



Comment on “A theoretical upper limit for offshore wind energy extraction“ by Simão Ferreira et al. (2026)

Maarten Paul van der Laan¹ and Simon Watson²

¹Technical University of Denmark, DTU Wind and Energy Systems, Risø Campus, Frederiksborgvej 399, 4000 Roskilde, Denmark

²Faculty of Aerospace Engineering, Delft University of Technology, 2629 HS Delft, the Netherlands

Correspondence: Maarten Paul van der Laan (plaa@dtu.dk)

Abstract. A theoretical limit for the energy extraction of offshore wind farms has been suggested by Simão Ferreira et al. (2026) based on a simple analytical model that was originally designed to provide an estimate of the wake loss of an infinite wind farm. Simão Ferreira et al. (2026) validated the model with 72 offshore wind farms using an *ad hoc* and undocumented method to correct the model for application to finite wind farms. In this work, we discuss a number of concerns regarding the reproducibility of the finite wind farm correction and its sensitivity to the model results and validation, as well as the application of the model to assess national policies. We conclude that the limit proposed in Simão Ferreira et al. (2026) is not a theoretical limit but a model limit that is strongly dependent on the finite wind farm correction.

1 Introduction

In a recent paper, Simão Ferreira et al. (2026) suggested a theoretical limit for the energy extraction of offshore wind farms in terms of the capacity factor. Simão Ferreira et al. (2026) applied simplified analytic models of a wind turbine power curve, the wind resource and the interaction between the atmospheric boundary layer and a wind farm of infinite size. Furthermore, a largely unspecified model correction for finite wind farms is applied that depends on the wind farm layout, wind rose and neighboring wind farms. The model is validated against measured net capacity factors of 72 offshore wind farms situated in the Baltic, North, and Irish Seas. Finally, national policies for planned offshore wind farms are investigated, and some of these are stated to assume capacity factors significantly in excess of the proposed theoretical limit, especially for the Netherlands. The latter led to a public hearing in the Dutch parliament where the authors were interviewed regarding their findings.

Simão Ferreira et al. (2026) addresses an important issue regarding the saturation of offshore wind farms in waters with limited space leading to reduced energy yield, mainly due to wind turbine and farm wake losses. The wind industry and academia have developed a range of complex models to calculate such losses Fitch et al. (2012); Volker et al. (2017); Fischereit et al. (2022), which due to their complexity and computational cost, may not be accessible to policy makers. For this reason, Simão Ferreira et al. (2026) proposed a simplified analytical model that can potentially be applied in a simple spreadsheet, based on the work of Frandsen (1992); Sørensen and Larsen (2021).



In this paper, we address several concerns regarding the validation and application of the model in Simão Ferreira et al. (2026). We also offer a number of clarifications, as the chosen terminology in Simão Ferreira et al. (2026) can lead to misinterpretation of their results. Our main concerns are:

1. The proposed limit of the capacity factor is not a theoretical limit in the same way as, for example, the Betz limit is considered to be for the power coefficient of a single turbine. Instead, the proposed limit is an analytical model limit, meaning that a different choice in model parameters can lead to a different limit.
2. The plotted limit labelled as *theoretical limit* (solid line) in Fig. 4, 5 and 9 in Simão Ferreira et al. (2026) represents a normalized gross annual energy production (AEP), but this is not clear from the paper.
3. The validation of the analytical model with 72 wind farm in Figs. 3, 4 and 5, is not reproducible. This is because the model is corrected by manually counting the free stream turbines for each wind farm, taking into account the wind farm layout, wind rose and neighboring wind farms. This manual approach is only briefly described by Simão Ferreira et al. (2026), while a scientific method is not provided. In addition, the model correction is very sensitive to the outcome of the validation, which is not described in Simão Ferreira et al. (2026).
4. The analytical model of the infinite wind farm wake loss is implicit in Simão Ferreira et al. (2026) due to the need for solving a geostrophic drag law numerically. However, for the application of the 72 wind farms, the model can be expressed as a simple explicit relation that only depends on the turbine spacing, due the use of a constant latitude, thrust coefficient, and roughness length, and the fact that the 72 wind farms have turbines with similar hub heights in logarithmic space. It should be noted that the turbine spacing depends on the wind farm area, but the latter is mathematically undefined for a wind farm layout with a concave shape, which can lead to model uncertainties. Furthermore, the proposed wind farm wind factor mainly depends on two parameters, the finite wind farm correction and the turbine spacing, which is not clear in the work of Simão Ferreira et al. (2026).
5. Simão Ferreira et al. (2026) calculated that the Dutch national policy overestimates the analytical maximum capacity factor (assuming 10% losses) by 49%. However, the references provided by Simão Ferreira et al. (2026) state a range of values for the planned installed rated wind farm power per unit area, or capacity density, of between 4 and 10.5 MW km⁻², and also mention different values of the expected annual full load hours, namely 3700, 4750-5100 hours, which correspond to capacity factors in between 0.42 and 0.58. While a capacity factor of 0.58 is indeed an optimistic estimate, the lower value of 0.42 is in the range of the measured capacity factors of the 72 wind farms. In addition, given the model sensitivity to the finite wind farm correction, it is difficult to claim that the Dutch policy exceeds the modeled capacity factor by 49%. Finally, if the planned wind farm with an installed capacity of 10000 MW is realized, it is unrealistic to consider it as one large wind farm with a uniform turbine density. A more realistic scenario is a wind farm cluster where separate wind farms with a size of 1000-2000 MW are installed over time including space between them, which the analytical model cannot account for.



55 To understand our principal concerns with the work of Simão Ferreira et al. (2026), the main model equations are summarized and discussed in Sect. 2. The finite wind farm correction is addressed in Sect. 3, where we also compare results of an automated method with the results of the undocumented manual method of Simão Ferreira et al. (2026). Several simplifications are shown in Sect. 4, which we use to understand the main parameters of the model. Finally, we address the problems with the validation method in Sect. 5.

60 2 Model definition

The main model equations of Simão Ferreira et al. (2026) are repeated here. We start with a simplified model of the wind distribution at the location of a wind farm, which is the well known Weibull distribution of wind speed, being a function of a shape parameter, $k = 2.4$, and a scale parameter, λ :

$$f(U) = \frac{k}{\lambda} \left(\frac{U}{\lambda}\right)^{k-1} \exp\left(-\frac{U}{\lambda}\right), \quad U_0 = \lambda\Gamma(1 + 1/k). \quad (1)$$

65 Here, U_0 is the mean wind speed and Γ is a Gamma function. Note that we use the subscript 0 to denote freestream conditions while the subscript ∞ is used for infinite wind farm variables.

Subsequently, a simplified model of a wind turbine power curve, P , as function of the wind speed, U , is defined as:

$$\begin{aligned} P(U) &= P_r \left(\frac{U}{U_r}\right)^3 & U \leq U_r \\ P(U) &= P_r, & U_r < U \end{aligned}, \quad U_r = 2\sqrt[3]{\frac{P_r}{\rho C_P \pi D^2}} \quad (2)$$

75 Here, P_r is rated electric wind turbine power generation and U_r is the wind speed at which rated power is achieved. Furthermore, $\rho = 1.225 \text{ kg m}^{-3}$ is the air density, C_P is the constant below-rated power coefficient and D is the rotor diameter. The wind turbine model does not have a cut-in, $U_{\text{cut-in}}$ and cut-out wind speed, $U_{\text{cut-out}}$. For the energy yield calculations, this simplification holds if $U_{\text{cut-in}}/\lambda \ll U_r/\lambda \ll U_{\text{cut-out}}/\lambda$. In Simão Ferreira et al. (2026), values of $k = 2.4$ and $C_P = 0.46$ are assumed for all sites.

The integration of the power curve and Weibull distribution, normalized by the rated power, leads to the capacity factor of a single turbine, which can be expressed as function of $x \equiv U_r/A$ and k :

$$C_{f,0} = f(x, k) = x^{-3} \Gamma\left(1 + \frac{3}{k}\right) \Gamma_{ic}\left(1 + \frac{3}{k}, x^k\right) + \exp(-x^k), \quad (3)$$

80 with Γ_{ic} as the incomplete Gamma function. The equation for $C_{f,0}$ multiplied by a loss factor for losses unrelated to wake effects, f_{loss} , is the analytical upper limit that Simão Ferreira et al. (2026) propose, though this is not clearly stated in their work. Hence, the limit represents a normalized gross AEP $\times f_{\text{loss}}$. The variable x is a parametric variable in Eq. 3 which gives a single line for a fixed k . This variable can also be defined as the ratio of U_r/U_0 , using the constant $c_0 = \Gamma(1 + 1/k)$ from Eq. 1. Furthermore, Eq. 3 is reused several times by Simão Ferreira et al. (2026) (their Eqns. 12, 13 and 16) but it is the same as Eq. 3 with different x definitions.



For an infinite wind farm with uniform turbine spacing, the model of Frandsen (1992); Sørensen and Larsen (2021) can be used to calculate the corresponding wake loss:

$$85 \quad \varepsilon_\infty = \frac{U_\infty}{U_0} = \frac{1 + \frac{\gamma}{\delta}}{1 + \frac{\gamma}{\kappa} \sqrt{\frac{\pi C_T}{8s^2} + \left(\frac{\kappa}{\delta}\right)^2}}, \quad \gamma = \ln\left(\frac{G}{f'h}\right), \quad \delta = \ln\left(\frac{h}{z_0}\right), \quad s = \frac{\sqrt{A_{wf}}}{D(\sqrt{N_{tot}} - 1)}, \quad f' = f \cdot e^4 \quad (4)$$

with $\kappa = 0.4$ as the von Kármán constant, G as the geostrophic wind speed, f as the Coriolis parameter taken at a latitude of 55° , h as the turbine hub height, $z_0 = 10^{-4}$ m as the offshore roughness length, $C_T = 0.75$ as a constant turbine thrust coefficient and s as the turbine spacing normalized by the rotor diameter, which depends on the wind farm area, A_{wf} and the total number of turbines in the wind farm, N_{tot} . For large wind farms, $\sqrt{N_{tot}} \gg 1$, one can express the normalized turbine spacing in terms of installed wind farm power, P_{wf} , per unit area: $s \approx \sqrt{\rho C_P \pi U_r^3 / 8} / \sqrt{P_{wf} / A_{wf}}$. Equation 4 can be used to calculate the geostrophic wind speed using an iterative numerical method by setting $C_T = 0$. Furthermore, Eq. 4 can be used to calculate the capacity factor of an infinite wind farm $C_{f,\infty}$ by the substitution of $x = c_0 U_r / (\lambda \varepsilon_\infty)$ in Eq. 3. The latter is an analytical model for the lower limit of the wind farm capacity factor. It should be noted that the infinite wind farm wake loss may never be reached for a large finite wind farm. For example, Volker et al. (2017) showed that a wind farm covering an area of 10^5 km² has not yet reached a wake loss limit. The latter was obtained from mesoscale simulations including a simplified wind farm model representing a square wind farm using a wind farm length of 338 km, and a range of uniform turbine spacing and wind climates.

Simão Ferreira et al. (2026) introduced the wind farm wind factor, $\phi = U_r / (U_0 \varepsilon)$, which represents $x = c_0 / \lambda \phi$ in Eq. 3. The wind farm wind factor corrects the mean wind speed or Weibull scale parameter to account for wake losses. It should be noted that ε in ϕ is the wake loss for a finite wind farm. An additional model is required to calculate the capacity factor of a finite wind farm, C_f , from $C_{f,0}$ and $C_{f,\infty}$, and is discussed in detail in Sect. 3. Furthermore, Simão Ferreira et al. (2026) also included external wind farm wake losses in their finite correction model. Simão Ferreira et al. (2026) set C_f equal to Eq. 3 and solved for x using a numerical root finding method, from which ϕ can be calculated.

3 Model correction for finite wind farms

105 The model summarized in Sect. 2 can provide two values of the capacity factor, representing a normalized gross AEP, $C_{f,0}$, and a capacity factor including wake losses for an infinite wind farm, $C_{f,\infty}$. These values provide analytical bounds of the capacity factor of a finite wind farm. Sørensen and Larsen (2021) introduced a model to interpolate between $C_{f,0}$ and $C_{f,\infty}$ to obtain a capacity factor of a finite wind farm, C_f :

$$C_f = w C_{f,0} + (1 - w) C_{f,\infty}, \quad w = \frac{N_{free}}{N_{tot}} \quad (5)$$

110 with w as a weight determined from the ratio of free stream turbines, N_{free} , to the total number of turbines. The problem with this method is that the weight has a large impact on C_f and it is not trivial to obtain the weight for real finite wind farms that range in size and can have irregular shapes, as well as non-uniform turbine spacing. Sørensen and Larsen (2021) determined N_{free} by assuming a square regular turbine layout, $N_{free} = a \sqrt{N_{tot}}$, and initially proposed $a = 3$, later revised to a



value between 4.1 and 5.9 (Sørensen et al., 2024) based on a fit using an engineering wake model applied to six offshore wind
115 farms. This gave a corresponding average value of $a = 5.3$. One problem with this method is that the weighting variable can
become larger than one for a wind farm with fewer turbines than a^2 (i.e. fewer than 29 for $a = 5.3$). Hence, one should limit
the weight to one. In a non-peer-reviewed work, Simão Ferreira (2024) proposed an alternative approach by determining the
weight as:

$$N_{\text{free}} = M_{\text{rows}} M_{\text{turbines}} \quad (6)$$

120 where $M_{\text{rows}} = 2.5$ and M_{turbines} is the number of wind farm edge turbines that operate in free stream conditions. Simão
Ferreira et al. (2026) determined M_{turbines} manually for a given wind farm layout, wind rose and neighboring wind farms and
their results were provided in a database Simão Ferreira (2024). However, a scientific method was not provided, meaning that
one cannot reproduce the results given in Simão Ferreira (2024). In this work, we have made an attempt to automate the manual
method by calculating M_{turbines} as follows, performed for each wind farm layout:

- 125 1. A concave polygon shape is fitted to determine the edge turbine and the connections between them.
2. An outward normal vector for each edge turbine is calculated by taking the average of the outward normal vectors of the
neighboring connecting edge lines.
3. For each wind direction sector, l , with steps of 30° , the dot product of the wind direction vector (representing the sector
midway-direction, $\bar{\theta}_l$), with the turbine outward normal vectors, \bar{n}_t is calculated and the inflow edge turbines, $M_{\text{turbines},l}$,
130 are flagged for $\bar{\theta}_l \cdot \bar{n}_t < 0$.
4. The inflow edge turbines are removed if they are in the shadow of an upstream wind farm located within a distance L
using a ray casting method.
5. The number of remaining inflow edge turbines for all sectors is aggregated using a wind rose frequency, f_l ; $M_{\text{turbines}} =$
 $\sum_{l=1}^{12} f_l M_{\text{turbines},l}$.

135 The wind rose is taken from the Global Wind Atlas 4.0 (Davis et al., 2023). The wind farm layouts are obtained from the Open
European offshore wind turbine database (Fischereit et al., 2025) with the exception of the Fryslân offshore wind farm layout,
which is taken from the Open Street Map database (OpenStreetMap contributors (2026)).

An example of our automatic method is shown in Fig. 1, where the Amrumbank West offshore wind farm layout is used.
Figure 1a depicts a concave polygon (although it has become convex for the present example), the edge turbines and the
140 obtained free stream turbines for a wind direction of 240° , namely, $M_{\text{turbines}} = 16$. It is clear that the polygon does not find all
edge turbines at the Eastern side of the farm, and this is related to the fact that a concave polygon is mathematically undefined.
The Amrumbank West wind farm is part of the N4 wind farm cluster, and the upstream neighboring wind farms are used to
filter the free stream turbines if they are located in their wake with a distance $L = 10S = 59D$, which reduces M_{turbines} to 8.
These steps are then repeated for all twelve sectors and the results are averaged using weights from the wind rose frequency

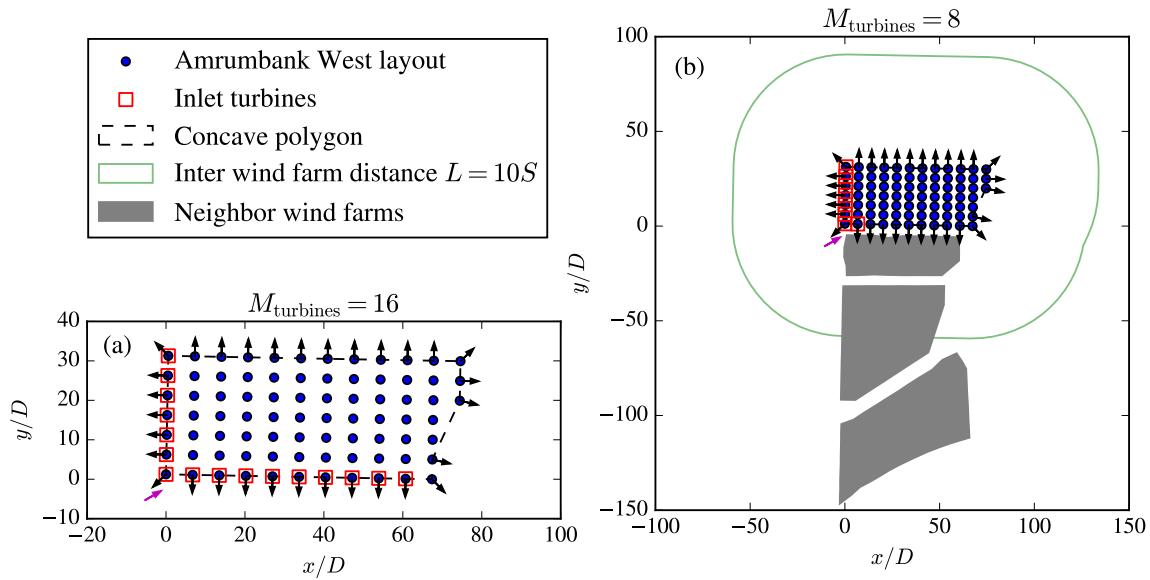


Figure 1. Example of the automated method for determining the number of free stream edge turbines, M_{turbines} , of the Amrumbank West offshore wind farm. (a) without considering neighboring wind farms, (b) considering neighboring wind farms. The black arrows are the turbine outwards normal vectors and the magenta arrow is the wind direction set to 240° .

145 leading to $M_{\text{turbines}} = 11.3$. The manual method of Simão Ferreira et al. (2026) reported $M_{\text{turbines}} = 15$ in Simão Ferreira (2024) for this wind farm. The results of our automated method are compared with the results of the manual method of Simão Ferreira et al. (2026) in terms of the ratio of free stream turbines to the total number of turbines in Fig. 2. Our results are shown including and excluding upstream wind farms (Step 4). In addition, the results of the analytical method of Sørensen et al. (2024) with $a = 5.3$ are also shown in Fig. 2. Sørensen et al. (2024) never intended to use their method for including effects of the wind rose and neighboring wind farms; therefore, the comparison of their model results shown in Fig. 2 should not be compared directly with the other results. Overall, our method replicates the trends of Simão Ferreira et al. (2026) when taking upstream wind farms into account. However, there are also large differences, for example, for the Anholt offshore wind farm, possibly because many turbines are located at the edge of the farm. The impact of the different methods of obtaining N_{free} is large and is described in Sect. 5

155 It should be noted that we do not recommend our automated method to be used as a correction for finite wind farms situated in a wind farm cluster. For example, it is not trivial to determine the distance, L , at which upstream wind farm wakes should be taken into account. In addition, the original model from Frandsen (1992); Sørensen and Larsen (2021) was developed for uniformly spaced wind farms excluding effects of the wind rose, wind farm layout and upstream wind farms. In our opinion, a better application of the model is to include a wind farm cluster as one large wind farm with an effective turbine spacing, although the results may not compare well with higher fidelity models.

160

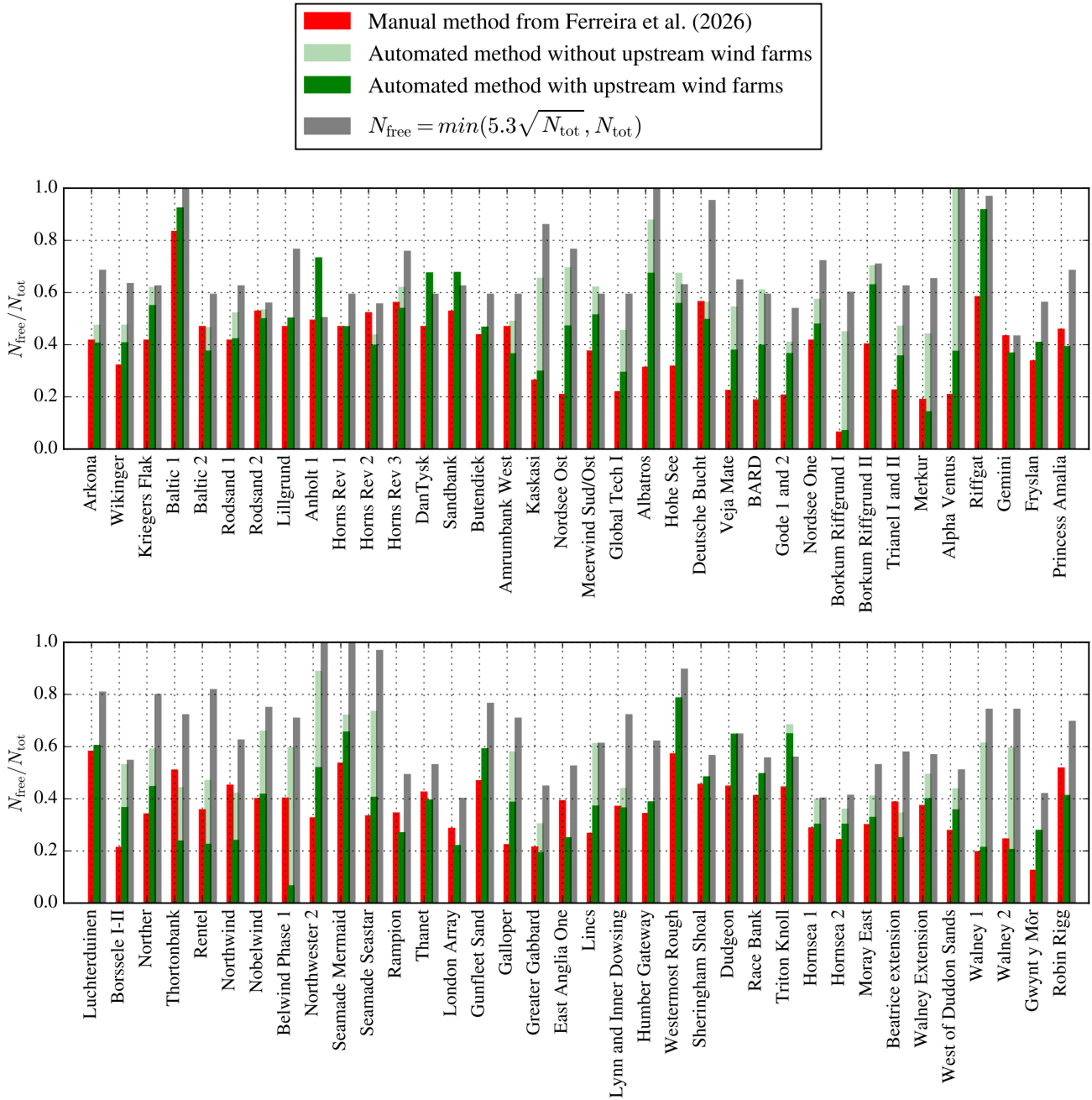


Figure 2. Results of automated model correction for finite wind farms compared to Simão Ferreira et al. (2026).



4 Model simplifications and main parameters

The model from Simão Ferreira et al. (2026) is implicit but it can be shown that simple explicit expression for ε_∞ and ϕ can be derived, when the model is applied to the 72 wind farms. These simplifications are not used in the model validation of Sect. 5. However, it allows us to better understand the main model parameters.

165 The equation for the infinite wind farm wake loss (Eq. 4) is implicit due to the need for solving the geostrophic drag law (Eq. 4 using $C_T = 0$). However, for the 72 offshore wind farms investigated by Simão Ferreira et al. (2026), ε_∞ can be approximated with a simple explicit expression, which was not shown in their work:

$$\varepsilon_\infty = \frac{1 + c_1}{1 + \sqrt{\frac{c_2}{s^2} + c_1^2}}, \quad c_1 = \frac{\gamma}{\delta} \approx 0.218, \quad c_2 = \frac{\pi C_T \gamma^2}{8 \kappa^2} \approx 16.5 \quad (7)$$

Here, the only remaining variable is the normalized turbine spacing, s . The simple expression approximates Eq 4 to within 3%
 170 for all 72 wind farms or 2% when excluding the Lillgrund wind farm (which is an outlier since it has the smallest spacing and lowest turbine hub height), and a comparison with the model results are shown in Fig. 3. The reason why this simplification can be made is because Simão Ferreira et al. (2026) used constant values for the latitude, roughness length and thrust coefficient. In addition, the ratio of hub height to roughness length, h/z_0 and the ratio of the geostrophic wind speed to hub height, G/h , are very similar in logarithmic space for the 72 wind farms, leading to values in the range of $13.3 < \delta < 14.0$ and $2.67 < \gamma < 3.36$,
 175 with corresponding mean values $\delta = 13.7$ and $\gamma = 2.99$, respectively. The mean values of δ and γ , together with the parameters that are chosen as constants by Simão Ferreira et al. (2026), are used to obtain c_1 and c_2 . It should be noted that for much taller turbines, i.e. $h \gg 100$ m, the approximation may not hold.

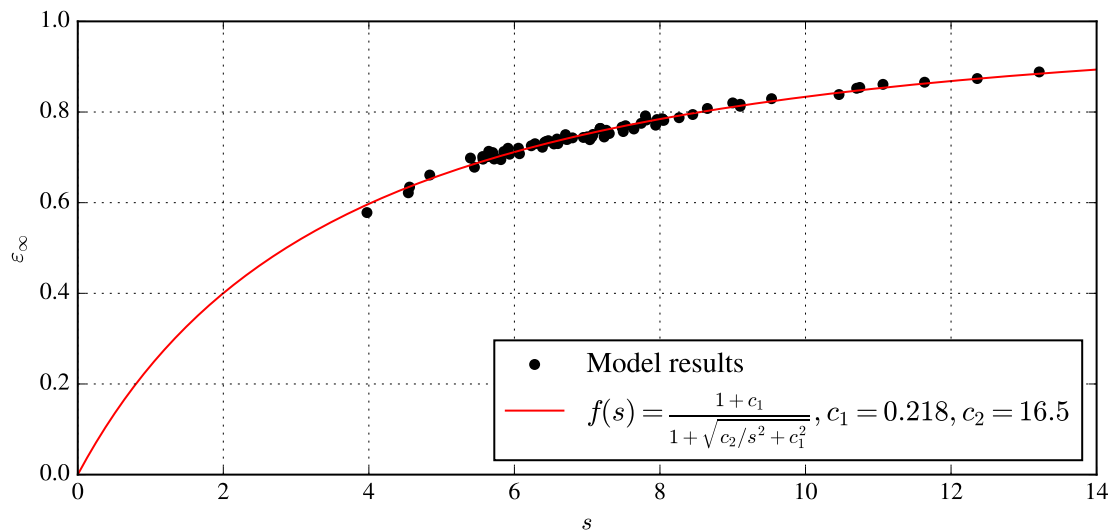


Figure 3. Comparison of model results and simplified expression (Eq. 7) for the infinite wind farm wake loss, ε_∞ .

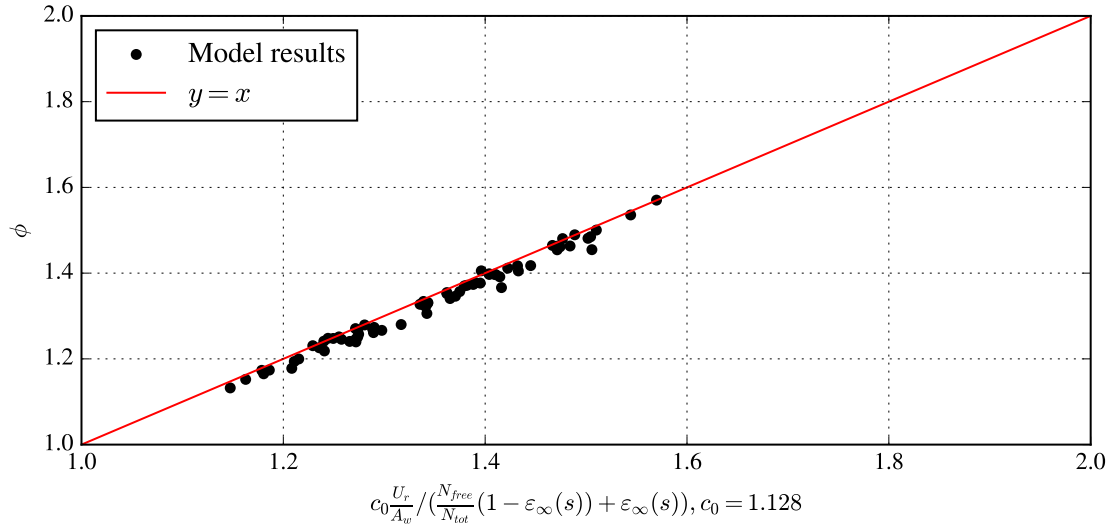


Figure 4. Comparison of model results and simplified expression (Eq. 8) of the wind farm wind factor, ϕ .

The wind farm wind factor, ϕ , is solved numerically by Simão Ferreira et al. (2026), by setting C_f equal to Eq. 3. However, one can show that for the present database of 72 offshore wind farms, ϕ can be approximated with the following explicit relationship using ε_∞ from Eq. 7:

$$\phi \approx c_0 \frac{U_r}{A_w} \frac{1}{\frac{N_{free}}{N_{tot}} (1 - \varepsilon_\infty(s)) + \varepsilon_\infty(s)}, \quad (8)$$

A comparison of ϕ using the implicit method of Simão Ferreira et al. (2026) and our explicit expression of Eq. 8 is shown in Fig. 4. The maximum difference with the implicit calculation method of Simão Ferreira et al. (2026) is 3.5%. This shows that the main parameters to calculate ϕ are the finite wind farm correction factor N_{free}/N_{tot} and the normalized turbine spacing s , which is further motivated from the fact that U_r/A_w is often of the order of 1.

5 Model validation

Simão Ferreira et al. (2026) validated their model with measured capacity factors from 72 offshore wind farms. It is important to note that these measured capacity factors include losses from wake effects and any other losses, such as grid losses, curtailment and turbine availability. The main validation was performed by plotting the net measured capacity factor as a function of the wind farm wind factor $\phi = U_r/(U_0\varepsilon)$, where U_r is the rated wind speed (Eq. 2), U_0 is the mean wind speed (Eq. 1) and ε is the modeled wake loss for a finite wind farm. The model results for ϕ of Simão Ferreira et al. (2026), taken from their Table S1, are depicted in Fig. 5. We disregard results of four wind farms: Baltic 1 – Baltic 2 and Princess Amalia – Luchterduinen, because their measured capacity factors were only available in pairs, not individually. Fig. 5 also includes the normalized analytical model gross AEP (Eq. 3 using x as a parametric variable) and the corresponding analytical model result \times a loss

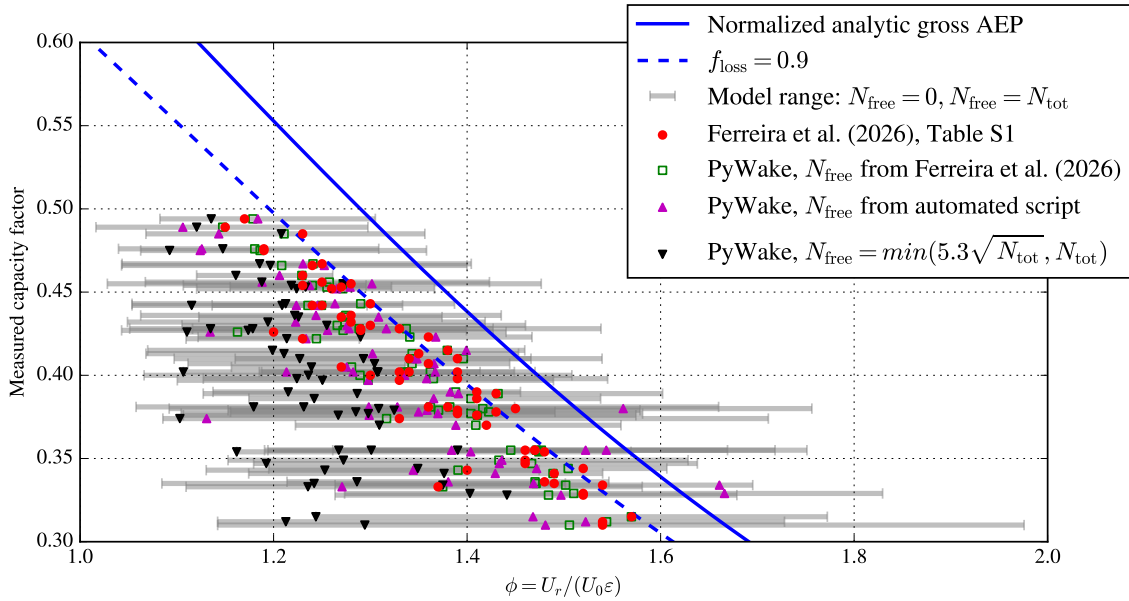


Figure 5. Measured capacity factor as function of modeled wind farm wind factor, ϕ , using different models of the finite wind farm corrections.

195 factor of 0.9. The model only determines the location of x in Fig. 5. However, since the model is heavily dependent on the model correction for finite wind farms, $N_{\text{free}}/N_{\text{tot}}$, this x location can vary between $\varepsilon = 1$ (no wake losses, $N_{\text{free}} = N_{\text{tot}}$) and $\varepsilon = \varepsilon_{\infty}$ (infinite wind farm wake losses, $N_{\text{free}} = 0$). The latter is depicted as a model range in Fig. 5, which shows that the model of the finite wind farm correction has a large influence on ϕ . The left and right error bar symbols reflect no wake losses and infinite wind farm wake losses. This means that a data point moves to the right and can even cross the normalized analytic gross AEP for $N_{\text{free}} \rightarrow 0$. Figure 5 also depicts three more results for ϕ , where the model implementation of Sørensen et al. (2024) (*MinimalisticPredictionModel*) in PyWake v2.6.18 (Pedersen et al., 2023) is employed, and with different models of the finite wind farm correction in terms of N_{free} . First, PyWake is used with N_{free} from Simão Ferreira et al. (2026) in an attempt to obtain the same results. Despite using the same input data as Simão Ferreira et al. (2026), different results are obtained possibly due to differences in model implementation. Subsequently, PyWake is employed with our automated script
 200 for calculating N_{free} , as discussed in Sect. 3, which results in a larger spread of the x -values in Fig. 5. Finally, PyWake is used with the N_{free} model of Sørensen et al. (2024), which results in lower ϕ values and an even large spread in the model results.

The four model results of Fig. 5 are also depicted in Fig. 6 and are plotted against the measured net capacity factor. These results are fitted with a linear relationship, which shows how the r^2 value reduces when going from the manual N_{free} method of Simão Ferreira et al. (2026) (Fig. 5a) to our automated method (Fig. 5c). The r^2 values are the lowest for the N_{free} method
 210 of Sørensen et al. (2024) (Fig. 5d). Here, we remind the reader that Sørensen et al. (2024) never intended to use their method to include effects of the wind rose and neighboring wind farms, hence, it is expected to obtain a large spread.

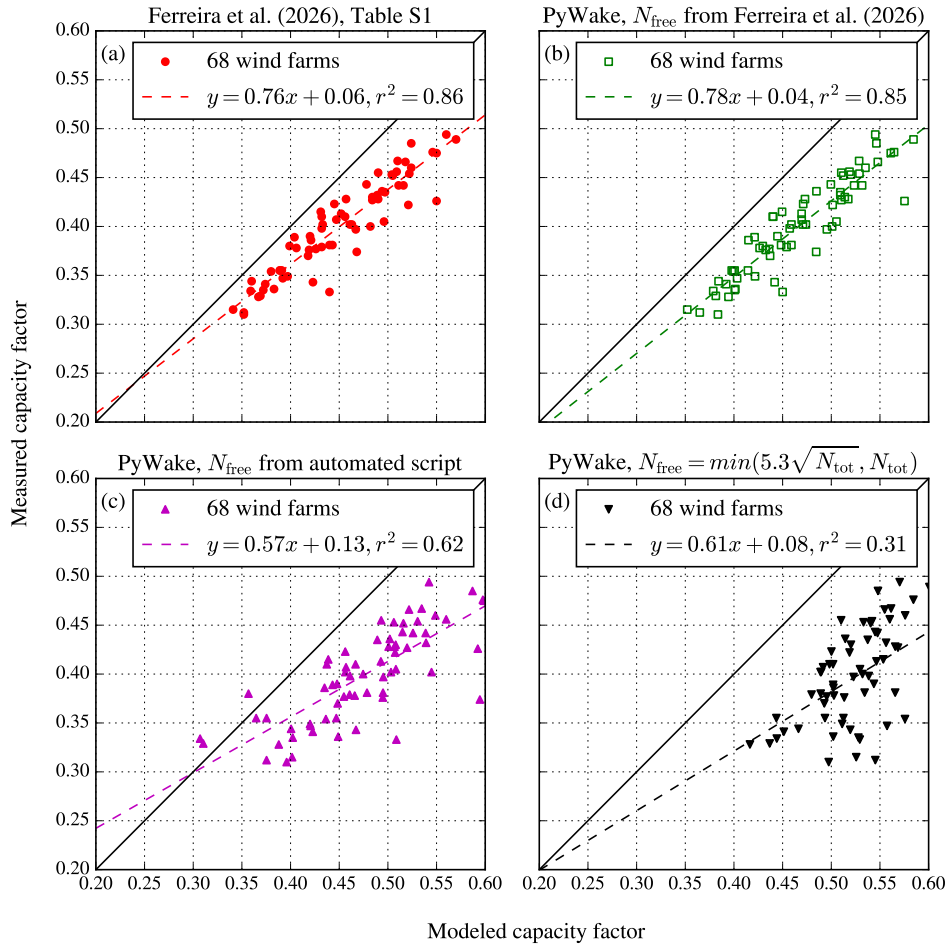


Figure 6. Measured vs modeled capacity factor as using different models for N_{free} compared to Simão Ferreira (2024).

While the model can provide analytical bounds of the wind farm capacity factor representing no wake losses and infinite wind farm wake losses, one should be careful when applying the model to finite wind farms. The large sensitivity of N_{free} , as shown in Figs. 5 and 6, makes it impossible to draw strong conclusions about a limit for finite wind farms.

215 6 Conclusions

In this work, we have discussed a number of concerns regarding the paper of Simão Ferreira et al. (2026). We have shown that the proposed limit of the wind farm capacity factor from Simão Ferreira et al. (2026) is not a theoretical limit but should be considered a model limit that is based on a normalized gross AEP multiplied by a loss factor. The application of the model to the 72 offshore wind farms and choice of model parameters by Simão Ferreira et al. (2026) reveal two main model parameters, namely, the wind turbine spacing and the finite wind farm correction. The latter is a very sensitive model parameter that

220



dominates the model results and validation with net measured capacity factors. Furthermore, the finite wind farm correction applied in Simão Ferreira et al. (2026) (as briefly discussed in a non-peer-reviewed work of Simão Ferreira (2024)), is an *ad hoc* manual method that is not well described and we were not able to reproduce the results with an automated method. Given the sensitivity of the model to finite wind farm correction, it is not trivial to use the model to assess national policies regarding the capacity factors of planned offshore wind farms. Finally, the Dutch national policy is even more difficult to assess due to the range of capacity factors and wind farm densities mentioned in the references provided by Simão Ferreira et al. (2026).

Code and data availability. The Python script to generate the plots is available at <https://doi.org/10.5281/zenodo.19235300>.

Author contributions. MPVDL has performed the model calculations, introduced the model simplifications, created the automated method of the finite wind farm correction, drafted the article and produced the figures. SW analyzed the 72 wind farms, produced a preliminary result of Fig. 6d and investigated the Dutch national policy case. All authors contributed to the discussions, methodology and finalization of the paper.

Competing interests. The authors declare that they have no conflict of interest.

Acknowledgements. We would like to thank Jake Badger for his feedback on the initial draft of this work.



References

- 235 Davis, N. N., Badger, J., Hahmann, A. N., Hansen, B. O., Mortensen, N. G., Kelly, M., Larsén, X. G., Olsen, B. T., Floors, R., Lizcano, G.,
Casso, P., Lacave, O., Bosch, A., Bauwens, I., Knight, O. J., Potter van Loon, A., Fox, R., Parvanyan, T., Krohn Hansen, S. B., Heathfield,
D., Onninen, M., and Drummond, R.: The Global Wind Atlas: A High-Resolution Dataset of Climatologies and Associated Web-Based
Application, *Bulletin of the American Meteorological Society*, 104, E1507–E1525, <https://doi.org/10.1175/BAMS-D-21-0075.1>, 2023.
- Fischereit, J., Schaldemose Hansen, K., Larsén, X. G., van der Laan, M. P., Réthoré, P.-E., and Murcia Leon, J. P.: Comparing and validating
240 intra-farm and farm-to-farm wakes across different mesoscale and high-resolution wake models, *Wind Energy Science*, 7, 1069–1091,
<https://doi.org/10.5194/wes-7-1069-2022>, 2022.
- Fischereit, J., Vollmer, L., and Hansen, A.: Open European offshore wind turbine database, <https://doi.org/10.5281/zenodo.17311571>, 2025.
- Fitch, A. C., Olson, J. B., Lundquist, J. K., Dudhia, J., Gupta, A. K., Michalakes, J., and Barstad, I.: Local and Mesoscale Impacts of Wind
Farms as Parameterized in a Mesoscale NWP Model, *Monthly Weather Review*, 140, 3017–3038, [https://doi.org/10.1175/MWR-D-11-
00352.1](https://doi.org/10.1175/MWR-D-11-
245 00352.1), 2012.
- Frandsen, S.: On the wind speed reduction in the center of large clusters of wind turbines, *Journal of Wind Engineering and Industrial
Aerodynamics*, 39, 251–265, [https://doi.org/https://doi.org/10.1016/0167-6105\(92\)90551-K](https://doi.org/https://doi.org/10.1016/0167-6105(92)90551-K), 1992.
- OpenStreetMap contributors (2026): Distributed under the Open Database License (ODbL), <https://www.openstreetmap.org>.
- Pedersen, M. M., Meyer Forsting, A., van der Laan, P., Riva, R., Alcayaga Román, L. A., Criado Risco, J., Friis-Møller, M., Quick, J.,
250 Schøler Christiansen, J. P., Valotta Rodrigues, R., Olsen, B. T., , and Réthoré, P.-E.: PyWake 2.5.0: An open-source wind farm simulation
tool, <https://gitlab.windenergy.dtu.dk/TOPFARM/PyWake>, 2023.
- Simão Ferreira, C.: Offshore wind farm energy production database. 4TU.ResearchData, [https://doi.org/10.4121/ff8c99b5-c273-4ae0-9c82-
4ade1391813a.v1](https://doi.org/10.4121/ff8c99b5-c273-4ae0-9c82-
4ade1391813a.v1), 2024.
- Simão Ferreira, C., Larsen, G. C., and Sørensen, J. N.: A theoretical upper limit for offshore wind energy extraction, *Cell Reports Sustain-
255 ability*, 3, 1–19, <https://doi.org/doi:10.1016/j.crsus.2025.100573>, 2026.
- Sørensen, J. N. and Larsen, G. C.: A Minimalistic Prediction Model to Determine Energy Production and Costs of Offshore Wind Farms,
Energies, 14, <https://doi.org/10.3390/en14020448>, 2021.
- Sørensen, J. N., Garcia, A. M. I., Larsen, G. C., Pedersen, M. M., and Fournely, D.: Extension and Validation of Minimalistic Pre-
diction Model to Determine the Energy Production of Offshore Wind Farms, *Journal of Physics: Conference Series*, 2767, 092022,
260 <https://doi.org/10.1088/1742-6596/2767/9/092022>, 2024.
- Volker, P. J. H., Hahmann, A. N., Badger, J., and Jørgensen, H. E.: Prospects for generating electricity by large onshore and offshore wind
farms, *Environmental Research Letters*, 12, 034022, <https://doi.org/10.1088/1748-9326/aa5d86>, 2017.