large-eddy simulation of wind turbines operating under an atmospheric condition reconstructed by assimilating lidar measurements of AGWs. Our results show that: (i) Low-frequency wake meandering becomes more pronounced owing to large-scale AGW flow structures and intensified smaller-scale turbulent structures. This enhanced meandering, combined with stronger turbulent mixing, accelerates mean wake recovery. (ii) Turbulence kinetic energy (TKE) spectrum in the wake region exhibits a peak Strouhal number of approximately 0.3, although the inflow spectrum peaks at significantly lower frequencies. This observation indicates that, under AGW conditions, wake turbulence generation follows a convective instability mechanism. Notably, faster wake recovery reduces wake shear, leading to lower amplification of TKE. Power analysis for three turbines arranged in a streamwise column further highlights the dominant role of convective instabilities. Large-amplitude, low-frequency power fluctuations observed at the most upstream turbine are significantly attenuated for downstream turbines, as low-frequency velocity fluctuations shift to higher frequencies in the far-wake regions. These findings add further insights into wake meandering and turbulence generation, offering guidance for modeling wind turbine and farm flows under non-stationary atmospheric conditions.

1 Introduction

Atmospheric gravity waves (AGWs) commonly occur when the atmosphere is vertically displaced by topographical features, such as mountains and coastlines ([Nappo, 2012](#)), [or meteorological phenomena, such as fronts and thunderstorms \(Stull, 1988; Nappo, 2012\)](#). These waves are trapped by the stable capping inversion layer aloft and propagate horizontally within the lowest 1-5 km of the troposphere (Durrán, 2003). This transient phenomenon can cause fluctuations in wind speed experienced by wind farms, resulting in variations in power output and aerodynamic loading compared to conditions under mean synoptic forcing. In a wind farm, [most turbines](#) [wind turbines can fully or partially](#) operate in the wake regions of [upstream turbines](#) [those upstream, depending on the wind direction](#). Therefore, understanding the response of turbine wakes to atmospheric phenomena, including AGWs, is critical for accurately modeling wind farm performance under realistic atmospheric conditions.

25 The influence of AGWs on wind farm performance has recently attracted considerable attention (Wilczak et al., 2019; Xia et al., 2021; Draxl et al., 2021). Through spectral analysis of field measurements and mesoscale simulations, researchers have observed that low-frequency oscillations in turbine and farm power production correlate with wind speed fluctuations associated with AGWs. More recently, Ollier and Watson (2022) conducted a parametric study using Reynolds-averaged Navier–Stokes simulations to investigate factors influencing AGW effects. Their findings highlight the importance of the wind
30 farm’s location within the wave cycle: wake losses in power production are mitigated during AGW peaks and exacerbated during AGW troughs.

Large-eddy simulation (LES) provides a robust method for generating detailed data on wind farm flows and outputs. To account for large-scale meteorological effects, mesoscale simulations (e.g., the Weather Research and Forecasting (WRF) model (Skamarock et al., 2008)) or field measurements (Allaerts et al., 2023; Quon, 2024) are often used to inform mesoscale
35 forcing, which captures non-stationary atmospheric conditions such as diurnal thermal instability. Recently, Wise et al. (2024) combined LES with the WRF model to study interactions between AGWs and wind farms. Their results revealed that the passage of an AGW modulates the mesoscale environment, significantly impacting wind farm power production and structural loading.

Despite these advancements, several gaps remain. While prior studies have primarily focused on turbine outputs, the response
40 of turbine wakes to AGWs remains poorly understood. Furthermore, it is unclear whether LES driven by field measurements can accurately capture transient atmospheric phenomena like AGWs. In this work, we use measurement-driven LES to explore the potential effects of AGWs on wake dynamics. Our analysis focuses on two key wake phenomena: (1) low-frequency meandering motions, which govern wake expansion and recovery, and (2) turbulence generation due to wake shear, which enhances turbulent kinetic energy (TKE) within the wake region.

45 We introduce the American WAKE experimeNt (AWAKEN) field campaign which provides measurements of AGWs and the measurement-driven LES setup in Sect. 2. Then, we analyze the effects of AGWs on wake meandering, wake turbulence generation, mean wake recovery, and power fluctuations in Sect. 3. Finally, we present our conclusions in Sect. ??.

2 Methods

2.1 AWAKEN measurement

50 AWAKEN is a large-scale field campaign designed to obtain detailed observations of wind farm–atmosphere interactions, with the goal of advancing the understanding of wind farm physics and improving overall performance (Moriarty et al., 2020). [Figure 1](#) shows the schematic of the measurement sites and terrain features in the AWAKEN campaign. Given the prevailing southerly wind direction, site A1 serves as the inflow condition for the King Plains wind farm, which is the most instrumented wind farm. ~~The west-east mountainous terrain in this region causes multiple AGW events, which~~
55 [Multiple AGW events](#) have been identified from [atmospheric measurements](#) [horizontal scanning by X-band radars and vertical profiling by scanning Doppler lidars](#). [The high-resolution lidar measurements at site A1 are used in our data assimilation in order to capture transient features of AGWs.](#)

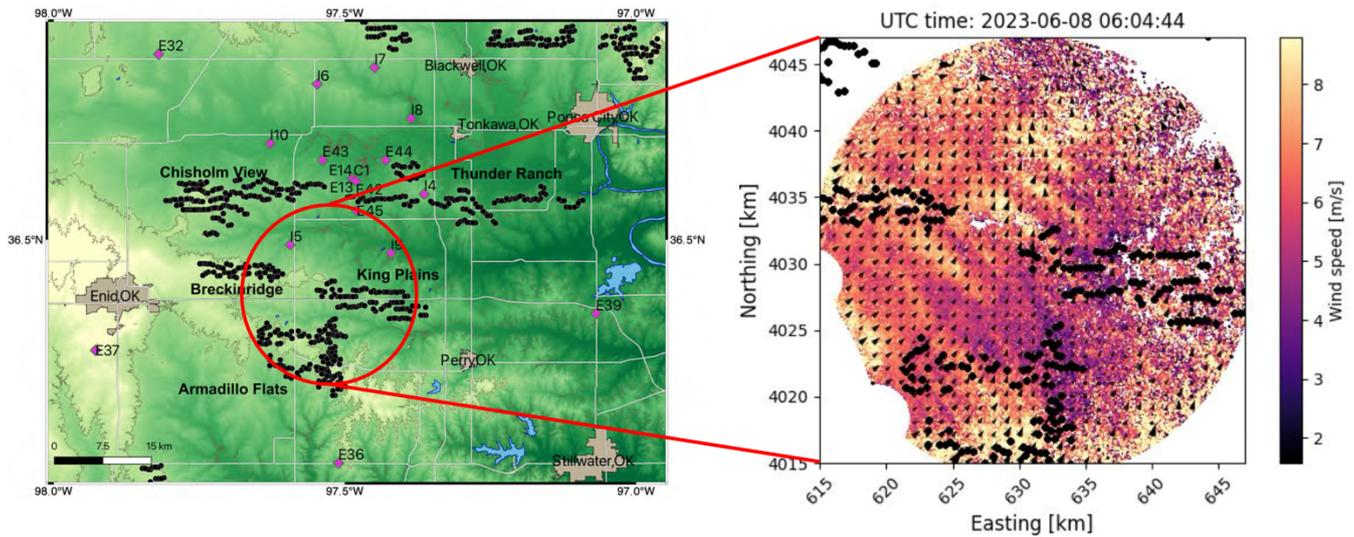


Figure 1. Left: Map of AWAKEN measurement sites. The contour value is elevation over the sea level. The terrain is a fluviate plain with a gradual west-to-east slope (Debnath et al., 2022). This figure is adapted from Debnath et al. (2022) Moriarty et al. (2024). The white arrow indicates Right: Radar measurement taken approximately at the prevailing southerly hub height during the AGW event on 8 June 2023. The figure is provided by US National Renewable Energy Laboratory (NREL). Black solid circles represent wind turbines.

For this study, we focus on the AGW event on 8 June 2023, because its vertical extent spans the rotor layer of a wind turbine. Figure ?? The right panel of Fig. 1 shows the radar observations of this AGW event. The wind speed peaks and troughs elongated in the northwest-southeast direction indicate large-scale wave-like structures flowing over multiple wind farms. These wave-like structures horizontally propagate from southwest to northeast with a wavelength of approximately 2.5-3 km. Radar measurement taken approximately at the hub height during the AGW event on 8 June 2023. The figure is provided by US National Renewable Energy Laboratory (NREL). Black solid circles represent wind turbines.

In Fig. 2, the top-left panel shows lidar measurements of wind speed at site A1 during the selected AGW event. The horizontal axis represents UTC time (local time + 5 hours), while the vertical axis represents height above ground level. The duration of the AGW event is approximately 1200 s and the wind speed exhibits low-frequency oscillations with a period of roughly 600 s. Missing The missing observations near the ground have been will be filled using a natural neighbor interpolation technique (Allaerts et al., 2023) , and the resulting fixed time-height history is shown in the bottom-left panel. It should be noted that although orographically-induced AGWs are theoretically stationary, this is only true for the component of the wave group velocity parallel to the background wind. This means that in practice the AGWs are advected by the background wind depending on its component perpendicular to the wave group velocity. In addition, horizontal shear in the background wind speed can contribute to horizontal advection by refracting the AGWs. The high-speed region at lower heights suggests the presence of a low-level jet. This vertical wind profile deviates significantly from the standard atmospheric boundary layer profile, where wind speed typically increases monotonically with height above the ground. in the following data assimilation.

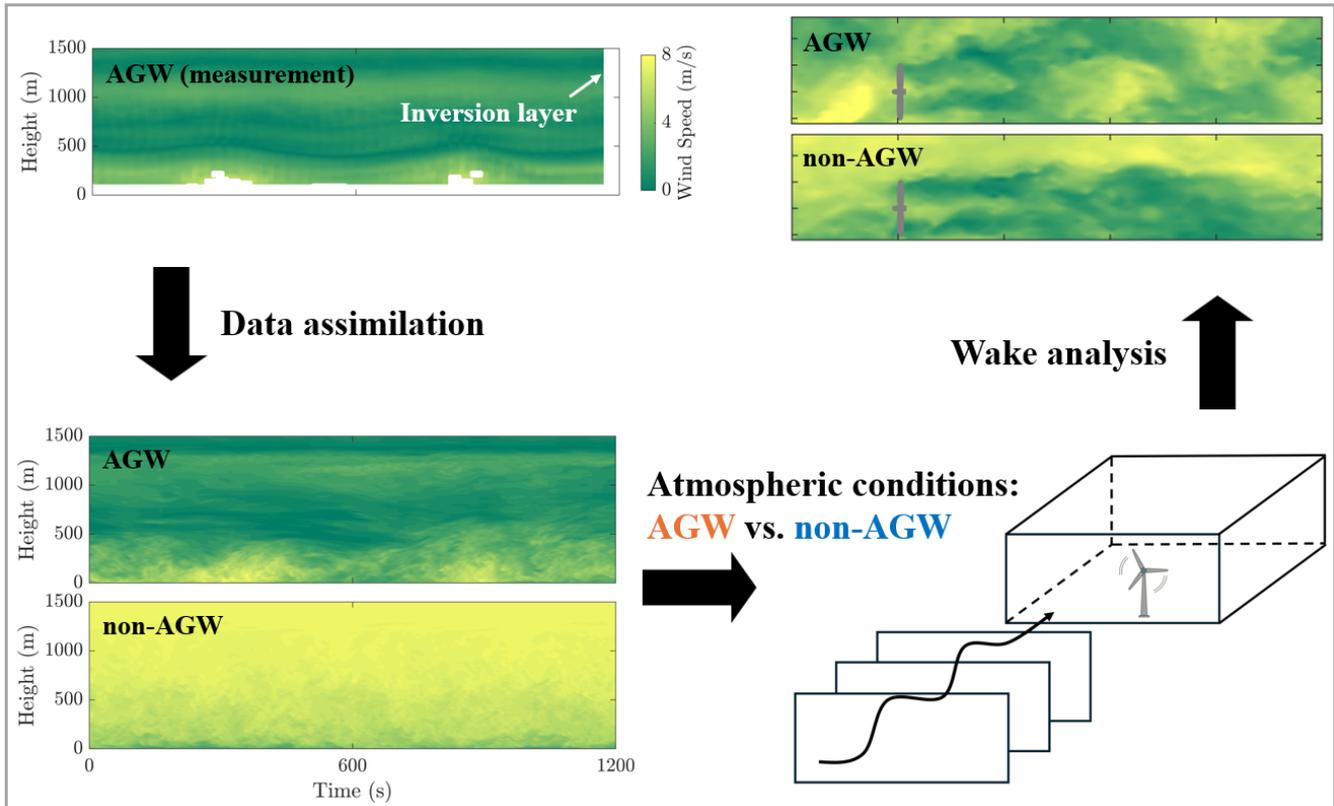


Figure 2. Flow chart of the present measurement-driven LES study. In the left column of contours, from blue to yellow indicates wind speed from 0 to 7.5 m/s. In top-right contour, from green to yellow indicates magnitudes from 0.2 to 1.4 for streamwise velocity normalized by inflow mean velocity at the hub height.

75 2.2 Measurement-driven LES

A measurement-driven large-eddy simulation (LES) model is developed to simulate turbine flow under AGW inflow conditions. This approach leverages the mesoscale-microscale coupling capability of SOWFA (Simulator for Wind Farm Applications) (Churchfield et al., 2012) and the high spatio-temporal resolution measurements from the AWAKEN campaign. The simulation is carried out in two stages: (i) inflow simulation, which assimilates AGW measurements into the atmospheric simulation, and (ii) turbine simulation, which generates wind turbine wake flow under the measurement-assimilated inflow condition.

In the first stage, the inflow simulation solves the spatially filtered incompressible Navier–Stokes equations of mass and momentum, and the transportation equation of potential temperature. The momentum equation includes two source terms. One source term accounts for mesoscale forcing computed through an indirect profile assimilation method (Allaerts et al., 2020).

85 This method ensures that the LES solution reproduces the time-height wind speed profile shown in the top panel of the bottom-

left contour in Fig. 2, thus capturing the key characteristics of the AGW inflow. The other source term in the momentum equation accounts for the Coriolis force induced by planetary rotation.

The potential temperature remains constant below the capping inversion layer and increases linearly in the above regions, which follows the potential temperature profile in conventionally neutral boundary layers. Such a simplification of the thermal stability condition is necessary due to lack of temperature measurement data. Consequently, the atmospheric condition in our simulation is neutral, whereas in reality it could have been either neutral or thermally stable. The inversion layer height is set as 1250 m, based on the vertical distribution of wind speed shown in the left column of Fig. 2. Subgrid-scale effects are modeled using a standard turbulent kinetic energy (TKE) equation (Deardorff, 1980).

The computational domain is configured as a straight channel with dimensions of $3000 \times 3000 \times 1500$ m in the streamwise, spanwise and vertical directions, respectively. The domain is discretized into $300 \times 300 \times 150$ grid cells. A slip-wall condition is applied at the upper boundary, with velocity gradients set to zero, while the bottom boundary uses a local-similarity-based logarithmic wall model (Moeng, 1984) to account for viscous and subgrid-scale stresses. The effective roughness height is set to 0.1 m, representing typical onshore terrain. Periodic conditions are applied at the lateral boundaries.

The inflow simulation runs for 2400 s, with the first 1200 s allocated for spin-up and the remaining 1200 s representing the AGW event. In the bottom-left contour of Fig. 2, the bottom panel displays the time-height wind speed history from the inflow simulation. When compared to the lidar measurements in the top panel, the present LES not only captures the low-frequency wind speed oscillations caused by the AGW event but also resolves turbulence structures with higher spatio-temporal resolution than can be captured by the lidar. The LES solution for velocity and temperature at the upstream boundary is saved at a time step of 0.5 s during the last 1200 s, providing inflow conditions for the subsequent turbine simulation. ~~These inflow data are represented by the orange slices in the bottom-right of~~

The bottom-left panel of Fig. 2 shows time-height histories from inflow simulations of the AGW event (the AGW case) and a standard atmospheric boundary layer (the non-AGW case). The AGW simulation shows overall agreement with the AGW measurement. The high-speed region at lower heights in the AGW case suggests the presence of a low-level jet. This vertical wind profile differs significantly from that for the non-AGW case, where wind speed typically increases monotonically with height above the ground. To further quantify these comparisons, we show in Fig. 2-3 wind speed time series at the hub-height. The results indicate that our simulation not only captures the large-scale wavy oscillations observed in the measurements, but also resolves smaller-scale turbulent fluctuations.

In the second stage, the turbine simulation incorporates the effect of wind turbines as additional source terms in the Navier–Stokes momentum equations. The turbine is modeled using the NREL 5-MW reference turbine (Jonkman, 2009), a three-bladed horizontal-axis turbine with a rotor diameter of $D = 126$ m and a hub height of 90 m. This open-source turbine model is used as a proxy for the ~~2.8-MW-MW~~ General Electric turbines deployed at the King Plains wind farm. Regarding the geometric features, the differences between the GE 2.8 MW turbine and the NREL 5 MW reference turbine are minor: rotor diameter of 127 m vs. 126 m, and hub height of 88.5 m vs. 90 m, respectively.

The turbine is placed $5D$ downstream of the inflow boundary, and its forcing is modeled using an actuator disk method with rotation (Wu and Porté-Agel, 2011). While the effects of the nacelle and tower are neglected, this method has demonstrated

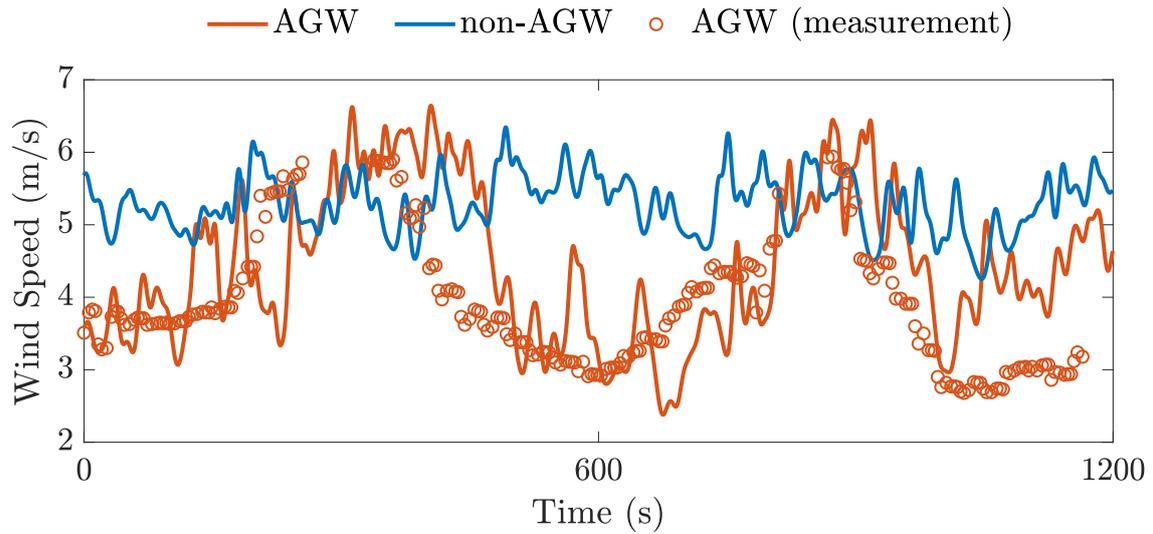


Figure 3. Time series of wind speed at hub-height from both simulation cases, AGW and non-AGW, and from measurements for the AGW case.

been demonstrated to show good agreement with wind tunnel measurements and high-fidelity numerical simulations in the far wake region (Wu and Porté-Agel, 2011; Stevens et al., 2018), which primarily influences wind farm flow characteristics. The turbine operates at a constant rotational speed of nine ~~rotations-per-minute~~ rotations per minute (9 rpm). This simplified operating condition is used because the present work serves as a preliminary investigation of a single turbine, rather than a
 125 detailed simulation of the exact AWAKEN wind farm.

The inflow simulation slices are imposed at the inflow boundary. A Rayleigh damping layer is applied at the outflow boundary to prevent unphysical wave reflections. The remaining boundary conditions (top, bottom, and lateral) are consistent with those used in the precursor inflow simulation. After convergence, the flow field and turbine power are saved. The flow data collection subdomain spans $-2 \leq x/D \leq 8$, $-2 \leq y/D \leq 2$, and $-0.7 \leq z/D \leq 2$, where x , y , and z represent the streamwise, spanwise, and vertical coordinates, respectively. The origin is located at the turbine hub center.
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The turbine simulation provides wake flow data which can be used to analyze the wake dynamics under the AGW inflow condition, referred to as the AGW case. For comparison, we also perform a turbine simulation without AGWs, referred to as the non-AGW case. In this case, a conventionally neutral boundary layer is simulated as the inflow condition using a wall-modeled LES method designed to capture scaling laws for both mean velocity and velocity fluctuations (Feng et al., 2024a).
 135 Once the inflow simulation reaches a statistically steady state, the flow data are collected for an additional 1200 s, as in the AGW case. Both the mean wind speed at the hub height, $U_{\text{hub}} = 5$ m/s (consistent with the mean lidar measurements), and

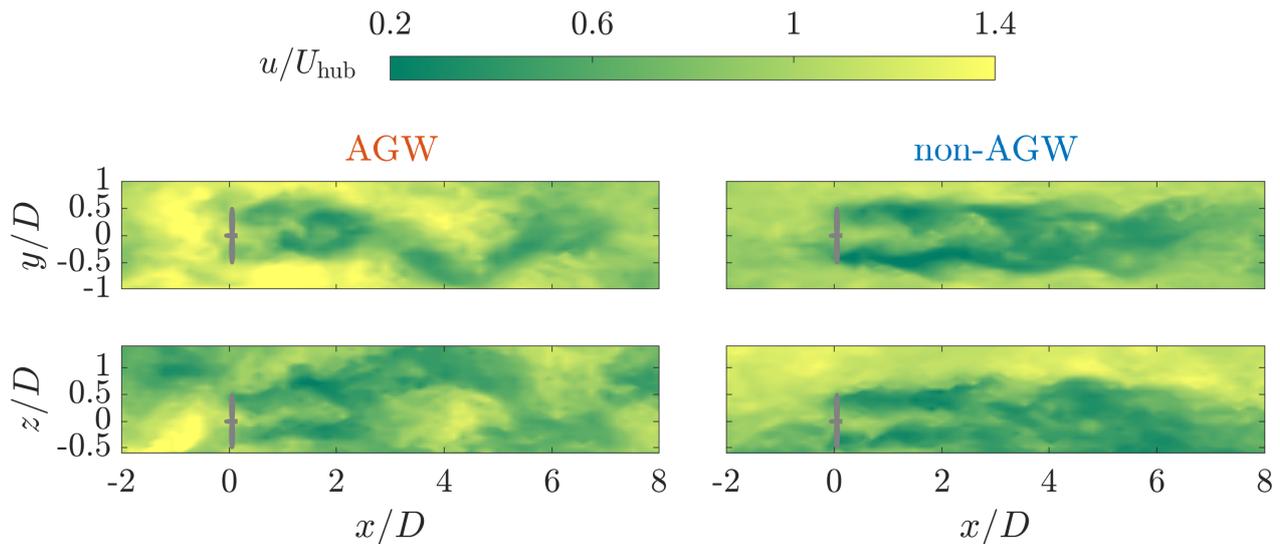


Figure 4. Instantaneous streamwise velocity normalized by U_{hub} in the spanwise (top) and (bottom) vertical planes passing through the turbine center. The data are compared between the AGW (left) and non-AGW (right) cases. The gray bar in each plot indicates the turbine location.

vertical temperature profile remain identical for the AGW and non-AGW inflow conditions. However, while the non-AGW inflow follows a logarithmic scaling law, the AGW inflow exhibits a jet-like shape in the vertical wind-speed profile.

Throughout this paper, the instantaneous streamwise, spanwise, and vertical velocity components are denoted as u , v and w with their time-averaged counterparts denoted as U , V and W . Time-averaging is performed over the 1200-s duration of the AGW event, which corresponds to approximately two wave cycles.

3 Results and discussions

3.1 Wake meandering

Wake meandering refers to large-scale oscillations of the wake flow driven by low-frequency spanwise and vertical velocity fluctuations in the atmospheric flow (Ainslie, 1988). These velocity fluctuations intermittently change the wind direction, causing the wake flow to deflect as if it were a passive tracer. Fig. 4 presents instantaneous velocity contours in the spanwise (top) and vertical (bottom) planes for both the AGW (left) and non-AGW (right) cases. The snapshot corresponds to the first peak in wind speed during the AGW event. In both planes, the AGW case causes larger-scale deflections of the wake center, indicative of stronger wake meandering, compared to the non-AGW case. As a result, the AGW case shows a greater range of wake excursions. Specifically, as shown in the left column of Fig. 4, both spanwise and vertical wake excursions extend beyond one rotor diameter for the AGW case, whereas for the non-AGW case, they only slightly exceed 0.5 turbine diameter.

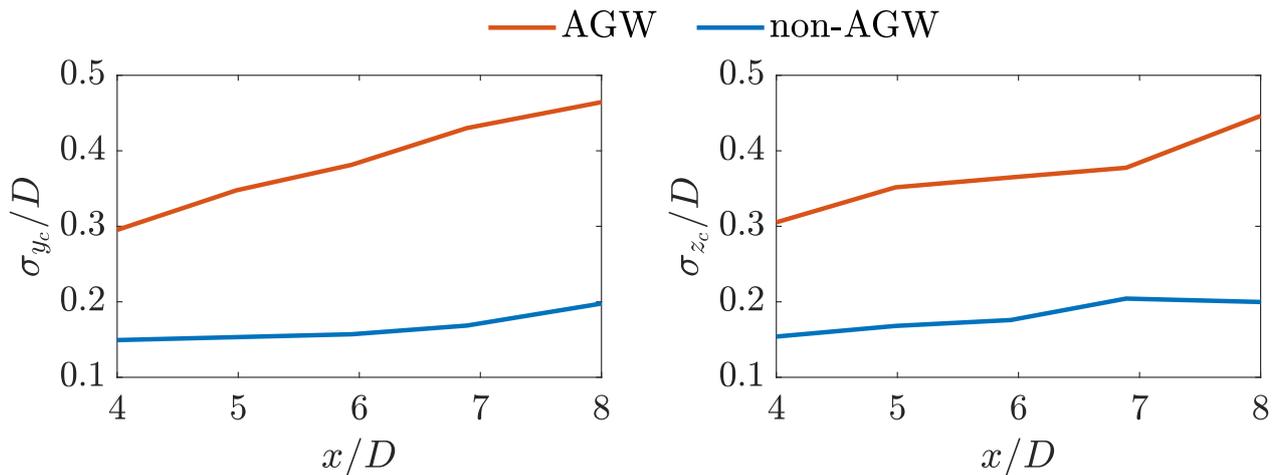


Figure 5. Mean magnitudes of wake meandering in the spanwise (left) and (right) vertical directions for distances $4D$ - $8D$ downstream of the turbine. The data are compared between the AGW (red line) and non-AGW (blue line) cases.

To quantify the mean amplitude of wake meandering, we use a metric, A_m , defined as the standard deviation of large-scale wake-center deflections. The wake centers are determined by first filtering the instantaneous ~~wake-deficit~~ wake deficit flow field with a spatial filter spanning three rotor diameters to isolate meandering motions. The filtered wake deficit is then fitted to a two-dimensional Gaussian profile at each downstream location, following the method described by Trujillo et al. (2011). The location of the maximum wake deficit is taken as the wake center. In both spanwise and vertical directions, the magnitudes of wake center deflections are found to be larger for the AGW case, as evident in Fig. 4. Fig. 5 shows A_m in the far-wake region ($4 \leq x/D \leq 8$). The meandering amplitude generally increases with downstream distance, as the wake-center deflection at each downstream location is a cumulative effect of upstream deflections. In both the spanwise and vertical planes, the AGW case results in A_m nearly double that of the non-AGW case, consistent with the observations in Fig. 4.

The stronger wake meandering observed in the AGW case can be attributed to ~~two primary factors:~~ (i) Presence of AGW wavy structures: These large-scale flow structures induce low-frequency, large-magnitude velocity fluctuations in both the the higher TKE at relatively low frequencies, as will be discussed below in relation to Fig. 8. Previous studies have shown that spanwise and vertical directions, thereby amplifying wake meandering magnitudes (Feng et al., 2022; Li et al., 2022). (ii) Increased turbulence level: Turbulent structures with length scales larger than three rotor diameters can cause velocity fluctuations at such a frequency range directly drive wake meandering (Larsen et al., 2008; Feng et al., 2022). This finding is consistent with the work of Wise et al. (2024), which reported that AGWs can increase overall turbulence levels and amplify horizontal wake meandering. These structures become more pronounced when AGWs are present, further intensifying the meandering motion.

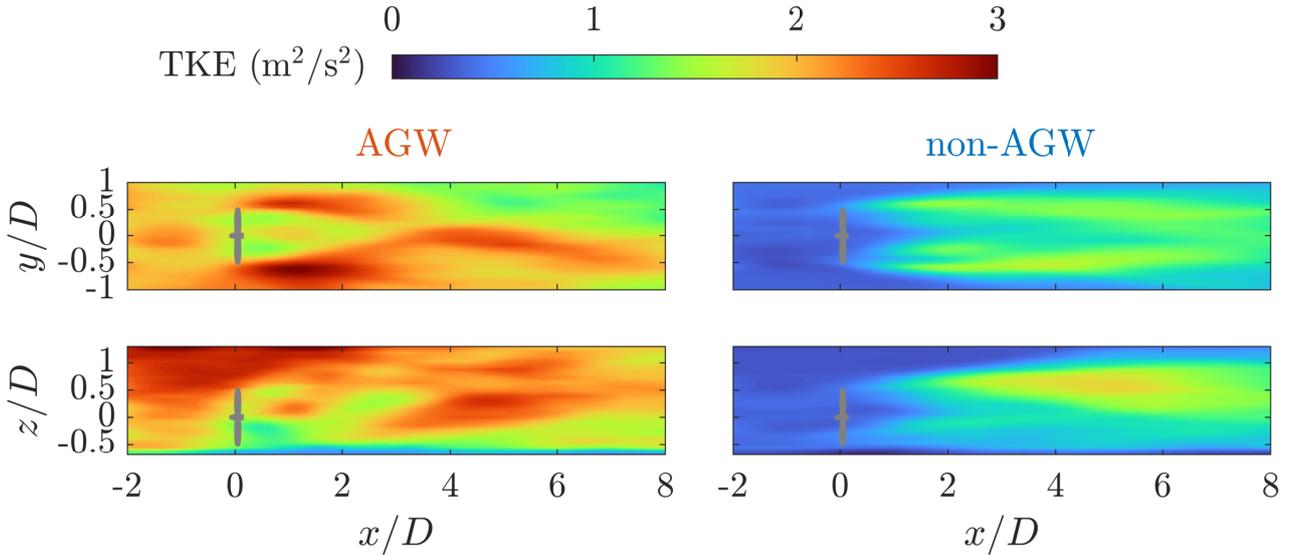


Figure 6. Mean-TKE in the spanwise (top) and vertical (bottom) planes passing through the turbine center. The data are compared between AGW (left) and non-AGW (right) cases.

3.2 Wake turbulence generation

170 While wake meandering is driven by large-scale velocity fluctuations, wake turbulence is predominantly generated through convective instabilities associated with smaller-scale velocity fluctuations (Heisel et al., 2018; Feng et al., 2022). The convective instability mechanism suggests that TKE generation in the wake arises from the selective amplification of upstream velocity fluctuations by shear instabilities induced by wake shear (Heisel et al., 2018; Foti et al., 2018; Feng et al., 2024b). The streamwise, spanwise and vertical velocity fluctuations are $u' = u - U$, $v' = v - V$ and $w' = w - W$, respectively. TKE is then
 175 calculated as $\overline{u'^2 + v'^2 + w'^2} = \overline{u'^2} + \overline{v'^2} + \overline{w'^2}$.

Figure 6 shows the time-averaged TKE in the spanwise (top) and vertical (bottom) planes for the AGW (left) and non-AGW (right) cases. Compared to the non-AGW case, the AGW case exhibits higher mean-TKE levels in both the inflow and wake regions, but lower TKE generated in the wake region when normalized by the inflow TKE. Herein, we define a measure for such inflow-normalized TKE generation as $\Delta TKE_{\text{mean}}^* = (\text{TKE}_{\text{mean}} - \text{TKE}_{\text{mean,in}}) / \text{TKE}_{\text{mean,in}}$, where $\text{TKE}_{\text{mean,in}}$
 180 is the mean $\Delta TKE^* = (\text{TKE} - \text{TKE}_{\text{in}}) / \text{TKE}_{\text{in}}$, where TKE_{in} is the TKE at $x/D = -2$. The TKE field is spatially-averaged over the rotor disk area at each streamwise location.

Figure ?? The left panel in Fig. 7 shows streamwise variation of $\Delta TKE_{\text{mean}}^*$ for the AGW and non-AGW cases. In For the AGW case, $\Delta TKE_{\text{mean}}^*$ initially remains close to zero before slightly decreasing in the far-wake region. By contrast, in the non-AGW case, $\Delta TKE_{\text{mean}}^*$ increases sharply to approximately 2 and maintains similar values in the far-wake region,

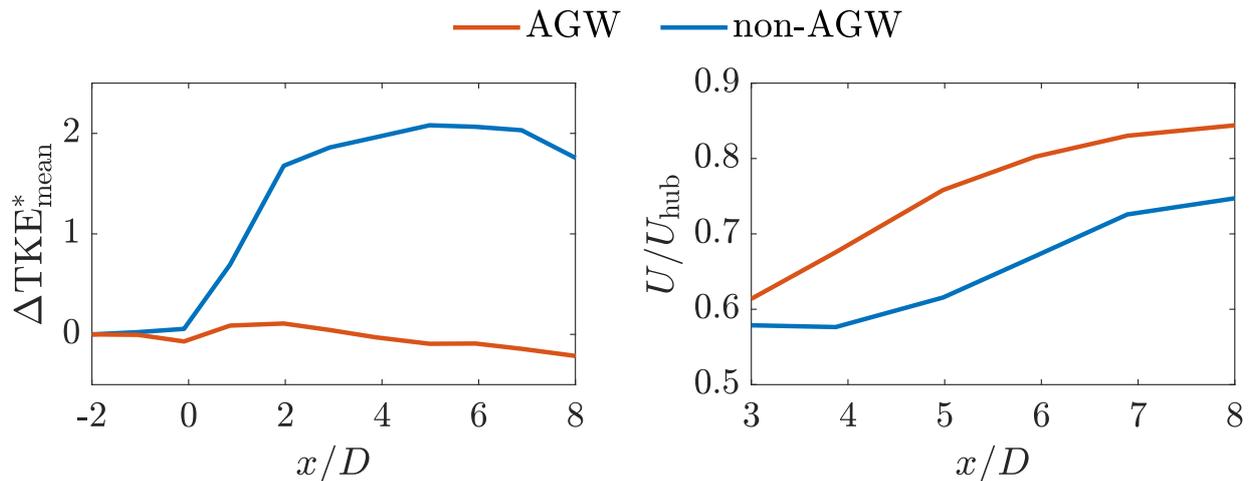


Figure 7. Left: Inflow-normalized TKE generation, $\Delta TKE_{\text{mean}}^*$, at each streamwise location. Right: Mean streamwise wake deficit along the turbine centerline. The data are compared between the AGW (red line) and non-AGW (blue line) cases.

185 indicating that the wake TKE is nearly three times the inflow TKE. The significantly lower $\Delta TKE_{\text{mean}}^*$ in the AGW case can be attributed to reduced wake shear, which results from faster wake recovery, as we will discuss in Sect. 3.3.

To investigate the spectral-time-varying characteristics of wake turbulence generation, we applied Fourier transforms to the time series of velocity fluctuations to compute the power spectral density of TKE, $\phi_{\text{TKE}} = \phi_u + \phi_v + \phi_w$ (where ϕ_u , ϕ_v and ϕ_w represent the power spectral density of u' , v' and w' , respectively). Fig.Figure 8 shows TKE spectra multiplied by frequency, $f\phi_{\text{TKE}}$, at various Strouhal numbers, $St = fD/U_{\text{hub}}$ (f is the frequency, D is the rotor diameter, and U_{hub} is the hub-height mean inflow wind speed), for the AGW (top) and non-AGW (bottom) cases. Note that the inverse of the Strouhal number corresponds to the wavelength normalized by the rotor diameter, indicating the characteristic turbulence length scales. The area under the spectral curve corresponds to the TKE within a specific frequency range. The dotted and solid lines represent the spectra calculated for the inflow region (2D upstream of the turbine) and the wake region (spectra are compared between
195 the AGW (top) and non-AGW (bottom) cases for both inflow and wake regions, and between the downstream 4D downstream of the turbine), respectively.

Despite differences in the peak frequencies of inflow TKE, the wake TKE for both AGW and non-AGW cases is concentrated within a similar frequency range, $0.1 < St < 1$. The peak Strouhal number in the wake TKE spectra, $St_{\text{wake}} \approx 0.3$, corresponds to the characteristic frequency of shear-induced wake turbulence. This frequency has been shown to be independent of turbine
200 design and operating conditions (Foti et al., 2018; Heisel et al., 2018). Therefore, we conclude that the presence of AGWs does not alter the dominant role of convective instabilities in wake turbulence generation (left) and 8D (right) cases for the wake region.

While the mechanism of turbulence generation remains consistent, the AGW and non-AGW cases exhibit notable differences in their TKE spectra. For the AGW case (top panel of Fig. 8), the inflow spectrum The inflow spectrum for the AGW case

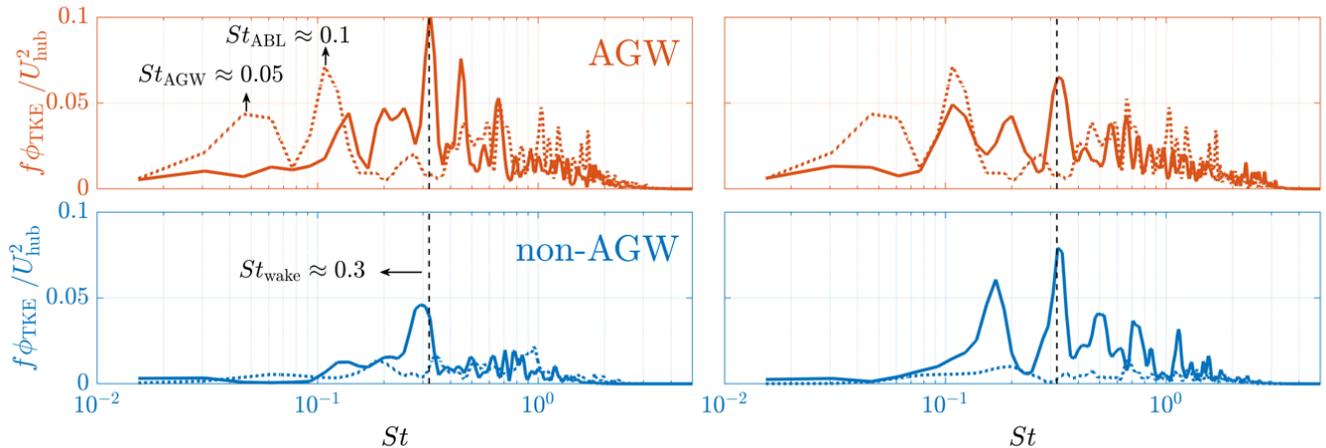


Figure 8. TKE spectra multiplied by the frequency f and non-dimensionalized by U_{hub}^2 as a function of Strouhal number $St = fD/U_{\text{hub}}$. The data are compared between the AGW (top) and non-AGW (bottom) cases. In each plot, the dotted and solid lines represent spectra calculated at $(x/D, y/D, z/D) = (-2, 0, 0)$ for the inflow $((x/D, y/D, z/D) = (-2, 0, 0))$ and $(x/D, y/D, z/D) = (4, 0, 0)$ for the wake, respectively. The wake spectra in the left and right panels are $4D$ and $8D$ downstream, respectively.

205 reveals two distinct peaks: (i) A lower-frequency peak at $St_{\text{AGW}} \approx 0.05$, corresponding to the AGW wavelength of approximately $2\text{--}2.5$ km, highlighting the capability of the precursor inflow simulation to capture the AGW event; (ii) A higher-frequency peak at $St_{\text{ABL}} \approx 0.1$ associated with the atmospheric boundary layer thickness of approximately 1250 m, as indicated by the inversion capping layer height in the top-left contour of Fig. 2. In the wake region For wall-bounded flows at high Reynolds numbers (e.g. atmospheric boundary layers), Smits et al. (2011) reported that the pre-multiplied TKE spectra in the logarithmic and outer regions exhibit a large-wavelength/low-frequency peak associated with the boundary-layer thickness (i.e., the inversion layer height in the atmospheric boundary layer). This peak arises from the presence of large-scale, the streamwise-elongated structures with characteristic length scales in the order of the boundary-layer thickness (Hutchins et al., 2012)

215 Despite differences in the peak frequencies of inflow TKE, the wake TKE for both AGW and non-AGW cases is concentrated within a similar frequency range, $0.1 < St < 1$, with a peak at $St_{\text{wake}} \approx 0.3$. This frequency peak, which is independent of turbine design and operating conditions, serves as an indicator of convective shear instabilities in far-wake dynamics (Foti et al., 2018; Heise). Therefore, we conclude that the presence of AGWs does not alter the dominant mechanism of wake turbulence generation. For both the AGW and non-AGW cases, such a frequency peak becomes less prominent in $8D$ downstream, as seen in Figure 8, because wake recovery has largely weakened shear instabilities at this region.

220 While the mechanism of turbulence generation remains consistent, the AGW and non-AGW cases exhibit notable differences. For the AGW case, the TKE from these inflow peaks shifts to higher frequencies, $0.1 < St < 1$, with comparable magnitudes. In contrast, for the non-AGW case, the inflow TKE magnitudes are significantly amplified in the wake TKE spectra. This

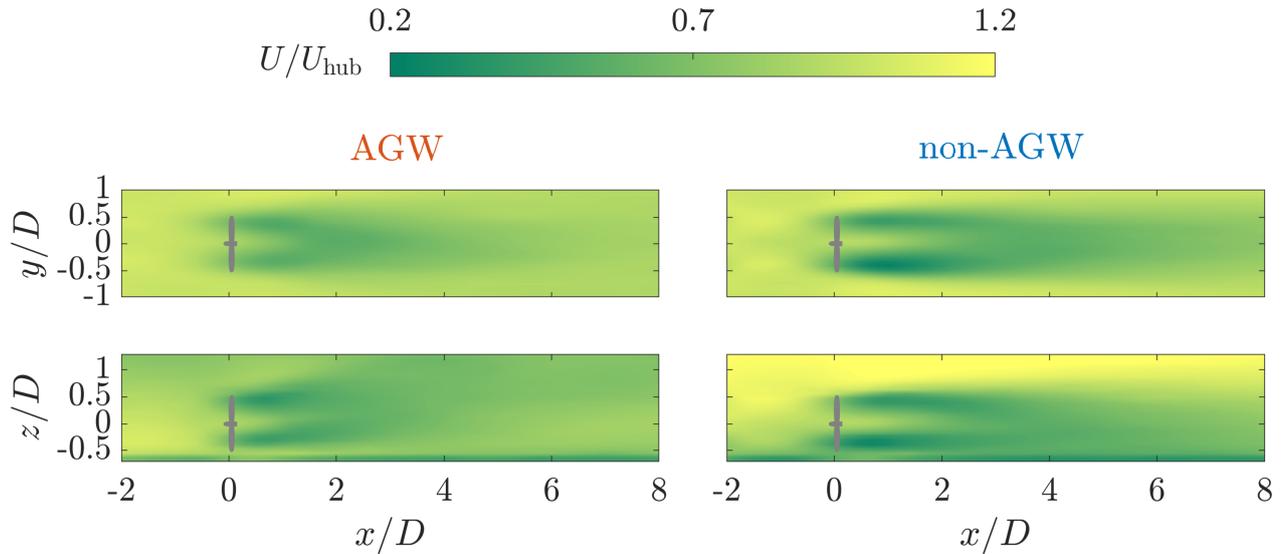


Figure 9. Mean streamwise velocity normalized by U_{hub} in the spanwise (top) and vertical (bottom) planes passing through the turbine center. The data are compared between AGW (left) and non-AGW (right) cases. The gray bar in each plot indicates the turbine location.

provides spectral evidence supporting the observation in Fig. 6, which shows that fractional TKE generation is higher in the non-AGW case.

225 3.3 Mean wake recovery

The expansion of the mean wake flow is driven by a combined effect of wake meandering and turbulent mixing in the instantaneous wake flow. Consequently, larger meandering amplitudes can lead to greater wake expansion and faster recovery. In this section, we analyze the characteristics of the mean wake flow to support the findings in Sect. 3.1, which suggest that AGWs enhance wake meandering.

230 **Figure 9** shows time-averaged streamwise velocity contours in the spanwise (top) and vertical (bottom) planes for the AGW (left) and non-AGW (right) cases. The velocity magnitudes are normalized by U_{hub} . For all plots, the wake region ($0 \leq x/D \leq 8$) exhibits a velocity deficit compared to the inflow region ($-2 \leq x/D \leq 0$) as might be expected. However, in both the spanwise and vertical directions, the wake velocity recovers more quickly towards the ambient velocity for the AGW case. Additionally, as shown in the bottom row of Fig. 9, the AGW and non-AGW cases exhibit distinctly different vertical profiles in the inflow region. While the non-AGW inflow follows a standard boundary layer profile, the AGW inflow shows a low-level jet with the jet nose located near hub height. These low-level jets are also evident in the time-height wind speed history depicted in the left column of Fig. 2.

In order to provide a quantitative comparison, [The right panel in Fig. ??-7](#) shows the U_{hub} -normalized mean streamwise velocity along the turbine centerline in the wake region. In both the AGW and non-AGW cases, the velocity initially decreases

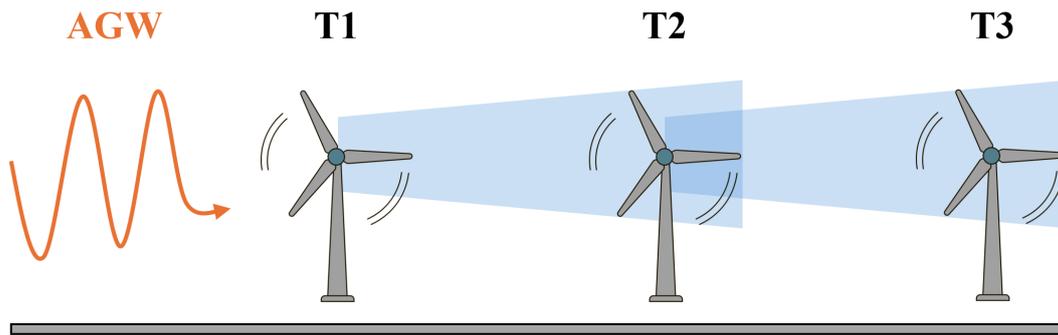


Figure 10. Schematic of the simulation of three turbines under the AGW inflow condition. From upstream to the downstream is subsequently T1, T2 and T3.

240 as a result of the pressure recovery immediately behind the rotor and due to the speed-up region near the turbine center gradually diffusing due to momentum exchange. The velocity then begins to recover from approximately $x/D = 2$ or 3, where the wake deficit becomes Gaussian-shaped. At $x/D = 8$, the velocity recovers to approximately 90% of the ambient velocity for the AGW case, compared to around 75% for the non-AGW case.

The faster recovery of the mean wake mean wake recovery in the AGW case can be attributed to two key factors: (i)
 245 Stronger wake meandering: The inflow spectra in Fig. 8 shows that the AGW inflow contains more intense large-scale turbulent structures, leading to greater meandering amplitudes and, consequently, larger mean wake expansion (Ainslie, 1988; Larsen et al., 2008). (ii) Higher turbulence levels: The presence of AGWs increases TKE, enhancing turbulent mixing mean turbulent kinetic energy contours in Fig. 6 show significantly higher turbulence levels in the AGW case. The increase of TKE enhances turbulent mixing, making the velocity recovery faster in the wake region and accelerating velocity recovery. Mean streamwise
 250 wake deficit along the turbine centerline. The data are compared between the AGW (red line) and non-AGW (blue line) cases.

3.4 Power output of waked turbines

In this section, we analyze the power output of turbines operating in wake regions to validate the dominant role of convective instabilities in wake turbulence generation, as discussed in Sect. 3.2. We simulated three turbines—T1, T2, and T3—arranged
 255 in a streamwise column under AGW inflow conditions, as shown in Fig. 10. Schematic of the simulation of three turbines under the AGW inflow condition. From upstream to the downstream is subsequently T1, T2 and T3. The turbines were spaced Two turbine spacing cases are set: $4D$ apart, ensuring that the waked turbines (T2 and T3) operated at the same downstream distances where the $8D$ spacings, corresponding to the downstream $4D$ and $8D$ wake spectra in Fig. 8 were computed.

Fig. 11 presents the time-series of power fluctuations for the three turbines. For T1, large-magnitude, low-frequency power
 260 fluctuations (with peaks and troughs marked by red circles) are observed, driven by large-scale wind speed fluctuations in the

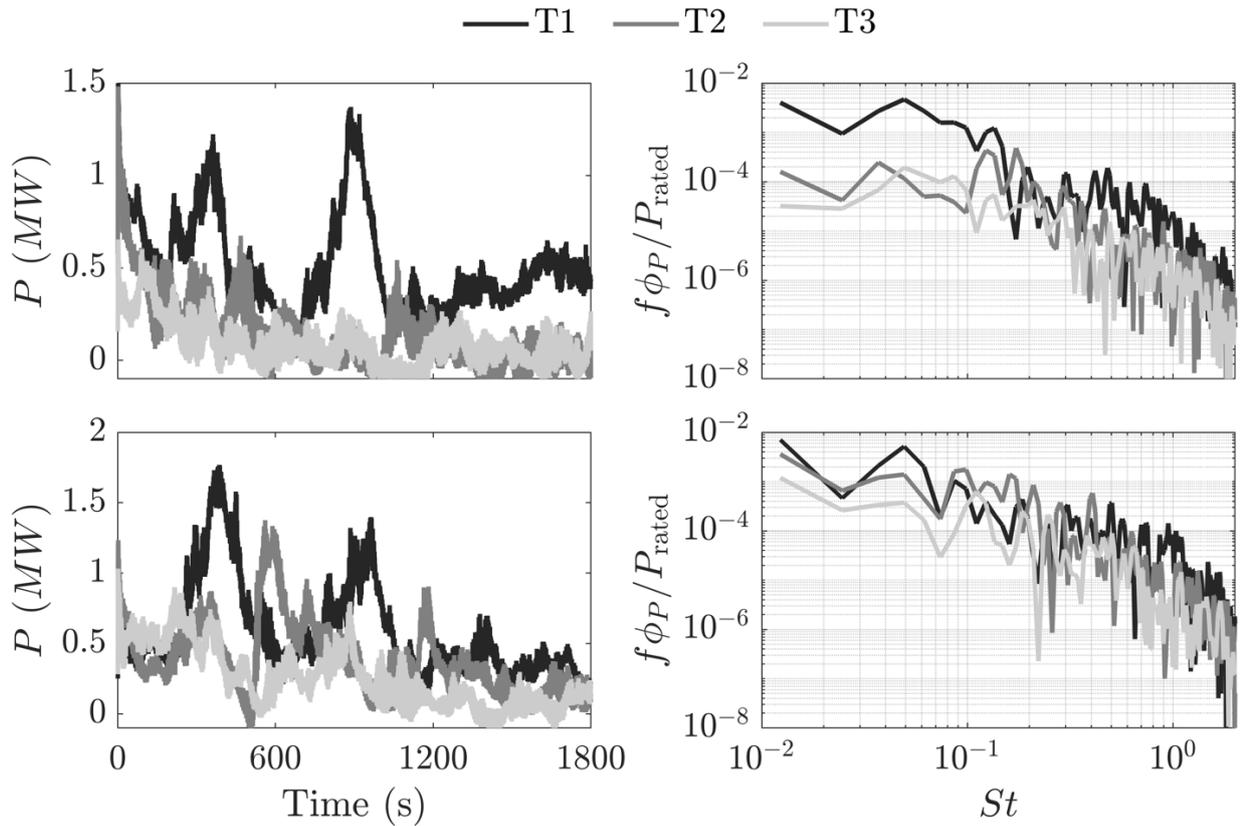


Figure 11. Power fluctuations—Time series (left) and spectra (right) of three turbines in a streamwise column—turbine power for the three-turbine simulations with 4D (top) and 8D (bottom) spacings during the AGW event. The black circles mark peaks and troughs of low-frequency oscillations in the power output of T1, which are associated with the presence of AGWs.

AGW inflow. These fluctuations are significantly attenuated—Figure 11 shows time series (left) and spectra (right) of turbine power for the three-turbine simulations with 4D (top) and 8D (bottom) spacings. For the 4D spacing case, the presence of AGWs induces large-scale power oscillations at the first turbine (T1), which are strongly attenuated at the downstream turbines (T2 and nearly disappear for T3. This trend results from the convective instability mechanism, which shifts the low-frequency velocity fluctuations in the inflow to higher-frequency ones in). For the 8D spacing case, the wake region, as shown in the TKE spectra of the AGW case (top plot of Fig. 8). Consequently, the inflow conditions for attenuation of power oscillations is weaker, and T2 still exhibits visible peaks with a time delay relative to T1. The difference in power attenuation between 4D and T3 feature fewer large-scale wind speed fluctuations—8D spacing is also evident in the corresponding spectra. This behavior is because, as we showed in Fig. 8, the shear instability mechanism that damps low-frequency velocity fluctuations becomes weaker further downstream.

However, it is noteworthy that For both 4D and 8D spacing, T2 exhibits ~~power peaks~~ low-frequency power peaks, although with lower magnitudes and a time delay of approximately 100 s compared to T1. Considering the advection velocity of the AGWs ($U_{\text{hub}} = 5$ m/s) and the turbine spacing (~~4D = 504 m~~), these peaks could be caused by the AGW event. ~~Specifically,~~ T2 occasionally operates in large-scale AGW flow structures when the wake behind T1 meanders away, temporarily exposing T2 to the undisturbed AGW inflow.

4 Conclusions

4 Conclusions

By simulating turbine flow under an AGW event and a standard atmospheric boundary layer (non-AGW), we investigate the impact of AGWs on two key phenomena in wind turbine wake dynamics: wake meandering and wake turbulence generation. Additionally, we analyze mean wake recovery and turbine power fluctuations to support our findings.

Firstly, AGWs result in stronger low-frequency, meandering motions in the wake region. This is attributed to two factors: (i) large-scale AGW flow structures generate low-frequency, large-magnitude velocity fluctuations in both the spanwise and vertical directions, amplifying wake meandering, and (ii) smaller-scale turbulent structures (with length scales greater than three rotor diameters) become more intense due to the elevated turbulence levels. The combination of stronger wake meandering and enhanced turbulent mixing in the instantaneous wake flow leads to faster mean wake recovery under AGW inflow conditions.

Secondly, TKE spectra in the wake region consistently peak at a Strouhal number of approximately 0.3 for both AGW and non-AGW cases, even though the dominant frequencies in the AGW inflow are significantly lower. This finding suggests that turbulence generation in the far-wake region adheres to the convective instability mechanism in both cases. Compared to the non-AGW case, the AGW case exhibits higher inflow TKE levels but a lower amplification factor via convective instabilities in the wake region, likely due to reduced wake shear resulting from faster wake recovery. To further support this conclusion, we examine the power production of three turbines arranged in a streamwise column under AGW inflow conditions. Large-scale AGW flow structures induce significant low-frequency power fluctuations at the most upstream turbine. However, these fluctuations are significantly attenuated at the two downstream turbines, which predominantly operate within the wake regions. This observation underscores the dominant role of convective instabilities in wake turbulence generation.

These findings offer insights for wake modeling under realistic atmospheric conditions, particularly in the presence of transient phenomena such as AGWs. Furthermore, the current measurement-driven LES method can serve as a robust tool for understanding and modeling the inter-scale coupling between mesoscale synoptic forcing and microscale wind-farm flow dynamics.

The present ~~study focuses on terrain-induced AGWs, with a certain period which depends on the wavelength of the AGWs and their effective streamwise advection speed. In other synoptic situations, this period could vary significantly. Furthermore, AGWs can also be triggered by meteorological phenomena such as thunderstorms and cold or warm fronts. In such cases, AGWs can be propagating waves. Future study work is intended as a case study focusing on a specific AGW event. Future studies~~ should incorporate AGW events originating from various sources and with different ~~periods~~ wavelengths to comprehen-

sively understand their roles in ~~wake-dynamics~~turbine wake and wind farm flows. Additionally, extending the measurement-
305 driven LES method to other transient atmospheric phenomena, such as convective structures and low-level jets, ~~represents~~
would be a promising direction for further investigation.

Data availability. The atmospheric measurement data used in this paper are open source and can be found at <https://a2e.energy.gov/data>.

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analysis. ND was responsible for software, validation and discussion. SJW was responsible for the writing-review and editing, conceptual-
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Competing interests. The authors declare that they have no conflict of interest.

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References

- 315 Ainslie, J. F.: Calculating the flowfield in the wake of wind turbines, *Journal of wind engineering and Industrial Aerodynamics*, 27, 213–224, 1988.
- Allaerts, D., Quon, E., Draxl, C., and Churchfield, M.: Development of a time–height profile assimilation technique for large-eddy simulation, *Boundary-Layer Meteorology*, 176, 329–348, 2020.
- Allaerts, D., Quon, E., and Churchfield, M.: Using observational mean-flow data to drive large-eddy simulations of a diurnal cycle at the
320 SWiFT site, *Wind Energy*, 26, 469–492, 2023.
- Churchfield, M. J., Lee, S., Michalakes, J., and Moriarty, P. J.: A numerical study of the effects of atmospheric and wake turbulence on wind turbine dynamics, *Journal of turbulence*, p. N14, 2012.
- Deardorff, J. W.: Stratocumulus-capped mixed layers derived from a three-dimensional model, *Boundary-layer meteorology*, 18, 495–527, 1980.
- 325 Debnath, M., Scholbrock, A. K., Zalkind, D., Moriarty, P., Simley, E., Hamilton, N., Ivanov, C., Arthur, R. S., Barthelmie, R., Bodini, N., et al.: Design of the American Wake Experiment (AWAKEN) field campaign, in: *Journal of Physics: Conference Series*, vol. 2265, p. 022058, IOP Publishing, 2022.
- Draxl, C., Worsnop, R. P., Xia, G., Pichugina, Y., Chand, D., Lundquist, J. K., Sharp, J., Wedam, G., Wilczak, J. M., and Berg, L. K.: Mountain waves can impact wind power generation, *Wind Energy Science*, 6, 45–60, 2021.
- 330 Durran, D. R.: Lee waves and mountain waves, *Encyclopedia of atmospheric sciences*, 1161, 1169, 2003.
- Feng, D., Li, L. K., Gupta, V., and Wan, M.: Componentwise influence of upstream turbulence on the far-wake dynamics of wind turbines, *Renewable Energy*, 200, 1081–1091, 2022.
- Feng, D., Gupta, V., Li, L. K., and Wan, M.: Parametric study of large-eddy simulation to capture scaling laws of velocity fluctuations in neutral atmospheric boundary layers, *Physics of Fluids*, 36, 2024a.
- 335 Feng, D., Gupta, V., Li, L. K., and Wan, M.: Resolvent analysis for predicting energetic structures in the far wake of a wind turbine, *Physics of Fluids*, 36, 2024b.
- Foti, D., Yang, X., and Sotiropoulos, F.: Similarity of wake meandering for different wind turbine designs for different scales, *Journal of Fluid Mechanics*, 842, 5–25, 2018.
- Heisel, M., Hong, J., and Guala, M.: The spectral signature of wind turbine wake meandering: A wind tunnel and field-scale study, *Wind
340 Energy*, 21, 715–731, 2018.
- Hutchins, N., Chauhan, K., Marusic, I., Monty, J., and Klewicki, J.: Towards reconciling the large-scale structure of turbulent boundary layers in the atmosphere and laboratory, *Boundary-layer meteorology*, 145, 273–306, 2012.
- Jonkman, J.: Definition of a 5-MW Reference Wind Turbine for Offshore System Development, National Renewable Energy Laboratory, 2009.
- 345 Larsen, G. C., Madsen, H. A., Thomsen, K., and Larsen, T. J.: Wake meandering: a pragmatic approach, *Wind Energy: An International Journal for Progress and Applications in Wind Power Conversion Technology*, 11, 377–395, 2008.
- Li, Z., Dong, G., and Yang, X.: Onset of wake meandering for a floating offshore wind turbine under side-to-side motion, *Journal of Fluid Mechanics*, 934, A29, 2022.
- Moeng, C.-H.: A large-eddy-simulation model for the study of planetary boundary-layer turbulence, *Journal of the Atmospheric Sciences*,
350 41, 2052–2062, 1984.

- Moriarty, P., Hamilton, N., Debnath, M., Herges, T., Isom, B., Lundquist, J. K., Maniaci, D., Naughton, B., Pauly, R., Roadman, J., et al.: American wake experiment (awaken), Tech. rep., Lawrence Livermore National Lab.(LLNL), Livermore, CA (United States . . . , 2020.
- Moriarty, P., Bodini, N., Letizia, S., Abraham, A., Ashley, T., Bärffuss, K. B., Barthelmie, R. J., Brewer, A., Brugger, P., Feuerle, T., Frère, A., Goldberger, L., Gottschall, J., Hamilton, N., Herges, T., Hirth, B., Hung, L.-Y. L., Iungo, G. V., Ivanov, H., Kaul, C., Kern, S., Klein, P., Krishnamurthy, R., Lampert, A., Lundquist, J. K., Morris, V. R., Newsom, R., Pekour, M., Pichugina, Y., Porté-Angel, F., Pryor, S. C., Scholbrock, A., Schroeder, J., Shartzer, S., Simley, E., Vöhringer, L., Wharton, S., and Zalkind, D.: Overview of preparation for the American WAKE ExperimeNt (AWAKEN), *Journal of Renewable and Sustainable Energy*, 16, 053 306, <https://doi.org/10.1063/5.0141683>, 2024.
- Nappo, C. J.: Mountain Waves, in: *International Geophysics*, vol. 102, pp. 57–85, Elsevier, 2012.
- 360 Ollier, S. J. and Watson, S. J.: Modelling the impact of trapped lee waves on offshore wind farm power output, *Wind Energy Science Discussions*, 2022, 1–43, 2022.
- Quon, E.: Measurement-driven large-eddy simulations of a diurnal cycle during a wake-steering field campaign, *Wind Energy Science*, 9, 495–518, 2024.
- Skamarock, W. A., Klemp, J. B., Dudhia, J., Gill, D. O., Barker, D. M., Duda, M. G., Huang, X.-Y., Wang, W., and Power, J. G.: A Description of the Advanced Research WRF Version 3: NCAR Technical Note NCAR/TN-475+STR, Tech. rep., NCAR, Boulder, CO, <https://opensky.ucar.edu/islandora/object/technotes%3A500/datastream/PDF/view>, 2008.
- 365 Smits, A. J., McKeon, B. J., and Marusic, I.: High-Reynolds number wall turbulence, *Annual Review of Fluid Mechanics*, 43, 353–375, 2011.
- Stevens, R. J., Martínez-Tossas, L. A., and Meneveau, C.: Comparison of wind farm large eddy simulations using actuator disk and actuator line models with wind tunnel experiments, *Renewable Energy*, 116, 470–478, <https://doi.org/https://doi.org/10.1016/j.renene.2017.08.072>, 2018.
- 370 Stull, R. B.: *An introduction to boundary layer meteorology*, vol. 13, Springer Science & Business Media, 1988.
- Trujillo, J.-J., Bingöl, F., Larsen, G. C., Mann, J., and Kühn, M.: Light detection and ranging measurements of wake dynamics. Part II: two-dimensional scanning, *Wind Energy*, 14, 61–75, 2011.
- 375 Wilczak, J. M., Stoelinga, M., Berg, L. K., Sharp, J., Draxl, C., McCaffrey, K., Banta, R. M., Bianco, L., Djalalova, I., Lundquist, J. K., et al.: The second wind forecast improvement project (WFIP2): Observational field campaign, *Bulletin of the American Meteorological Society*, 100, 1701–1723, 2019.
- Wise, A. S., Arthur, R. S., Abraham, A., Wharton, S., Krishnamurthy, R., Newsom, R., Hirth, B., Schroeder, J., Moriarty, P., and Chow, F. K.: Large-eddy simulation of an atmospheric bore and associated gravity wave effects on wind farm performance in the Southern Great Plains, *Wind Energy Science Discussions*, 2024, 1–35, 2024.
- 380 Wu, Y.-T. and Porté-Agel, F.: Large-eddy simulation of wind-turbine wakes: evaluation of turbine parametrisations, *Boundary-layer meteorology*, 138, 345–366, 2011.
- Xia, G., Draxl, C., Raghavendra, A., and Lundquist, J. K.: Validating simulated mountain wave impacts on hub-height wind speed using SoDAR observations, *Renewable Energy*, 163, 2220–2230, 2021.